# TH 169/TH 282/CR 9 Interchange Concept Study 

Prepared By:

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This concept study was completed in cooperation between the City of Jordan, MnDOT and


Scott County

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## INTRODUCTION

The City of Jordan has been working with Scott County and MnDOT for over 20 years to develop proposed solutions for the TH 169/TH 282/CR 9 intersection area. Improvements are needed to address safety and operational concerns in the area, and the challenges are complex. A long-term solution is needed for the area, and the consent of the City of Jordan, Scott County, MnDOT, and the Jordan business community must be obtained for any proposed solution.

On April 17, 2018, the Jordan City Council approved a consultant contract with Kimley-Horn and Associates, Inc. for Concept Design and Consensus Building for the TH 169/TH 282/CR 9 intersection area. Our scope included traffic engineering, conceptual design, and stakeholder engagement services to develop a preliminary layout that demonstrates the ultimate vision for the corridor. We considered past work completed for the project area and also explored new alternatives to develop a vision for the TH 169/TH 282/CR 9 area that the City, County, and MnDOT can move forward to implementation.

Funding is not currently available to allow the improvements to proceed to construction. The goal of this study was to establish an agency supported design concept and estimated cost for the improvements to allow the City, County, and MnDOT to move forward with additional planning and the pursuit of project funding. Additional environmental review will also be required as a part of the future planning efforts to comply with National Environmental Policy Act (NEPA) requirements.

A Technical Advisory Committee (TAC) consisting of staff from the City of Jordan, Scott County, and MnDOT as well as three Jordan City Council members met several times and worked cooperatively to advance this study. The purpose of the TAC was to understand individual agency perspectives and to gain insight relative to key issues or perceived impacts, discuss potential mitigation strategies to minimize negative impacts, and identify considerations that could influence the study outcome.

This report summarizes the findings and direction of the TAC, identifies the concept alternatives considered, details the scope and estimated cost for the proposed agency supported interchange concept, and provides a potential phasing plan for the proposed improvements.

A project location map is provided in Appendix A.

## STAKEHOLDER ENGAGEMENT SUMMARY

Stakeholder engagement was an essential element of this study as agency coordination was critical, considering that the roadways in the study area are under the jurisdiction of the City, Scott County, and MnDOT. The following is a summary of the stakeholder engagement activities that occurred:

## Technical Advisory Committee (TAC) Meetings

A TAC was formed at the beginning of the study to assist in making decisions and advancing the study. The committee included the following members:

- Tanya Velishek, Jordan Mayor
- Jeff Will, Jordan City Council Member
- Mike Franklin, Jordan City Council Member
- Tom Nikunen, Jordan City Administrator
- Mike Waltman, Jordan City Engineer
- Jon Solberg, MnDOT
- Almin Ramic, MnDOT
- Lisa Freese, Scott County
- Tony Winiecki, Scott County
- Craig Jenson, Scott County
- Mark Callahan, Scott County
- Jon Horn, Kimley-Horn
- Brandon Bourdon, Kimley-Horn

Over the course of the study, TAC meetings were held on the following dates:

- May 22, 2018
- June 26, 2018
- July 24,2018
- August 28, 2018
- September 25, 2018
- October 23, 2018

Minutes from the TAC meetings are included in Appendix B.

## Jordan City Council Meetings

Updates were provided to the Jordan City Council on the following dates:

- August 20, 2018 (work session)
- November 19, 2018 (work session)
- December 3, 2018 (regular meeting)

The City Council was asked to adopt an agency supported concept at its meeting on December 3, 2018.

## Public Open House

A public open house was held on October 29, 2018 to present the initial findings of the study and gather input from stakeholders. More than 25 people attended the open house meeting. The open house meeting materials were also made available on the City's website for those that were not able to attend the meeting. Written comments were received from 7 people in response to the materials shared at the open house and on the City's website.

The public open house materials are included in Appendix C.

## Local Business Meetings

Individual property owner meetings were held with Wolf Motors and Radermacher's at their request to discuss the interchange concepts and review specific impacts to their properties.

## CONCEPT DEVELOPMENT AND TRAFFIC ANALYSIS

This study utilized a collaborative process where concepts were developed over time with input from stakeholders. A traffic analysis was completed as an initial task to understand traffic forecasting, operations, and safety issues in the project area. The following intersections were included within the study area.

- CR 9/190 ${ }^{\text {th }}$ Street West
- CR 9/Union Pacific Railroad Crossing
- CR 9/Syndicate Street
- TH 169/TH 282/CR 9
- TH 169/Creek Lane
- TH 282/Triangle Lane
- TH 282/Business Access (Radermacher's)
- TH 282/Creek Lane
- Triangle Lane/Creek Lane

A memorandum summarizing the results of the traffic forecasting, safety, and operations analysis is provided in Appendix E.

The following is a summary of the key issues discussed as a part of the TAC meetings that helped support the development of a vision for corridor.

## TAC Meeting \#1

An overview of the scope of work for the interchange concept study was presented and feedback was received. There was discussion regarding the history of prior planning efforts for this project and preliminary design considerations that should be used to evaluate any proposed interchange alternatives.

## TAC Meeting \#2

The draft existing traffic operations and safety findings were presented. The traffic analysis showed that there is already a relatively high right-turn volume from Creek Lane to northbound TH 169 during the AM peak period. This shows that many drivers are avoiding the signalized intersection at TH 169/TH 282/CR 9. Overall, the intersections in the study area were found to operate acceptably but there are some turning movements that are experiencing an undesirable level-of-service (LOS) and delay. The intersections of TH 169/TH 282/CR 9 and TH 282/Triangle Lane both are experiencing crash issues due to those intersections being closely spaced full movement intersections.

Using the input provide during the first TAC meeting, a draft interchange concept evaluation matrix was reviewed, and input was obtained on the evaluation and scoring approach. Eight schematic interchange concepts were presented and discussed.

## TAC Meeting \#3

The traffic analysis, evaluation matrix, and schematic design concepts were the focus of the discussion. Key discussion items were as follows:

- There were some differences in the 2040 forecasts identified as part of the traffic forecasting process. The City and Scott County Comprehensive Plans showed 2040 traffic forecasts that did not consider much development potential north of TH 169, although those forecasts followed the required comprehensive planning process. The $190^{\text {th }}$ Street \& CSAH 9 Traffic Study completed by the City showed considerable growth potential north of TH 169. A set of forecasts that assumed some of the growth potential documented in the 190th Street \& CSAH 9 Traffic Study would occur north of TH 169 was presented to the TAC. The TAC agreed the forecasted traffic volumes presented were acceptable for the future conditions traffic analyses.
- An updated interchange evaluation matrix was presented that incorporated comments from the prior TAC meeting. The TAC agreed this version of the evaluation matrix should be used to evaluate the concepts.
- The TAC selected three concepts to move forward to more detailed concept development. The concepts included a roundabout/split diamond option with CR 9/TH 282 bridged over TH 169, a folded diamond/tight diamond with CR 9/TH 282 bridged over TH 169 and modified to include the split diamond configuration for northbound TH 169 access, and an option that included TH 169 bridged over CR 9/TH 282.


## TAC Meeting \#4

The meeting focused on the review of the three detailed concepts that were selected at TAC Meeting \#3 as follows:

- It was discussed that the railroad crossing volumes are relatively low, but there was also discussion that rail crossings could increase in the future and seasonally.
- A roundabout/split diamond option was presented that did not include grade separation of the CR $9 /$ railroad crossing. It was discussed that a railroad crossing could be added later; however, significant reconstruction costs would be incurred to address the differences in roadway profiles.

The TAC requested that a concept be developed that includes a roundabout/split diamond configuration with grade separation at the railroad crossing.

- Concerns were expressed regarding a higher frequency of wrong way incidents with folded diamonds.
- It was discussed that TH 169 being bridged over TH 282/CR 9 will result in TH 169 mainline reconstruction which would be challenging from a construction phasing/staging perspective. This option would be more conducive to allowing an additional vehicle and pedestrian connection under TH 169 at Creek Lane. The TAC requested that a concept be developed that includes grade separation at Creek Lane and TH 169.


## TAC Meeting \#5

The following topics were discussed:

- Draft future 2040 traffic analysis intersection LOS results were presented for no-action and all five interchange concepts. No action operates unacceptably at many intersections with significant delays and vehicle queuing. These results support the need for improvements. All the proposed concepts operate at acceptable overall intersection LOS under future conditions.
- Based on input from TAC Meeting \#4, the following five concepts were reviewed and discussed:
o Concept 1 - Roundabout/Split Diamond
o Concept 1A - Roundabout/Split Diamond with Railroad Grade Separation
o Concept 2 - Folded Diamond/Tight Diamond
o Concept 3 - TH 169 over CR 9/TH 282
o Concept 3A - TH 169 over CR 9/TH 282 and Creek Lane
- The interchange evaluation matrix was presented and discussed.
- Considering all factors (with costs being important) a majority of the TAC preferred Option 1 with some interest in adding the railroad grade separation shown in Option 1A if funding becomes available. There was also some support for Option 3 due to traffic routing concerns along Creek Lane and business visibility.


## TAC Meeting \#6

The following topics were discussed:

- Potential phasing plans for the concepts were reviewed with the TAC.
- Potential construction impacts for the concepts were discussed including that Concept 3 and 3A would likely result in the need to close portions of TH 169 during construction.
- Preparations for the October 29, 2018 public open house meeting were discussed.
- Feedback from recent property owner discussions was reviewed.
- A majority of the TAC continued to support Concepts 1 and 1A.

The five interchange concept layouts (1, 1A, 2, 3, 3A) developed during the study and the final evaluation matrix are provided in Appendix D.

Preliminary estimated costs for the five interchange concept layouts are summarized below. The costs include estimated construction, right-of-way acquisition, and indirect costs, and assume 2019 construction dollars.

- Concept 1 \$27 Million
- Concept 1A \$32 Million
- Concept 2 \$36 Million
- Concept 3 \$33 Million
- Concept 3A \$40 Million

Detailed preliminary cost estimates for each of the concepts are provided in Appendix F.

## IMPLEMENTATION PLAN

Concepts 1 and 1A were recommended by the TAC as the agency supported vision for the project area. As mentioned above, funding is not currently available to allow the improvements to proceed to construction. The goal of this study was to establish an agency supported design concept and estimated cost for the interchange to allow the City, County, and MnDOT to move forward with additional planning and the pursuit of project funding.

Potential funding sources that could be pursued for the interchange improvements include the following:

- Metropolitan Council Regional Solicitation (Federal Funding)
- MnDOT Corridors of Commerce Program (State Funding)
- MnDOT Freight Investment Plan (State Funding)
- FHWA TIGER Program (Federal Funding)
- Transportation Economic Development (TED) Program (State Funding)
- Bonding Bill Funds (State Funding)
- Other Federal and State Programs (LRIP, HSIP)
- Scott County Funds
- City of Jordan Funds (MnDOT State Aid or other City Funds)

The consensus and support of the jurisdictional agencies (MnDOT, Scott County, and the City of Jordan) will be important as potential funding sources are pursued.

The possibility of phasing the interchange improvements was investigated as a part of this study. The ability to implement the improvements in phases over time would provide some additional flexibility in how the project moves forward. The City has already secured LRIP funding for the construction of a roundabout at the TH 282/Creek Lane intersection that could serve as the first phase of the proposed interchange improvements. An implementation plan concept is provided in Appendix G that illustrates a possible phasing plan for the improvements. Implementing the project in phases could help mitigate construction impacts to the businesses in the project area and allow some improvements to proceed as funding is secured rather than waiting until all of the necessary funding is obtained for the complete interchange project.

A November 14, 2018 letter from MnDOT to the City of Jordan clarifying their interests and expressing support for improvements at the TH 169/TH 282/CR 9 intersection is provided in Appendix H.

A December 18, 2018 letter from Scott County to the City of Jordan stating their support for the interchange planning work and outlining their suggested next steps is provided in Appendix I.

## APPENDICES

## APPENDIX A - PROJECT LOCATION MAP

TH 169/TH 282/CR 9


## APPENDIX B - TAC MEETING MINUTES

## Minutes

## Technical Advisory Committee (TAC) Meeting \#1

May 22, 2018

Attendees<br>Tanya Velishek, Jordan Mayor<br>Jeff Will, Jordan City Council Member<br>Mike Franklin, Jordan City Council Member<br>Tom Nikunen, Jordan City Administrator<br>Jon Solberg, MnDOT (by phone)<br>Lisa Freese, Scott County<br>Tony Winiecki, Scott County<br>Craig Jenson, Scott County<br>Mike Waltman, Bolton \& Menk<br>Jon Horn, Kimley-Horn<br>Brandon Bourdon, Kimley-Horn

Meeting notes identified in Italics below. Action items are highlighted in Bold.

## 1. INTRODUCTIONS

2. REVIEW SCOPE OF WORK
A. Stakeholder Engagement
B. Traffic Analysis
C. Interchange Alternative Concept Development and Evaluation
D. Determine Preferred Design Concept
E. Cost Estimates and Funding Plan

After introductions, a brief review of the scope of work was provided.
3. BACKGROUND INFORMATION
A. History/Past Work
B. Design Considerations
C. Agency Comments/Concerns

A brief history of past work for this project was provided and the group reviewed/discussed a list of preliminary design considerations (attached) that would be used to evaluate various interchange alternatives. A summary of these discussions is provided below.

- Right-of-way impacts - partial versus total property takes should be considered since partial takes are generally more desirable that total takes.
- Travel distances and times between businesses and TH 169 may be good way to present information if comparable distances and travel times are provided using different routes.
- Need to consider oversize truck access to businesses.
- The Renaissance Festival has a lease thru 2019 at their current location. Scott County is waiting for the Renaissance Festival to provide anticipated traffic information including an event traffic management plan for the proposed relocation site. The last meeting between the Renaissance Festival and Scott County occurred before Christmas 2017. Given an EIS is required it may take longer than 2019 before the potential relocation occurs.
- A roundabout layout has been developed for the intersection of TH 282 and Creek Lane. The City is currently looking for funding for the improvements. The City supports this as an initial phase of the project and it is included in the City's CIP for 2019. Bolton \& Menk will provided the proposed roundabout layout to Kimley-Horn.
- Emergency access is particularly important given the police department is located on the northeast quadrant of the TH 169 / TH 282 / CR 9 intersection.
- There has been prior discussion of raising the TH 169 overpass over Sand Creek due to floodplain issues. If that were to occur, it could also serve as a potential pedestrian crossing of TH 169.
- County policy is to have bike and pedestrian facilities on both sides of a roadway. MnDOT only contributes to providing pedestrian facilities on one side of the roadway.
- Snowmobiles travel from the trail along the Minnesota River to/from the Holiday Station. Scott County mentioned that snowmobile access through interchanges can cause challenges but snowmobile crossings have been accommodated at other interchanges.
- It was clarified that total project costs need to be considered including construction, engineering, administrative, and right-of-way costs.
- The City mentioned that Section $4 f$ issues should not be a problem at Lions Park; however, this should be confirmed. Lions Park also serves as a small park-n-ride lot (informal - not operated by a transit authority).
- There are no transit or park-n-ride plans anticipated in the project area. We should consider options for a small park-n-ride lot if space is available.
- Future environmental review for any proposed improvements needs to be considered as a part of the concept design process. Our scope of work does not include any NEPA or formal environmental review. We need to make sure that the concept design process provides flexibility for any future environmental review process.
- It is desirable to minimize impacts to the Valley Green neighborhood (social justice concerns).
- It was discussed whether an on-ramp to northbound TH 169 could be provided from Creek Lane rather than TH 282 / CR 9. This could be an option but the grades in the area need to be reviewed.
- TH 282 may be a future jurisdictional transfer candidate from MnDOT to the County.
- The need to maintain business visibility was discussed further. Belle Plaine was cited as an example where an interchange has impacted businesses. There was some discussion
regarding the importance of visibility and how that varies by the type of customer a particular business attracts.
- Creek Lane likely will need to be reconstructed and it is anticipated to be more than a twolane roadway.
- There was some discussion on what the impacts may be to TH 282 access east of the Sand Creek bridge and if there will be adequate gaps for traffic to access TH 282 between Sand Creek and TH 21.


## 4. PROJECT SCHEDULE

A. Future TAC Meeting Dates/Times

The group decided that future meetings should occur the fourth Tuesday of each month from 7:00 AM - 8:30 AM at Jordan City Hall. Kimley-Horn will send out a schedule invite for the future meetings.
5. NEXT STEPS
A. Gather Background Information
B. Begin Traffic Analysis
C. Begin Concept Development
D. Develop Draft Evaluation Matrix

Kimley-Horn to begin traffic analysis work.
Kimley-Horn to prepare draft evaluation matrix for review/discussion at the next TAC meeting.
Kimley-Horn to prepare initial interchange alternative concepts for review/discussion at the next TAC meeting.

6. QUESTIONS/OTHER DISCUSSION | CIFTO |
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## Design Considerations - Draft

May 22, 2018

1. RIGHT-OF-WAY AND BUSINESS IMPACTS
A. Right-of-way impacts (\# of parcels and area)
B. Maintain existing businesses and business access
C. Provide for future development potential
D. Maintain business visibility
2. TRAFFIC
A. Safety
B. Capacity
C. Ability to serve seasonal events (Renaissance Festival and Scott County Fair)
3. ROADWAY DESIGN
A. Meets intersection access spacing guidelines
B. Number of access restrictions
C. Allows for phased implementation
D. Construction staging flexibility
E. UP Railroad impacts/coordination
F. Utility impacts
4. ENVIRONMENTAL IMPACTS
A. Wetland impacts (area)
B. Sand Creek impacts
C. Park impacts
D. Tree impacts
E. Floodplain/floodway impacts
5. MULTI-MODAL CONSIDERATIONS
A. Bicycle and pedestrian accommodations
B. Transit compatibility
6. COST
A. Total Project Costs
B. Maintenance Costs
7. OTHERS?
A.
B.
C.

## Minutes

## Technical Advisory Committee (TAC) Meeting \#2

June 26, 2018

Attendees<br>Tanya Velishek, Jordan Mayor (by phone)<br>Jeff Will, Jordan City Council Member<br>Mike Franklin, Jordan City Council Member<br>Tom Nikunen, Jordan City Administrator<br>Jon Solberg, MnDOT<br>Tony Winiecki, Scott County<br>Craig Jenson, Scott County<br>Mike Waltman, Bolton \& Menk<br>Jon Horn, Kimley-Horn<br>Brandon Bourdon, Kimley-Horn

Meeting notes identified in Italics below. Action items are highlighted in Bold.

1. TRAFFIC ANALYSIS UPDATE
A. Existing Operations

- Existing turning movement count and AADT exhibit was reviewed.
- The relatively high right-turn volume from Creek Lane to northbound TH 169 during the AM peak was noted.
- Existing level-of-service and delay exhibit was reviewed.
- Eastbound and westbound left-turns from TH 169 operate at LOS E during the AM and PM peak hours.
- Westbound left from the Frontage Road to CR 9 operates at LOS E during the PM peak period. This operations issue has also been identified by Jordan Police.
- The northbound to eastbound right from Creek Lane to TH 169 operates at LOS E in the PM peak period. Tony Winiecki questioned whether the AM and PM LOS for that movement may have been flipped.


## Kimley-Horn to review delays and LOS at the Creek Lane / TH 169 intersection.

B. Existing Safety

- Crash rate exhibit, based on 2010-2015 MnCMAT data was presented.
- TH 169 /TH 282 / CR 9 and TH 282 / Triangle Lane intersections both have a critical index over 1.0. This indicates that a crash issue exists at these two intersections.
- Crash rates at TH 282 / Triangle Lane are due in part to close intersection spacing and sight-line challenges due to traffic congestion at TH 169 /TH 282 / CR 9.
- The TAC questioned the types of accidents that are occurring at these intersections.

Kimley-Horn to review crash types in more detail at the intersections of TH 169 / TH 282 / CR 9 and TH 282 / Triangle Lane.
C. Discuss Traffic Forecasting

- Existing and forecast ADT exhibit was presented
- It was noted that there is a considerable difference in 2040 forecasts from the Scott County Comprehensive Plan and the Jordan 190 th Street Study. Discussion occurred about concerns over the differences, and those differences needed to be resolved prior to additional traffic analysis. The City noted that some additional grown is likely by 2040 in this area as the Comprehensive Plan assumed virtually no growth on the north side of TH 169 and there was also some housing that was not included in the Comprehensive Plan forecasts that was later approved.


## Kimley-Horn to coordinate with the City, County, and MnDOT to develop traffic forecasts that all parties can accept.

- Jeff Will asked about the volumes south of TH 41 on TH 169. Craig Jenson said existing volumes were around 29,000 vehicles per day (vpd). Kimley-Horn has checked the 2040 forecasts along TH 169, and they are 45,000 vpd just north of TH 41, 36,000 vpd just south of CR 14 (150 ${ }^{\text {th }}$ Street), 33,000 vpd just north of Jordan, and 28,000 vpd south of Jordan.


## 2. DISCUSS INTERCHANGE EVALUATION CRITERIA

A. Review Draft Evaluation Matrix

- The following comments were provided on the draft alternative evaluation matrix:
- Change "Minimize Impacts to TH 169 Operations" to "Improves TH 169 Operations"
- Add a category for "Improves Safety"
- Add a category for "Reasonable to Maintain"
- Network travel times were discussed and they will be part of the "Minimize Impacts to Business Access" category
- Add a category for "Serves Freight"
B. Discuss Evaluation/Scoring Approach
- The group discussed ways to evaluate each alternative ranging from trying to score each category with a number (say 1-10) or using red, yellow, and green color codes (bad, fair, good). The group agreed that we should use the color code approach.

Kimley-Horn to update the evaluation matrix based on comments from the TAC.

## 3. REVIEW ALTERNATIVE INTERCHANGE CONCEPTS

- 8 alternative concepts were presented and discussed. Comments are summarized below.
- For options that show a new connection between the Frontage Road/Syndicate Street to Valley View Drive, the inplace Creek Lane alignment should be used to provide the connection to Valley View Road rather than a new alignment.
- Concept 1 can be removed since Concept 2 is identical on the north side of TH 169.
- Concepts 2, 3, 6 and 8 should be carried forward for further evaluation.
- Either Concept 4 or 5 can be removed since the only difference is the intersection control at the south TH 169 / TH 282 ramp terminal (roundabout versus signal).
- Concept 7 can be removed since it is identical to Concept 2, 4 and 5 on the south side.
- It was requested that a concept showing TH 169 going up and over TH 282 /CR 9 be developed.
- It was requested that a concept be developed that shows a TH 282 / CR 9 bridge over TH 169 with right-in/right-out access at the Creek Lane location.
- Tony Winiecki asked about planning level ADTs for a single lane roundabout. KimleyHorn has reviewed NCHRP 672, and the lower volume thresholds range from 15,000 to 18,000 vpd, although more typical volumes served are from 23,000 to 27,000 vpd (the vpd represent the total volume of traffic on both roads at the intersection).
- Once the traffic forecasting issue is resolved, additional analysis can be completed to determine appropriate intersection design.
- An access scenario exhibit for the area along TH 282 between TH 169 and Creek Lane was discussed. A new $3 / 4$ mid-point access scenario was shown that replaced the current Triangle Lane access. Jon Solberg mentioned that this mid-point access could be critical because MnDOT was not confident that grades at Triangle Lane would work with a new interchange at TH 169. It was discussed that Kimley-Horn should look at this area in greater detail and determine potential local roadway reconfigurations with a new mid-point $3 / 4$ access.

Kimley-Horn to update interchange concepts for review/discussion at the next TAC meeting.

## 4. PROJECT SCHEDULE

5. NEXT STEPS
A. Continued Interchange Concept Development and Refinement
B. Traffic Analysis
C. Refine Evaluation Matrix

## 6. QUESTIONS/OTHER DISCUSSION

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## Technical Advisory Committee (TAC) Meeting \#3

July 24, 2018

## Attendees

Tanya Velishek, Jordan Mayor<br>Mike Franklin, Jordan City Council Member<br>Tom Nikunen, Jordan City Administrator<br>Jon Solberg, MnDOT<br>Tony Winiecki, Scott County<br>Craig Jenson, Scott County<br>Mike Waltman, Bolton \& Menk<br>Jon Horn, Kimley-Horn<br>Brandon Bourdon, Kimley-Horn

Meeting notes identified in Italics below. Action items are highlighted in Bold.

## 1. TRAFFIC ANALYSIS UPDATE

A. Creek Lane / TH 169 Operations

- The results previously presented at northbound TH 169 / Creek Lane showed better operations during the AM as opposed to the PM peak periods for the right turn movement from Creek Lane. That seemed odd given the higher side-street traffic volumes during the AM peak. This was reviewed and it was determined that there was a coding error and revised delay output was presented.
B. Crash Type Details
- Additional crash detail was reviewed. The crash trends showed quite a few rear-end crashes as are common at a traffic signal. Several of the crashes were consistent with the close intersection spacing between TH 169 / TH 282 and TH 282 / Triangle Lane.
C. Traffic Forecasting Updates
- A revised table of 2040 traffic forecasts was presented with traffic volumes that were developed taking into consideration some of the growth anticipated to occur as part of the City's $190^{\text {th }}$ Street Study. The group agreed that proceeding with these traffic volumes was reasonable at this point for the analysis of interchange concepts.

2. INTERCHANGE EVALUATION MATRIX
A. Review Updated Evaluation Matrix

- An updated evaluation matrix was presented and discussed. No additional changes were identified. The matrix will be used to compare the 3 selected interchange concepts.


## 3. REVIEW UPDATED INTERCHANGE CONCEPTS

- 7 alternative concepts were presented and discussed as follows:
- The five concepts carried forward from TAC Meeting \#2 with minor updates were: Concept 1 - Diamond / Split Diamond, Concept 2 - Roundabout / Tight Diamond, Concept 3 - Roundabout / Split Diamond, Concept 4 - Folded Diamond / Tight Diamond, Concept 5 - Offset Single Point Urban Interchange. The most notable change was on Concepts 1 \& 5, where the inplace Creek Lane alignment was used to provide the connection to Valley View Road from the frontage road/Syndicate Street.
- Concept 6, a new Quadrant Interchange concept as identified at TAC Meeting \#2 was presented.
- Concept 7, a new concept identified at TAC Meeting \#2 that showed TH 169 going over TH 282 / CR 9 was presented.
- The CR 9 railroad crossing was discussed. Several indicated they did not recall this being a very active at-grade crossing. Kimley-Horn to review rail crossing data and report back to the TAC on findings.
- Additional access scenarios were reviewed along TH 282. A three-quarter access at a slightly relocated shared driveway between Wolf Motors and Radermacher's and a right-in/right-out at Triangle Lane was identified as the preferred design. Kimley-Horn to review access along TH 282 in more detail and develop a proposed design that includes a right-in/right-out at Triangle Lane and a three-quarter access for Wolf Motors/Rademacher's.
- The TAC selected the following three concepts to move forward for further development:
- Concept 3 - Roundabout / Split Diamond
- Concept 4 - Folded Diamond / Tight Diamond modified to include the split diamond configuration for northbound TH 169 access.
- Concept 7-TH 169 going over TH 282 / CR 9

Kimley-Horn to develop more detailed concept designs and begin the evaluation process for the 3 selected concepts (Roundabout / Split Diamond, Folded Diamond / Tight Diamond, and TH 169 going over TH 282 / CR 9).

## 4. PROJECT SCHEDULE

5. NEXT STEPS
A. Preparation of Detailed Interchange Concepts
B. Traffic Operations Analysis
C. Evaluation of Interchange Concepts including Cost Estimates
6. QUESTIONS/OTHER DISCUSSION

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## Technical Advisory Committee (TAC) Meeting \#4

August 28, 2018

Attendees<br>Tanya Velishek, Jordan Mayor<br>Mike Franklin, Jordan City Council Member<br>Jeff Will, Jordan City Council Member<br>Tom Nikunen, Jordan City Administrator<br>Jon Solberg, MnDOT<br>Almin Ramic, MnDOT Traffic<br>Mike Waltman, Bolton \& Menk<br>Tony Winiecki, Scott County<br>Craig Jensen, Scott County<br>Mark Callahan, Scott County<br>Jon Horn, Kimley-Horn<br>Beth Engum, Kimley-Horn

Meeting notes identified in italics below. Action items are highlighted in bold.

## 1. TRAFFIC ANALYSIS UPDATE

A. Rail Crossing Data

- MnDOT's data states there are 5 trains per day crossing CR 9. Kimley-Horn counted 4 trains per day on May 16, 2018 and observed a gate closure duration of around 2 minutes per train. It was discussed that there could be the potential for more trains in the fall for grain hauling and in the future if frac sand hauling increases.
B. Traffic Forecasting Updates
- Traffic forecasting and analysis updates will be presented in more detail at the next TAC meeting; however, all three alternatives generally function at acceptable levels of service. Traffic operations and safety criteria are not a differentiator among the alternatives.
- It was discussed that travel time comparison by alternative will be important for businesses.


## 2. REVIEW INTERCHANGE CONCEPT DESIGNS

- A design speed of 35 mph has been used for CR 9/TH 282 and a design speed of 65 mph has been used for TH 169.
- A large tractor trailer (WB-63) was used for the design of all roundabouts.
- Kimley-Horn to obtain truck dimension information from area truckers/haulers to verify that navigation through roundabouts can be accommodated.
- MnDOT commented that the roundabouts are too large for current traffic volumes. When a locally preferred alternative is determined, the roundabout designs should be reviewed such
that initial construction is based on near-term volumes with the ability to expand capacity as traffic grows.
A. Roundabout/Split Diamond
- Adding a railroad overpass on CR 9 in the future would require reconstruction of a significant portion of the adjacent roundabout.
- Kimley-Horn will develop a layout for Concept 1A to include a railroad overpass. Concept $1 A$ will be added to the matrix and an estimated cost increase compared to Concept 1 will be determined.
B. Folded Diamond/Tight Diamond
- A 5\% maximum profile grade was used and the loop ramp was designed with the minimum radius allowed to avoid impacting the railroad.
- MnDOT commented that a disadvantage of this concept was the potential for drivers traveling the wrong direction on the southbound 169 exit ramp.
- A concern was raised for both Concepts 1 and 2 regarding the ability for trucks to enter TH 169 NB from Creek Lane.
- Kimley-Horn will add information on the layouts for Concept 1 and Concept 2 detailing the modifications needed on the TH 169 NB Sand Creek Bridge as well as a profile of the northbound acceleration lane.
- MnDOT mentioned the need to check sight lines at the NB TH 169 off-ramp looking west on CR 9/TH 282 over the bridge. This will need to be verified during detailed design.
C. TH 169 going over TH 282/CR 9
- This option includes about 4,000 feet of TH 169 reconstruction.
- The detour route for this option was discussed since it would likely require the full closure of TH 169 during construction. It was discussed that there is no good detour option in the area.
- It was discussed whether this option could also include TH 169 going over Creek Lake to provide improved local access for vehicles and pedestrians/bikes.
- Kimley-Horn will develop Concept 3A to include TH 169 also going over Creek Lane which will result in more TH 169 reconstruction. Concept $3 A$ will be added to the matrix and an estimated cost increase compared to Concept 3 will be determined.


## 3. INTERCHANGE EVALUATION MATRIX

A. Review Draft Evaluation Matrix

- A draft evaluation matrix was handed out and discussed.
- Kimley-Horn to change "Minimize Railroad Impacts" criteria to "Improves Railroad Crossing Safety" and change colors (from top to bottom) to yellow, yellow, green, red.

4. PROJECT SCHEDULE

- A current project schedule was distributed.

5. NEXT STEPS
A. Refine Interchange Concept Designs
B. Refine Evaluation Matrix
C. Preparation of Corridor Study Report

## 6. QUESTIONS/OTHER DISCUSSION

- Comments were gathered from the TAC members regarding the three concept alternatives as follows:

Tanya - Wants to see the project done safely and with the least cost. Prefers Concept 1.
Jeff - Prefers Concept 3 but understands that costs could be an issue. When evaluating Concept 3A, we need to recognize that a Creek Lane underpass and new TH 169 bridge over Sand Creek have value.

Jon S. - Not a fan of Concept 2. Is leaning toward Concept 1, especially when considering budget. Concerned about Concept 3 since MnDOT recently replaced the TH 169 pavement in the project area.

Tony - Given that traffic operations, environmental considerations, and right-of-way impacts do not differentiate, the cost factor will be important. Prefers Concept 1.

Craig - Prefers Concept 1 but wants to understand the cost of Concept 1A with the railroad overpass.

Mike W. - Same thoughts as Tony/Craig. Prefers Concept 1.
Mike F. - Leaning toward Concept 1. Likes Concept 3 design, but not if cost prohibitive.
Mark - Prefers Concept 1.
Almin - Prefers Concept 1. Concept 3 is difficult given cost and regional construction impacts.
Tom - Likes Concept 1. Likes the flexibility in phasing the construction of this option.

## Minutes

## Technical Advisory Committee (TAC) Meeting \#5

September 25, 2018

Attendees<br>Tanya Velishek, Jordan Mayor<br>Mike Franklin, Jordan City Council Member<br>Jeff Will, Jordan City Council Member<br>Tom Nikunen, Jordan City Administrator<br>Jon Solberg, MnDOT<br>Tony Winiecki, Scott County<br>Mark Callahan, Scott County<br>Mike Waltman, Bolton \& Menk<br>Jon Horn, Kimley-Horn<br>Brandon Bourdon, Kimley-Horn<br>Meeting notes identified in Italics below. Action items are highlighted in Bold.

1. TRAFFIC ANALYSIS UPDATE
A. Review Traffic Operations Analysis

Kimley-Horn reviewed the traffic analysis. The future forecasts that were used to develop the peak hour turning movement counts were the same as previously presented. Overall intersection level-ofservice (LOS) diagrams were presented for existing, 2040 no action, and 2040 conditions for the three alternatives developed (Concepts 1, 2 and 3). No action operates unacceptably at many locations supporting the need for improvements. All the proposed concepts operate at acceptable overall intersection LOS under future conditions, although the westbound ramp intersection at TH 169 and TH 282 under the Concept 2 alternative operates worse than Concepts 1 and 3. KimleyHorn will provide a draft report summarizing the results of the traffic analysis in advance of our next TAC meeting.

## 2. REVIEW UPDATED INTERCHANGE CONCEPTS

The five concepts were reviewed and discussed as follows:

- Jeff Will suggested that we look at a tight diamond on the north side of TH 169 for Concept 3 (as opposed to roundabout).
- Jon Solberg said he still wanted to get additional input from others at MnDOT regarding the slip ramp concept shown in Concepts 1, 1A, and 2. Kimley-Horn to provide a more detailed Creek Lane slip ramp layout to Jon Solberg so that it can be shared with others at MnDOT for review and comment.
- MnDOT and Scott County do not want to select a concept that rules out the possibility of future grade separation at the railroad crossing. Alternatives 3 and $3 A$ would rule out future grade separation since the grades would not allow you to get from below TH 169 to up and over the railroad given the distance between the proposed westbound ramps and the railroad crossing.
- Jon Solberg was asked the degree to which railroad grade separation may be beneficial in terms of pursuing freight funding. Jon Solberg to seek input from others at MnDOT regarding the advantages of CR 9 railroad grade separation for the pursuit of freight funding.
- Tom Nikunen said that meetings were being scheduled with the local businesses and that the goal is to meet with the most impacted businesses prior to having a general public open house meeting. An open house is being planned for October 29th. It was discussed that we could then present the information to the City Council at a work session on either November $5^{\text {th }}$ or $19^{\text {th }}$.


## 3. INTERCHANGE EVALUATION MATRIX

A. Review Updated Evaluation Matrix

An updated evaluation matrix was reviewed and there were no significant comments. Members of the TAC provided input on their preferences among the options. Considering all factors (with costs being important) a majority of the TAC preferred Option 1 with some interest in adding the railroad grade separation (Option 1A) if additional funding can be obtained for the railroad bridge. There was also some support for Option 3 due to concerns associated with the routing of all northbound TH 169 traffic to Creek Lane and business visibility.

## 4. PROJECT SCHEDULE

5. NEXT STEPS
A. City Council Update on October $1^{\text {st }}$

It was discussed that the City Council update would be delayed until after the October $29^{\text {th }}$ open house meeting.
B. Refine Locally Preferred Concept
C. Prepare Corridor Study Report
D. Develop Implementation and Funding Plan

## 6. QUESTIONS/OTHER DISCUSSION

APPENDIX C - PUBLIC OPEN HOUSE MATERIALS

Scott

## Scope of Study

- Traffic Analysis
- Interchange Alternative Concept Development and Evaluation
- Cost Estimates and Implementation Plan
- Determine Locally Preferred Interchange Concept
- Schedule May - December 2018



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 Kimley＂）HornEXISTING INTERSECTION CONTROL AND GEOMETRY TH 169 ／TH 282 ／CR 9
INTERCHANGE CONCEPT DESIGN

CRASH RATES（2011－2015） INTERCHANGE CONCEPT DESIGN



NO-ACTION LOS
INTERCHANGE CONCEPT DESIGN


CONCEPT 1 - LOS INTERCHANGE CONCEPT DESIGN



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| Alternative | Screening Criteria |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Trafic Operations |  |  | Rooaway Design |  |  |  |  |  |  |  | Environmental Considerations |  |  | Right-of.Way |  |  |  | Estimated Cost (1) <br> Total Project $\operatorname{cost}($ (s) |
|  | Minimize Impacts to Business Access | $\begin{aligned} & \text { Improves TH } 169 \\ & \text { Operations } \end{aligned}$ | Improves Safety | $\begin{array}{\|c} \text { Flexibility for } \\ \text { Phased } \\ \text { Implementation } \end{array}$ | $\begin{gathered} \text { Construction } \\ \text { Staging Flexibility } \end{gathered}$ | $\begin{gathered} \text { Minimize Impacts } \\ \text { to TH } 169 \\ \text { Alignment } \end{gathered}$ | $\begin{array}{\|c\|} \hline \begin{array}{c} \text { Meets MDDO and } \\ \text { Sounty } \\ \text { Spaceang Guidelines } \end{array} \\ \text { Spo } \end{array}$ | $\begin{aligned} & \text { Improves Railroad } \\ & \text { Crossing Safety } \end{aligned}$ | Safe Sidewalk/Trail Connection across TH 169 | Senes Freight | Reasonable to Maintain | Wetand Impats | Floodplain Impats | Valley Green Neighborhood Impacts | Impacted Area (Acres) | Number of Total Takes | $\begin{gathered} \text { Peviure } \\ \substack{\text { Devoment } \\ \text { potetantala }} \end{gathered}$ | $\begin{array}{\|c\|} \text { Business } \\ \text { Visibility/Property } \\ \text { Impacts } \end{array}$ |  |
| No Build |  |  |  | N/A | N/A | N/A |  |  |  |  |  |  | O |  |  |  |  | 0 |  |
| Concept 1-Roundabout/Split Diamond |  |  |  | O |  | O |  |  |  |  |  |  |  |  |  |  |  | $\bigcirc$ |  |
| Concept 1A - Roundabout/Split Diamond, RR Overpass |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Concept 2 - Folded Diamond/ Split Diamond |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | ) | ) |  |
| Concept 3-TH 169 Over TH 282/ CR9 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Concept 3A - TH 169 Over TH 282/ CR 9, Bridge over Creek Lane |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | ) |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  | 4.1 acres |  |  |  | 3 |  |  | st0M |

LEGEND

## Kimley»Horn

## MEM ORANDUM

To: Tom Nikunen, ICM A-CM<br>City Administrator<br>City of Jordan<br>Tony Winiecki, P.E.<br>County Engineer<br>Scott County Highway Department<br>Jon Solberg<br>South Area M anager<br>Minnesota Department of Transportation

From: Brandon Bourdon, P.E.
Kimley-Horn and Associates, Inc

Date: November 28, 2018
Re: TH 169 / TH 282 / CR 9 Interchange
Forecasting, Safety and Operations Analysis

## Introduction

Kimley-Horn has been hired by the City of Jordan, as part of a joint project between the City, Scott County and MnDOT, to provide traffic engineering, concept design, and stakeholder engagement services for the TH 169 / TH 282 / CR 9 interchange area. As part of the traffic engineering services, an operations analysis was performed at critical intersections within the study area to support interchange concept development and determine the most appropriate intersection control and geometry to accommodate existing and future traffic.

This memorandum provides a summary of historic crash data along the study corridor, intersection capacity analysis for Existing and Design Year conditions, and a discussion on potential roadway and intersection improvement alternatives.

## Existing Conditions Analysis

The traffic study was centered around potential interchange improvements at TH 169 / CR 9 / TH 282. From that intersection, the study area extended north on CR 9 to $190^{\text {th }}$ Street West/Valley View Drive and south on TH 282 to Creek Lane North. The study area also included the section of TH 169 from TH 282 to Creek Lane, Creek Lane North from TH 169 to TH 282 and Triangle Lane North from TH 282 to Creek Lane. The following provides a description of the roadways that were included within the study area:

- TH 169 is a northeast-southwest roadway that runs through the northwest edge of Scott County just south of the M innesota River. Within the study area, TH 169 is four-lane divided roadway and has a posted speed limit of 55 mph . TH 169 is classified as a Principal Arterial by MnDOT.
- CR 9 is a north-south roadway that runs between the County Line (to the north where it changes to Carver County Road 11) to TH 169 (to the south where it becomes TH 282), and is one of the only major north-south roadways in the area that offers a river crossing over the M innesota River. CR 9 is a two-lane undivided roadway between the M innesota River and $9^{\text {th }}$ Street; a four-lane undivided roadway between $9^{\text {th }}$ Street and Frontage Road; and a four-lane divided roadway just north of the Frontage Road to TH 169. The roadway has a posted speed limit of 50 mph between the Minnesota River and Jennifer Lane (the north intersection) and 40 mph between Jennifer Lane and TH 169. CR 9 is classified as a M inor Arterial by Scott County.
- TH 282 is an east-west roadway that connects TH 169 (to the west) to TH 21 (Broadway Street). Within the study area, TH 282 is four-lane divided near TH 169 and two-lane undivided east of Triangle Lane. The roadway has a posted speed limit of 30 mph and is classified as a M inor Arterial.
- 190h Street West/ Valley View Drive is a northeast-southwest roadway that connects $173{ }^{\text {rd }}$ Street W (to the northeast) to TH 169 (to the southwest) between the Minnesota River (to the north) and TH 169 (to the south). The roadway is two-lane undivided with a posted speed limit of 30 mph east of CR 9 and 45 mph west of CR 9 .
- Triangle Lane North is a short local road that runs parallel to TH 169 that connects Creek Lane (to the east) to TH 282 (to the west).
- Creek Lane North is a local roadway that connects to TH 169 (to the north) and Sunset Drive (to the south). The roadway is two-lane undivided with a posted speed limit of 30 mph . This roadway is one of the primary roads used to reach Jordan Elementary, Middle, and High Schools.
- Frontage Road is a local roadway that runs parallel to TH 169 and to the east of CR 9 that connects Syndicate Street (to the east) to CR 9 (to the west). The roadway is two-lane undivided with a posted speed limit of 30 mph . This roadway is the primary access to the Jordan Police Department.
- CR 9 Railroad Crossing is an at-grade railroad crossing located between TH 169 and 190 ${ }^{\text {th }}$ Street West/Valley View Drive along CR 9. Based on a review of MnDOT's Twin Cities Area Freight Railroad Map, this railroad is operated by Union Pacific. It has a maximum operating speed of 49 MPH and there are six trains per day at this crossing. The actual rail-crossing train volume was counted on May 16, 2018 and there were four trains that crossed CR 9 during a 24-hour period. The duration of the train crossings were between 1:15 and 2:15 minutes and traffic queues on CR 9 dissipated within 45 seconds after the gate arms raised.


## Kimley»Horn

Exhibit 1 provides the existing lane geometry and intersection control for the study area. The study intersections included the following:

- CR $9 \& 190^{\text {th }}$ Street West/Valley View Drive
- CR 9 \& Frontage Road
- TH 169 / CR 9 / TH 282
- TH 169 \& Creek Lane North
- TH 282 \& Triangle Lane North
- TH 282 \& Business Access
- TH 282 \& Creek Lane North
- Triangle Lane North \& Creek Lane North


## Existing Traffic Volumes

Intersection traffic count data for most the intersections was provided to Kimley-Horn by the City of Jordan because they were collected recently (November 2016). New traffic counts were collected at the intersections of TH 169 \& Creek Lane North, Triangle Lane North \& Creek Lane North, and TH 282 \& Business Access (May 2018). Daily roadway volumes, reported as Average Annual Daily Traffic (AADT), was provided by the M innesota Department of Transportation’s Traffic M apping Application.

Exhibit 2 provides a summary of the roadway AADT information as well as the AM and PM peak hour turning movement volumes.


EXHIBIT 1


EXHIBIT 2

## ExistingIntersection Operations

An intersection capacity analysis was performed at the study intersections using the weekday AM and PM peak hour turning movement volumes that were provided in Exhibit 2 The capacity analysis was performed using Synchro/SimTraffic software to determine the baseline Level of Service (LOS), delay, and queueing at the study intersections.

The LOS boundaries, as documented in the Highway Capadity Manual for signalized and unsignalized intersections, are shown in Table 1 For this study, LOS A through LOS D are considered to be acceptable levels of operation for both signalized and unsignalized intersections.

Table 1: Level of Service Boundaries

| Level of Service | Average Control Delay per Vehicle (sec/veh) |  | Description |
| :---: | :---: | :---: | :---: |
|  | Signalized | Unsignalized |  |
| $A$ and $B$ | $\begin{gathered} \leq 10(\mathrm{~A}) \\ >10 \text { and } \leq 20 \end{gathered}$ <br> (B) | $\begin{gathered} \leq 10(\mathrm{~A}) \\ >10 \text { and } \leq 15(\mathrm{~B}) \end{gathered}$ | No delays at intersections with continuous flow traffic. Uncongested operations; high frequency of long gaps available for all left and right-turning traffic; no observable queues. |
| C | $>20$ and $\leq 35$ | $>15$ and $\leq 25$ | Moderate delays at intersections with satisfactory to good traffic flow. Light congestion; infrequent backups on critical approaches. |
| D | $>35$ and $\leq 55$ | $>25$ and $\leq 35$ | Increased probability of delays along every approach. Significant congestion on critical approaches, but intersection functional. No long standing lines formed. |
| E | $>55$ and $\leq 80$ | $>35$ and $\leq 50$ | Heavy traffic flow condition. Heavy delays probable. No available gaps for cross-street traffic or main street turning traffic. Limit of stable flow. |
| F | $>80$ | $>50$ | Unstable traffic flow. Heavy congestion. Traffic moves in forced flow condition. Average delays greater than one minute highly probable. Total breakdown. |

Table 2 provides a summary of the delay (seconds per vehicle) and LOS for each individual movement of the study intersections. The LOS information is also summarized by movement in Exhibit 3. Based on the Existing Conditions (2017) capacity analysis, all intersections are currently operating at an acceptable LOS during the weekday AM and PM peak hours. Additionally, all individual movements are operating at LOS D or better for both the AM and PM peak hours except for the eastbound and westbound lefts at TH 169 and TH 282, which are operating at LOS E during the AM and PM peak hours. Although TH 282 and Creek Lane operate at acceptable LOS during the peak hour, there are periods of congestion and complaints regarding traffic at this intersection in part due to traffic traveling to and from the Jordan schools. The SimTraffic reports are included in the Appendix

Kimley»Horn
Table 2: Existing Year (2017) Peak Hour Delay and Level of Service Results

| Intersection |  |  | AM PEAK HOUR |  |  |  |  |  |  |  | PM PEAK HOUR |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Left |  | Through |  | Right |  | Overall |  | Left |  | Through |  | Right |  | Overall |  |
|  |  |  | $\stackrel{\text { ® }}{\stackrel{\omega}{0}}$ | $0$ | $\stackrel{\pi}{\frac{\pi}{8}}$ | $0$ | $\stackrel{\text { 会 }}{2}$ | n | $\frac{\widetilde{0}}{\stackrel{\sigma}{0}}$ | $0$ | $\frac{\sigma}{\stackrel{\sigma}{0}}$ | $0$ | $\frac{\pi}{0}$ | $\stackrel{\sim}{0}$ | $\underset{\sim}{\mathbb{O}}$ | $0$ | $\stackrel{\text { ® }}{\circ}$ | 0 <br> 0 |
| CR 9 (Quaker Avenue) \& 190th Street W/Valley View Drive | StopControlled | EB Approach | 9.3 | A | 12.1 | B | 4.2 | A | 2.3 | A | 8.7 | A | 13.6 | B | 4.9 | A | 2.3 | A |
|  |  | WB Approach | 8.9 | A | 11.2 | B | 3.9 | A |  |  | 11.3 | B | 12.3 | B | 6.5 | A |  |  |
|  |  | NB Approach | 3.6 | A | 1.3 | A | 1.6 | A |  |  | 6.7 | A | 1.3 | A | 1.1 | A |  |  |
|  |  | SB Approach | 1.2 | A | 0.4 | A | 0.2 | A |  |  | 1.6 | A | 0.6 | A | 0.3 | A |  |  |
| CR 9 (Quaker Avenue) \& Frontage Rd | Stop <br> Controlled | WB Approach | 10.8 | B | - | - | 4.7 | A | 2.4 | A | 22.6 | C | - | - | 4.2 | A | 5.4 | A |
|  |  | NB Approach | - | - | 1.8 | A | 1.5 | A |  |  | - | - | 1.7 | A | 1.7 | A |  |  |
|  |  | SB Approach | 2.8 | A | 1.3 | A | - | - |  |  | 3.5 | A | 6.4 | A | - | - |  |  |
| TH 169 \& CR 9 (Quaker Avenue)/TH 282 (2nd Street W) | Signalized | EB Approach | 58.9 | E | 27.0 | C | 6.4 | A | 30.2 | C | 73.1 | E | 38.6 | D | 7.8 | A | 34.7 | C |
|  |  | WB Approach | 57.7 | E | 28.9 | C | 3.1 | A |  |  | 64.4 | E | 34.0 | C | 4.4 | A |  |  |
|  |  | NB Approach | 26.0 | C | 33.7 | C | 22.0 | C |  |  | 34.5 | C | 29.4 | C | 15.7 | B |  |  |
|  |  | SB Approach | 29.1 | C | 39.5 | D | 25.2 | C |  |  | 27.7 | C | 44.3 | D | 32.9 | C |  |  |
| TH 282 (2nd Street W) \& Triangle Lane N | Stop <br> Controlled | EB Approach | 6.8 | A | 2.9 | A | 1.9 | A | 3.5 | A | 9.4 | A | 4.6 | A | 2.4 | A | 5.0 | A |
|  |  | WB Approach | 4.4 | A | 0.4 | A | 0.4 | A |  |  | 4.5 | A | 0.6 | A | 0.5 | A |  |  |
|  |  | NB Approach | 17.9 | C | 17.9 | C | 3.2 | A |  |  | 16.1 | C | 24.2 | C | 8.3 | A |  |  |
|  |  | SB Approach | 17.3 | C | 17.0 | C | 8.6 | A |  |  | 24.3 | C | 22.1 | C | 13.8 | B |  |  |
| TH 282 (2nd Street W) \& Business Access | Stop <br> Controlled | EB Approach | - | - | 0.7 | A | 0.6 | A | 1.0 | A | - | - | 1.2 | A | 0.6 | A | 2.1 | A |
|  |  | WB Approach | 3.7 | A | 0.6 | A | - | - |  |  | 7.2 | A | 0.6 | A | - | - |  |  |
|  |  | NB Approach | 10.8 | B | - | - | 3.5 | A |  |  | 19.1 | C | - | - | 4.2 | A |  |  |
| TH 282 (2nd Street W) \& Creek Lane | Stop <br> Controlled | EB Approach | 2.9 | A | 0.4 | A | 2.6 | A | 3.7 | A | 3.3 | A | 0.7 | A | 2.4 | A | 3.5 | A |
|  |  | WB Approach | 2.8 | A | 0.6 | A | 0.2 | A |  |  | 4.8 | A | 0.7 | A | 0.2 | A |  |  |
|  |  | NB Approach | 12.7 | B | 11.2 | B | 1.7 | A |  |  | 20.4 | C | 13.5 | B | 1.7 | A |  |  |
|  |  | SB Approach | 9.5 | A | 10.3 | B | 5.6 | A |  |  | 14.9 | B | 16.4 | C | 5.5 | A |  |  |
| Creek Ln N \& Triangle Lane N | Stop <br> Controlled | EB Approach | 6.7 | A | 6.2 | A | 4.7 | A | 3.1 | A | 5.0 | A | 6.5 | A | 2.9 | A | 2.2 | A |
|  |  | WB Approach | 3.4 | A | 4.4 | A | 5.0 | A |  |  | 3.9 | A | 4.8 | A | 2.5 | A |  |  |
|  |  | NB Approach | 1.9 | A | 1.0 | A | 0.3 | A |  |  | 2.0 | A | 0.5 | A | 0.2 | A |  |  |
|  |  | SB Approach | 1.2 | A | 0.1 | A | 0.1 | A |  |  | 1.0 | A | 0.2 | A | 0.1 | A |  |  |
| TH 169 \& Creek In N | Stop | WB Approach | - | - | - | - | - | - |  |  | - | - | - | - | - | - |  |  |
| TH 169 \& Creek LnN | Controlled | NB Approach | - | - | - | - | 15.5 | C | 8.4 | A | - | - | - | - | 7.9 | A | 4.6 | A |



EXHIBIT 3

In addition to intersection LOS and delay, the existing turn lane queue lengths were reviewed based on the SimTraffic analysis. Table 3 provides the existing $95^{\text {th }}$ percentile queue lengths for turning movements at the study intersection turn lanes for both the AM and PM peak hours. The existing storage lengths were based on a review of aerial photography. Based on the review of the $95^{\text {th }}$ percentile queues, the existing turn lanes are anticipated to accommodate the queues except for the northbound left-turn at the intersections of TH 169 / CR 9 / TH 282 and TH $282 \&$ Creek Lane North. The existing southbound through queue at the intersection of TH 169 / CR 9 / TH 282 extends through the intersection of CR 9 \& Frontage Road during the PM peak hour. In addition, the southbound approach at TH 282 \& Triangle Lane North and northbound right and left-turn lanes at TH 282 \& Business Access have queue lengths that extend beyond the southern Holiday and McDonald's access points and into the existing Radermacher's parking lot, respectively.

Table 3: Existing Year (2017) 95 ${ }^{\text {th }}$ Percentile Queue Summary

| Intersection | Lane | Storage <br> Length (it) | AM Peak | PM Peak |
| :---: | :---: | :---: | :---: | :---: |
| CR 9 (Quaker Avenue) \& 190th Street W/Valley View Drive | EB | $>500$ | 72 | 60 |
|  | WB | $>500$ | 49 | 58 |
|  | NB Left | $>500$ | 33 | 79 |
|  | SB Left | $>500$ | 5 | 8 |
| TH 169 \& CR 9 (Quaker Avenue)/TH 282 (2nd Street W) | EB Left | 260 | 162 | 70 |
|  | EB Right | 300 | 66 | 74 |
|  | WB Left | 550 | 94 | 165 |
|  | WB Right | 350 | 31 | 51 |
|  | NB Left | 90 | 115 | 199 |
|  | SB Left | 125 | 88 | 90 |
| TH 282 (2nd StreetW) \& Triangle Lane $N$ | WB Left | 150 | 15 | 11 |
|  | WB Right | 85 | 11 | 9 |
|  | NB | 55 | 36 | 35 |
|  | SB | 65 | 94 | 123 |
| TH 282 (2nd StreetW) \& Business Access | WB Left | 100 | 28 | 57 |
|  | NB Left | 40 | 42 | 60 |
|  | NB Right | 40 | 35 | 53 |
| TH 282 (2nd Street W) \& Creek Lane | EB Left | 100 | 12 | 9 |
|  | EB Right | 300 | 80 | 55 |
|  | WB Left | 200 | 46 | 60 |
|  | NB Left | 85 | 87 | 96 |
|  | NB Right | 85 | 0 | 24 |
|  | SB Left | 85 | 35 | 41 |
| TH 169 \& Creek Ln N | NB Right | 120 | 114 | 43 |
| Queue lengths are the 95th Percentile Queue as calculated in SimTraffic. |  |  |  |  |

## Crash Analysis

Historical crash data was obtained for the previous five (5) year period (2011-2015) using M nDOT's Crash M apping Analysis Tool (MnCM AT). A review of the crash data showed that there was a total of 100 crashes at study intersections. Of the 100 crashes, there were 2 fatalities, 0 incapacitating injuries, 4 nonincapacitating injuries, 19 possible injuries, and 75 property damage only crashes.

Table 4 provides a summary of the intersection crash analysis, and includes the number and type of crashes, observed crash rate, statewide average and critical crash rates, and the critical index. Crash rates
provide an indication of the number of crashes that can be expected per entering vehicle over a given analysis period. Using MnDOT's 2015 "Green Sheets," intersection crash rates were calculated and compared against statewide average values to develop a critical index value. This value is used to determine if an intersection is operating outside of the expected normal range, where a critical index value over 1.0 means the intersection is outside of the normal range.

The review of the crash analysis shows that the intersections of TH 169 / CR 9 / TH 282 and TH 282 \& Triangle Lane North have a critical index of greater than 1.0, meaning that these two intersections are operating outside of the normal, expected range (i.e. there is a crash issue at these intersections today). At the intersection of TH 169 / CR 9 / TH 282, the most common crash type was rear-end collisions (39 total over the five-year period). A fatal crash also occurred at TH 169 / CR 9 / TH 282. The most common crash types at the intersection of TH 282 \& Triangle Lane North were rear-end crashes (5) and sideswipe crashes (3). The crash data indicates that two contributing factors are having a traffic signal on a highspeed, high-volume facility (TH 169) and the queuing from this signal and the associated impacts due to the inadequate intersection spacing between Triangle Lane $N$ and TH 169. The number of crashes, crash rate, critical crash rate, and critical index information is summarized in Exhibit 4.

Table 4: Crash Summary

| Intersection | Total Number of Crashes | Crash Type |  |  |  |  | Observed Crash Rate | Statewide Average | Critical Crash Rate | Critical Index |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | PD | C | B | A | K |  |  |  |  |
| CR 9 (Quaker Avenue) \& 190 ${ }^{\text {th }}$ Street West/Valley View Drive | 3 | 2 | 0 | 0 | 0 | 1 | 0.20 | 0.25 | 0.62 | 0.32 |
| CR 9 (Quaker Avenue) \& Frontage Road | 2 | 0 | 1 | 1 | 0 | 0 | 0.13 | 0.25 | 0.62 | 0.21 |
| TH 169 <br> \& CR 9 (Quaker Avenue)/ TH 282 (2nd Street West) | 62 | 47 | 13 | 1 | 0 | 1 | 1.11 | 0.45 | 0.69 | 1.61 |
| TH 282 (2nd Street West) \& Triangle Lane | 15 | 12 | 2 | 1 | 0 | 0 | 0.76 | 0.25 | 0.57 | 1.33 |
| TH 282 (2 ${ }^{\text {nd }}$ Street West) \& Creek Lane North | 8 | 6 | 2 | 0 | 0 | 0 | 0.33 | 0.25 | 0.54 | 0.61 |
| TH 169 \& Creek Lane North | 10 | 8 | 1 | 1 | 0 | 0 | 0.25 | 0.25 | 0.47 | 0.53 |



EXHIBIT 4

## Design Year (2040) No-Action Intersection Analysis

A capacity analysis was performed at the study intersections for the Design Year (2040) to get an idea of operating conditions along the corridor in the future and use that information to determine necessary roadway and intersection improvements to provide acceptable LOSthrough the Design Year (2040). Below is a summary of the Design Year (2040) volume development and anticipated operating conditions during the AM and PM peak hours at the study intersections.

## Design Year (2040) Volume Forecast

Existing turning movement volumes and AADTs identified previously along with prior planning efforts were used to development Design Year (2040) traffic forecasts. There were two sets of future ADT forecasts available that were used including:

- 2040 Scott County Transportation Plan Update
- $190^{\text {th }}$ Street \& CSAH 9 Traffic Study

The Scott County traffic forecasts were developed as a part of the regional planning process that begins with M etropolitan Council growth projections and requires a travel demand model update based on the Metropolitan Council projections. There was also forecasting completed by the City of Jordan that considered the full development potential of three land use scenarios on the north side of TH 169 as documented in the $190^{\text {th }}$ Street \& CSAH 9 Traffic Study, completed in 2017, which involved growth anticipated by the City beyond the M etropolitan Council forecasts. The concern by the City was that very little growth was assumed on the north side of TH 169 as a part of the M etropolitan Council forecasts. Scott County and MnDOT had concerns that concepts may be overdesigned if the forecasts were too aggressive and deviated significantly from the comprehensive planning process. There was dialog between the parties and the following process was used to develop the 2040 traffic forecasts:

- One-half of the ultimate development potential north of TH 169 as documented in the $190^{\text {th }}$ Street \& CSAH 9 Traffic Study is to occur by 2040. The traffic generated east of Fairview Lane will generally travel to CR 9 to get to the regional roadway network. Conversely, traffic generated west of Fairview Lane will travel to Delaware Avenue to gain access to the regional roadway network.
- We assumed that background growth on $190^{\text {th }}$ Street West shown in the 2040 Scott County Forecasts was due to development assumed in the $190^{\text {th }}$ Street \& CR 9 Traffic Study (i.e. some of the growth in the study did get included in the forecasts previously presented).
- We assumed that land uses with seasonal events will be handled through event traffic management plans rather than designing the transportation system to accommodate these events (Renaissance Festival, Scott-Carver Threshers, Scott County Fairgrounds). Therefore, we did not include those event trips in the forecasts.
- This resulted in the 2040 Scott County Plan ADTs being adjusted to include an additional 9,500 trips that were distributed onto the roadway network ( $1 / 2$ of 22,000 minus 1,500 that was already accounted for in the Scott County model).
The forecasts developed as a part of this study along with the existing AADTs and Scott County 2040 and $190^{\text {th }}$ Street Growth Area full build forecasts are shown on Exhibit 5.

The developed 2040 ADT forecasts, existing traffic counts, and future forecasts documented in the 190th Street \& CR 9 Traffic Study were all used in combination to develop 2040 turning movement counts shown in Exhibit 6.

## Design Year (2040) No-Action Intersection Capacity Analysis

Using the forecasted Design Year (2040) AM and PM peak hour turning movement volumes, a capacity analysis was performed at the study intersections to determine baseline operating conditions in 2040. Existing intersection control and geometries were assumed for this No-Action analysis, except for the intersections of CR 9 \& 190 ${ }^{\text {th }}$ Street West/Valley View Drive and TH 282 \& Creek Lane North, where traffic signal control was assumed.

Table 5 provides a summary of the delay (seconds/vehicle) and LOS at the study intersections. Exhibit 7 also provides a summary of the delay and LOS for each individual movement at the study intersections. Based on the analysis, there are a significant number of intersections that are anticipated to operate at overall LOS E or LOS F during the AM and PM peak hours. These intersections include the following:

- CR 9 \& 190 ${ }^{\text {th }}$ Street West/Valley View Drive (PM peak hour)
- CR 9 \& Frontage Road (AM and PM peak hours)
- TH 169 / CR 9 / TH 282 (PM peak hour)
- TH 282 \& Triangle Lane North (PM peak hour)
- Creek Lane North \& Triangle Lane North (AM peak hour)
- TH 169 \& Creek Lane North (PM peak hour)

Due to a significant number of intersection that are anticipated to operate below the acceptable LOS for Design Year (2040) No-Action conditions, improvements along the study corridor will be necessary to provide acceptable LOS into the future. The continued deterioration of LOS between today and future conditions is anticipated to result in additional crash concerns along the corridor.


EXHIBIT 5


Kimley»Horn
Table 5: Design Year (2040) No-Action Capacity Analysis Summary

| Intersection |  |  | AM PEAK HOUR |  |  |  |  |  |  |  | PM PEAK HOUR |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Let |  | Through |  | Right |  | Overall |  | Left |  | Through |  | Right |  | Overall |  |
|  |  |  | $\frac{\widetilde{\circ}}{\stackrel{\sigma}{\circ}}$ | $0$ | $\frac{\widetilde{\circ}}{\stackrel{\sigma}{0}}$ | $\begin{aligned} & \infty \\ & 0 \end{aligned}$ | $\stackrel{\text { ® }}{\stackrel{\sigma}{0}}$ | $0$ | $\stackrel{\text { ® }}{\stackrel{\sigma}{\mathrm{O}}}$ | $0$ | $\frac{\text { ® }}{\stackrel{\circ}{\circ}}$ | $0$ | $\frac{\text { ® }}{\stackrel{\sigma}{0}}$ | 0 | $\frac{\text { ® }}{\stackrel{\sigma}{0}}$ | on | $\stackrel{\text { ® }}{\text { ® }}$ | $0$ |
| CR 9 (Quaker Avenue) \& 190th Street W/Valley View Drive | Signalized | EB Approach | 56.6 | E | 59.3 | E | 44.9 | D | 31.2 | C | * | F | * | F | * | F | 91.4 | F |
|  |  | WB Approach | 39.8 | D | 39.5 | D | 32.4 | C |  |  | 54.5 | D | 50.6 | D | 35.7 | D |  |  |
|  |  | NB Approach | 36.3 | D | 23.3 | C | 17.2 | B |  |  | 84.6 | F | 14.9 | B | 14.5 | B |  |  |
|  |  | SB Approach | 44.6 | D | 23.6 | C | 6.1 | A |  |  | * | F | * | F | * | F |  |  |
| CR 9 (Quaker Avenue) \& Frontage Rd | Stop <br> Controlled | WB Approach | * | F | - | - | * | F | 94.9 | F | * | F | - | - | * | F | * | F |
|  |  | NB Approach | - | - | 1.9 | A | 2.0 | A |  |  | - | - | 1.8 | A | 1.9 | A |  |  |
|  |  | SB Approach | 42.3 | E | 60.0 | F | - | - |  |  | * | F | * | F | - | - |  |  |
| TH 169 \& CR 9 (Quaker Avenue)/TH 282 (2nd Street W) | Signalized | EB Approach | 75.3 | E | 58.8 | E | 21.8 | C | 52.0 | D | * | F | 60.4 | E | 26.7 | C | 87.1 | F |
|  |  | WB Approach | 77.5 | E | 43.9 | D | 8.9 | A |  |  | * | F | * | F | 62.4 | E |  |  |
|  |  | NB Approach | 58.7 | E | 41.0 | D | 40.5 | D |  |  | * | F | 46.1 | D | 42.1 | D |  |  |
|  |  | SB Approach | 60.4 | E | 72.2 | E | 57.2 | E |  |  | 55.8 | E | 65.5 | E | 50.3 | D |  |  |
| TH 282 (2nd Street W) \& Triangle Lane N | Stop Controlled | EB Approach | 28.9 | D | 13.1 | B | 5.7 | A | 32.2 | D | 40.0 | E | 20.1 | C | 7.3 | A | 57.4 | F |
|  |  | WB Approach | 10.5 | B | 1.5 | A | 1.0 | A |  |  | 20.5 | C | 31.3 | D | 14.7 | B |  |  |
|  |  | NB Approach | * | F | * | F | 93.9 | F |  |  | * | F | * | F | * | F |  |  |
|  |  | SB Approach | * | F | * | F | * | F |  |  | * | F | * | F | * | F |  |  |
| TH 282 (2nd Street W) \& Business Access | Stop <br> Controlled | EB Approach | - | - | 4.7 | A | 0.8 | A | 4.8 | A | - | - | 5.9 | A | 0.7 | A | 30.5 | D |
|  |  | WB Approach | 12.0 | B | 2.1 | A | - | - |  |  | 26.2 | D | 18.3 | C | - | - |  |  |
|  |  | NB Approach | 56.1 | F | - | - | 15.4 | C |  |  | * | F | - | - | 52.6 | F |  |  |
| TH 282 (2nd Street W) \& Creek Lane | Signalized | EB Approach | 52.3 | D | 19.6 | B | 2.1 | A | 22.7 | C | 94.2 | F | 16.1 | B | 2.0 | A | 40.9 | D |
|  |  | WB Approach | 50.4 | D | 23.3 | C | 17.4 | B |  |  | 59.8 | E | 40.9 | D | 35.5 | D |  |  |
|  |  | NB Approach | 34.3 | C | 25.7 | C | 2.3 | A |  |  | * | F | 79.0 | E | 39.9 | D |  |  |
|  |  | SB Approach | 22.8 | C | 27.0 | C | 17.7 | B |  |  | 39.8 | D | 59.1 | E | 51.3 | D |  |  |
| Creek Ln N \& Triangle Lane N | Stop <br> Controlled | EB Approach | * | F | * | F | * | F | * | F | 5.3 | A | 6.0 | A | 2.9 | A | 2.3 | A |
|  |  | WB Approach | 35.8 | E | 86.2 | F | * | F |  |  | 3.0 | A | 4.9 | A | 2.2 | A |  |  |
|  |  | NB Approach | 74.4 | F | 94.5 | F | 85.0 | F |  |  | 1.9 | A | 0.7 | A | 0.3 | A |  |  |
|  |  | SB Approach | 1.1 | A | 0.1 | A | 0.1 | A |  |  | 0.9 | A | 0.2 | A | 0.1 | A |  |  |
| TH 160 \& Croek Ln N | Stop | WB Approach | - | - | 0.9 | A | - | - |  |  | - | - | 67.0 | F | - | - |  |  |
| TH 169 \& Creek Ln N | Controlled | NB Approach | - | - | - | - | 91.6 | F | 16.0 | C | - | - | - | - | 17.0 | C | 47.4 | E |



EXHIBIT 7

## Design Year (2040) Roadway and Intersection Conditions

To improve operating conditions along the corridor, improve safety, and provide sufficient capacity for future growth in traffic volumes, several interchange, roadway and intersection improvements were considered within the project study area. Several concepts were considered through the planning process, and based on input from the City, County and MnDOT three (3) preferred concepts were considered for further review and consideration as part of the traffic analysis. The following section provides a description of each of the three (3) preferred concepts.

## Concept 1

With Concept 1, CR 9 / TH 282 is proposed to be reconstructed as a four-lane divided roadway from 190 ${ }^{\text {th }}$ Street West/Valley View Drive to Creek Lane North. In conjunction with the widening, a split diamond interchange is proposed at the intersection of TH 169 / CR 9 / TH 282. The following provides a description of proposed improvements at the study intersections in the project's study area:

- CR 9 \& 190 ${ }^{\text {th }}$ Street West/Valley View Drive - The intersection is proposed to be expanded to provide three (3) lanes (one through lane and dedicated left and right-turn lanes) for the northbound, eastbound and westbound approaches and four (4) lanes (two through lanes and dedicated left and right-turn lanes) for the southbound approach. The intersection is proposed to be signal controlled. Although additional analysis would be required, a roundabout could also be considered at this intersection.
- CR 9 \& TH 169 Westbound Ramps - The intersection is proposed to be a five-legged intersection and serve the existing frontage road traffic in addition to the TH 169 westbound ramps. The northbound and southbound approaches will provide two (2) lanes (shared through-left and shared through-right). The westbound off-ramp approach will provide two (2) lanes (shared left-through-right and shared right/u-turn). The frontage road approach will provide one (1) shared lane. The intersection is proposed to be a roundabout.
- TH 282 \& TH 169 Eastbound Ramps - The intersection is proposed to be a three-legged intersection to serve the TH 169 eastbound off-ramp. The northbound and southbound approaches will provide two (2) through lanes, and the eastbound approach will provide two (2) lanes (dedicated left and right-turn lanes). The intersection is proposed to be signal controlled.
- TH 282 \& Triangle Lane North - Due to existing crash concerns and access spacing requirements, the intersection is proposed to be a three-legged intersection that serves TH 282 and Triangle Lane North. The Wolf Motors access to the south is proposed to be combined with the Radermacher's access located to the east. Access for Triangle Lane North will be restricted to right-in and right-out. The westbound approach will provide three (3) lanes (two through lanes and dedicated right-turn lane) and the eastbound approach will provide two (2) through lanes. The southbound approach will provide a single right-turn lane. The intersection is proposed to be side-street stop controlled.
- TH 282 \& Business Access - The intersection is proposed to be a three-legged three-quarter movement intersection that serves TH 282 and businesses along the south side of TH 282. Access for eastbound movements to/from the business access will be restricted to right-in and right-out
movements only. The westbound approach will provide three (3) lanes (two through lanes and dedicated left-turn lane) and the eastbound approach will provide three (3) lanes (two through lanes and dedicated right-turn lane). The northbound approach will provide a single right-turn lane. The intersection is proposed to be side-street stop controlled.
- TH 282 \& Creek Lane North - The intersection is proposed to be improved to provide two (2) lanes for the westbound and three (3) lanes for the eastbound approaches, with the westbound approach having a shared through-left and shared through-right lane and the eastbound approach having a dedicated left-turn, through and right-turn lane. Both the northbound and southbound approaches will provide one (1) shared lane. The intersection is proposed to be a roundabout. The roundabout will provide improved access for travelers accessing the local businesses due to the access restrictions at TH 282 \& Triangle Lane North and TH 282 \& Business access intersections.

The concept shows the roundabout configuration that would be required if the 2040 traffic forecasts materialize. MnDOT has stated this roundabout will need to be phased so that the initial roundabout is not oversized opening day. This will require that an interim configuration be constructed for both the initial roundabout and potentially adjacent segments of TH 282. The ultimate interim configuration required at and adjacent to this intersection will need to be determined considering both interim traffic operations and construction phasing impacts.

- Creek Lane North \& Triangle Lane North - The intersection is proposed to provide direct access to TH 169 eastbound. The northbound approach will provide two (2) lanes with a dedicated leftturn and shared through-right lane. The eastbound approach will provide two (2) lanes with a dedicated left-turn lane and a shared through-right lane. The westbound approach will provide a one (1) lane approach. The intersection is proposed to be side-street stop controlled.

Exhibit 8 provides the proposed roadway layout as well as intersection control and geometry for Concept 1.

Using the Design Year (2040) No-Action turning movement volumes as a base, traffic volumes were developed for Concept 1 to take into consideration the change in access at the study intersections. The following provides more detail about the traffic volume adjustments that were made:

- Traffic traveling eastbound on TH 169 from CR 9 and TH 282 (i.e. northbound right-turn and southbound left-turn movements at the intersection of TH 169 / CR 9 / TH 282) were redistributed to Creek Lane North.
- Traffic traveling to/from Wolf Motors that access TH 282 (northbound approach) at the intersection of TH 282 \& Triangle Lane North were redistributed to the TH 282 and Business Access.
- Traffic traveling southbound on TH 282 from Triangle Lane North (southbound left-turn movement) were redistributed to Creek Lane North.

Exhibit 9 provides the Design Year (2040) AM and PM peak hour traffic volumes for Concept 1.


EXHIBIT 8
CONCEPT 1 INTERSECTION CONTROL AND GEOMETRICS


CONCEPT 1 - DESIGN YEAR (2040) TRAFFIC VOLUMES

## Concept 2

With Concept 2, CR 9 / TH 282 is proposed to be reconstructed as a four-lane divided roadway from $190^{\text {th }}$ Street West/Valley View Drive to Creek Lane North. In conjunction with the widening, a folded diamond/split diamond interchange is proposed at the intersection of TH 169 / CR 9 / TH 282. The following provides a description of proposed improvements at the study intersections in the project's study area:

- CR 9 \& 190 ${ }^{\text {th }}$ Street West/Valley View Drive - The intersection geometry and control type is proposed to be the same as Concept 1.
- CR 9 \& TH 169 Westbound Ramps - The intersection is proposed to be expanded to provide four (4) lanes (two through lanes and dedicated left and right-turn lanes) for the northbound and southbound approaches and three (3) lanes (one through lane and dedicated left and right-turn lanes) for the eastbound and westbound approaches. The intersection is proposed to be signal controlled.
- TH 282 \& TH 169 Eastbound Ramps- The intersection geometry and control type is proposed to be the same as Concept 1.
- TH 282 \& Triangle Lane North - The intersection geometry and control type is proposed to be the same as Concept 1.
- TH 282 \& Business Access - The intersection geometry and control type is proposed to be the same as Concept 1.
- TH 282 \& Creek Lane North - The intersection geometry and control type is proposed to be the same as Concept 1.
- Creek Lane North \& Triangle Lane North - The intersection geometry and control type is proposed to be the same as Concept 1.

Exhibit 10 provides the proposed roadway layout as well as intersection control and geometry for Concept 2.

Using the Design Year (2040) No-Build turning movement volumes as a base, traffic volumes were developed for Concept 2 to take into consideration the change in access at the study intersections. The following provides more detail about the traffic volume adjustments that were made:

- Traffic traveling eastbound on TH 169 from CR 9 and TH 282 (northbound right-turn and southbound left-turn movements at the intersection of TH 169 / CR 9 / TH 282) were redistributed to Creek Lane North.
- Traffic traveling to/from Wolf Motors that access TH 282 (northbound approach) at the intersection of TH 282 \& Triangle Lane North were redistributed to the TH 282 \& Business Access.
- Traffic traveling southbound on TH 282 from Triangle Lane North (southbound left-turn movement) were redistributed to Creek Lane North.

Exhibit 11 provides the Design Year (2040) AM and PM peak hour traffic volumes for Concept 2.


EXHIBIT 10
CONCEPT 2 INTERSECTION CONTROL AND GEOMETRICS


CONCEPT 2 - DESIGN YEAR (2040) TRAFFIC VOLUMES
TH 169 / TH 282 / CR 9 INTERCHANGE CONCEPT DESIGN

## Concept 3

With Concept 3, CR 9 / TH 282 is proposed to be reconstructed as a four-lane divided roadway from $190^{\text {th }}$ Street West/Valley View Drive to Creek Lane North. In conjunction with the widening, a traditional diamond interchange is proposed at the intersection of TH 169 / CR 9 / TH 282 and TH 169 is proposed to be reconstructed so it goes over CR 9 / TH 282. The following provides a description of proposed improvements at the study intersections in the project's study area:

- CR 9 \& 190 ${ }^{\text {th }}$ Street West/Valley View Drive - The intersection geometry and control type is proposed to be the same as Concepts 1 and 2.
- CR 9 \& TH 169 Westbound Ramps - The intersection geometry and control type is proposed to be the same as Concept 1.
- TH 282 \& TH 169 Eastbound Ramps - The intersection is proposed to be expanded to a fourlegged intersection to serve the TH 169 eastbound ramps. The northbound approach will provide three (3) lanes (two through lanes and a dedicated right-turn lane) and the southbound approach will provide three (3) lanes (two through lanes and a dedicated left-turn lane). The eastbound approach will provide two (2) lanes (shared left-through and a dedicated right-turn lane). The intersection is proposed to be signal controlled.
- TH 282 \& Triangle Lane North - The intersection geometry and control type is proposed to be the same as Concepts 1 and 2.
- TH 282 \& Business Access - The intersection geometry and control type is proposed to be the same as Concepts 1 and 2.
- TH 282 \& Creek Lane North - The intersection geometry and control type is proposed to be the same as Concepts 1 and 2.
- Creek Lane North \& Triangle Lane North - The intersection is proposed to eliminate access to/from TH 169 eastbound. The southeast bound approach will provide two (2) lanes with a dedicated left-turn and shared through-right lane. The northwest bound approach will provide a shared through-right lane. The westbound approach will provide a one (1) lane approach. The intersection is proposed to be side-street stop controlled.

Exhibit 12 provides the proposed roadway layout, intersection control and geometry for Concept 3.
Using the Design Year (2040) No-Build turning movement volumes as a base, traffic volumes were developed for Concept 3 to take into consideration the change in access at some of the study intersections. The following provides more detail about the traffic diversion that was assumed:

- Traffic traveling to/from Wolf Motors that access TH 282 (northbound approach) at the intersection of TH 282 \& Triangle Lane North were redistributed to the intersection of TH 282 and Business Access.
- Traffic traveling southbound on TH 282 from Triangle Lane North (southbound left-turn movement) were redistributed to Creek Lane.


EXHIBIT 12
CONCEPT 3 INTERSECTION CONTROL AND GEOMETRICS


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CONCEPT 3 - DESIGN YEAR (2040) TRAFFIC VOLUMES
TH 169 / TH 282 / CR 9 INTERCHANGE CONCEPT DESIGN

- Traffic traveling to TH 169 eastbound via Creek Lane North were redistributed to the TH 169 / TH 282 / CR 9 eastbound ramp terminals.

Exhibit 13 provides the Design Year (2040) AM and PM peak hour traffic volumes for Concept 3.

## Design Year (2040) Build Intersection Alternatives Analysis

Intersection operating conditions at the study intersections were analyzed using Synchro/SimTraffic during the AM and PM peak hours for all three concepts listed in the previous section. The proposed intersection control and geometries provided in Exhibit 8 (Concept 1), Exhibit 10 (Concept 2), and Exhibit 12 (Concept 3) were assumed for the Design Year (2040) Build analysis. Forecasted traffic volumes for the three Concepts provided in Exhibit 9 (Concept 1), Exhibit $\mathbf{1 1}$ (Concept 2), and Exhibit $\mathbf{1 3}$ (Concept 3) were used for the intersection capacity analysis. The following provides a summary of intersection operating conditions for the Design Year (2040) Build AM and PM peak hours, including intersection LOS, delay, and queues.

## Design Year (2040) Build Capacity Analysis

Table 6 provides a summary of vehicle delay and LOS at the study intersections for Concept 1. Based on the analysis, all intersections are anticipated to operate at LOS B or better during the AM and PM peak hours with the proposed improvements. Additionally, all movements are anticipated to operate at LOS D or better during the AM and PM peak hours.

Exhibit 14 provides a summary of the intersection delay and LOS at the study intersections for Concept 1. The SimTraffic and RODEL reports for Concept 1 are provided in the Appendix.

Table 7 provides a summary of vehicle delay and LOS at the study intersections for Concept 2. Based on the analysis, all intersections are anticipated to operate at an acceptable LOS. Additionally, all individual movements are anticipated to operate at an acceptable LOS (LOSD or better) except for the following:

- Northbound left-turn and southbound through movements at the intersection of CR 9 \& TH 169 Westbound Ramp during the PM peak hour.
- Westbound left-turn movement at the intersection of TH 282 \& Business Access during the PM peak hour.

Exhibit 15 provides a summary of the intersection delay and LOS at the study intersections for Concept 2. The SimTraffic and RODEL reports for Concept 2 are provided in the Appendix.

Table 8 provides a summary of vehicle delay and LOS at the study intersections for Concept 3. Based on the analysis, all intersections are anticipated to operate at LOS B or better during the AM and PM peak hours with the proposed improvements. Additionally, all movements are anticipated to operate at LOSD or better during the AM and PM peak hours.

Exhibit 16 provides a summary of the intersection delay and LOS at the study intersections for Concept 3. The SimTraffic and RODEL reports for Concept 3 are provided in the Appendix.

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Table 6: Design Year (2040) Capacity Analysis Summary (Concept 1)

| Intersection |  |  | AM PEAK HOUR |  |  |  |  |  |  |  |  |  |  | M PE | HOUR |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Left |  | Through |  | Right |  | Overall |  | Left |  | Through |  | Right |  | Overall |  |
|  |  |  | $\frac{\text { 『 }}{\text { ® }}$ | $0$ | $\stackrel{\text { ® }}{0}$ | 0 | $\frac{\pi}{0}$ | $0$ | $\stackrel{\widetilde{O}}{\stackrel{\rightharpoonup}{0}}$ | $\begin{aligned} & \infty \\ & 0 \end{aligned}$ | $\frac{\widetilde{0}}{\stackrel{\sigma}{0}}$ | on | $\frac{\text { ® }}{\stackrel{0}{0}}$ | O | $\frac{\widetilde{0}}{\stackrel{\sigma}{0}}$ | $0$ | $\stackrel{\widetilde{O}}{\stackrel{\rightharpoonup}{0}}$ | $0$ |
| CR 9 (Quaker Avenue) \& 190th Street W/Valley View Drive | Signalized | EB Approach | 22.8 | C | 33.1 | C | 7.5 | A | 13.6 | B | 37.8 | D | 44.2 | D | 15.6 | B | 19.5 | B |
|  |  | WB Approach | 21.3 | C | 25.7 | C | 8.7 | A |  |  | 39.5 | D | 40.2 | D | 6.8 | A |  |  |
|  |  | NB Approach | 13.5 | B | 12.5 | B | 3.4 | A |  |  | 23.4 | C | 8.7 | A | 2.3 | A |  |  |
|  |  | SB Approach | 15.3 | B | 16.4 | B | 4.7 | A |  |  | 13.8 | B | 22.0 | C | 7.4 | A |  |  |
| CR 9 (Quaker Avenue) \& TH 169 Westbound On/Off Ramp/Frontage Rd | Roundabout | NW Approach | 4.6 | A | 4.6 | A | 4.6 | A | 4.3 | A | 5.0 | A | 5.0 | A | 5.0 | A | 8.8 | A |
|  |  | SW Approach | 5.6 | A | 5.6 | A | 5.6 | A |  |  | 5.8 | A | 5.8 | A | 5.8 | A |  |  |
|  |  | NB Approach | 4.2 | A | 4.2 | A | 4.2 | A |  |  | 4.5 | A | 4.5 | A | 4.5 | A |  |  |
|  |  | SB Approach | 4.0 | A | 4.0 | A | 4.0 | A |  |  | 13.4 | B | 13.4 | B | 13.4 | B |  |  |
| CR 9 (Quaker Avenue)/TH 282 <br> (2nd Street W) \& TH 169 <br> Eastbound Off Ramp | Signalized | EB Approach | 45.1 | D | - | - | 17.2 | B | 10.9 | B | 50.2 | D | - | - | 21.5 | C | 10.5 | B |
|  |  | NB Approach | - | - | 4.2 | A | - | - |  |  | - | - | 3.8 | A | - | - |  |  |
|  |  | SB Approach | - | - | 5.7 | A | - | - |  |  | - | - | 10.7 | B | - | - |  |  |
| TH 282 (2nd Street W) \& Triangle Lane N | Stop <br> Controlled | EB Approach | - | - | 0.8 | A | - | - | 1.8 | A | - | - | 1.3 | A | - | - | 1.6 | A |
|  |  | WB Approach | - | - | 1.3 | A | 1.4 | A |  |  | - | - | 1.1 | A | 1.2 | A |  |  |
|  |  | SB Approach | - | - | - | - | 16.4 | C |  |  | - | - | - | - | 13.1 | B |  |  |
| TH 282 (2nd Street W) \& Business Access | Stop <br> Controlled | EB Approach | - | - | 0.5 | A | 0.4 | A | 2.6 | A | - | - | 1.2 | A | 0.9 | A | 3.8 | A |
|  |  | WB Approach | 18.8 | C | 4.0 | A | - | - |  |  | 34.7 | D | 3.5 | A | - | - |  |  |
|  |  | NB Approach | - | - | - | - | 8.9 | A |  |  | - | - | - | - | 20.9 | C |  |  |
| TH 282 (2nd StreetW) \& Creek Lane | Roundabout | EB Approach | 4.9 | A | 4.9 | A | 4.9 | A | 5.6 | A | 7.1 | A | 7.1 | A | 7.1 | A | 7.1 | A |
|  |  | WB Approach | 5.3 | A | 5.3 | A | 5.3 | A |  |  | 6.2 | A | 6.2 | A | 6.2 | A |  |  |
|  |  | NB Approach | 9.0 | A | 9.0 | A | 9.0 | A |  |  | 10.9 | B | 10.9 | B | 10.9 | B |  |  |
|  |  | SB Approach | 5.5 | A | 5.5 | A | 5.5 | A |  |  | 6.0 | A | 6.0 | A | 6.0 | A |  |  |
| Creek Ln N/Th 169 Eastbound On Ramp \& Triangle Lane N | Stop <br> Controlled | EB Approach | 8.9 | A | 7.6 | A | 3.1 | A | 2.9 | A | 8.5 | A | 8.6 | A | 3.3 A |  | 2.6 | A |
|  |  | WB Approach | 6.2 | A | 6.6 | A | 4.7 | A |  |  | 10.7 | B | 5.6 | A | 4.9 | A |  |  |
|  |  | NB Approach | 2.2 | A | 0.9 | A | 0.3 | A |  |  | 2.5 | A | 1.1 | A | 0.6 | A |  |  |

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Table 7: Design Year (2040) Capacity Analysis Summary (Concept 2)

| Intersection |  |  | AM PEAK HOUR |  |  |  |  |  |  |  |  |  |  | M PE | HOUR |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Left |  | Through |  | Right |  |  |  | Left |  | Through |  | Right |  | Overall |  |
|  |  |  | $\frac{\sigma}{0}$ | $0$ | $\frac{\pi}{\stackrel{\sigma}{0}}$ | 0 | $\frac{\pi}{0}$ | $0$ | $\frac{\text { 『 }}{\stackrel{\circ}{0}}$ | $\begin{aligned} & \infty \\ & 0 \\ & \hline \end{aligned}$ | $\frac{\mathbb{\pi}}{\mathbb{O}}$ | $0$ | $\frac{\pi}{0}$ | $\stackrel{\sim}{0}$ | $\frac{\pi}{0}$ | $0$ | $\frac{\pi}{0}$ | 0 |
| CR 9 (Quaker Avenue) \& 190th Street W/Valley View Drive | Signalized | EB Approach | 21.2 | C | 29.0 | C | 7.5 | A | 13.2 | B | 46.3 | D | 40.6 | D | 23.0 | C | 21.0 | C |
|  |  | WB Approach | 21.6 | C | 29.9 | C | 9.8 | A |  |  | 43.2 | D | 41.7 | D | 7.1 | A |  |  |
|  |  | NB Approach | 13.8 | B | 12.4 | B | 3.7 | A |  |  | 26.0 | C | 9.9 | A | 1.8 | A |  |  |
|  |  | SB Approach | 13.7 | B | 15.9 | B | 4.3 | A |  |  | 12.9 | B | 22.0 | C | 7.9 | A |  |  |
| CR 9 (Quaker Avenue) \& TH 169 Westbound On/Off Ramp/Frontage Rd | Signalized | EB Approach | 21.9 | C | 22.3 | C | 8.6 | A | 16.9 | B | 33.7 | C | 32.5 | C | 18.5 | B | 43.8 |  |
|  |  | WB Approach | 22.1 | C | 30.0 | C | 8.0 | A |  |  | 37.6 | D | 45.2 | D | 7.4 | A |  | D |
|  |  | NB Approach | 24.4 | C | 12.6 | B | 2.3 | A |  |  | 83.9 | F | 23.2 | C | 4.8 | A |  |  |
|  |  | SB Approach | 18.0 | B | 19.2 | B | 6.7 | A |  |  | 33.4 | C | 58.4 | E | 26.8 | C |  |  |
| CR 9 (Quaker Avenue)/TH 282 | Signalized | EB Approach | 44.3 | D | - | - | 15.4 | B | 12.1 | B | 49.7 | D | - | - | 28.6 | C | 13.3 |  |
| (2nd StreetW) \& TH 169 |  | NB Approach | - | - | 3.9 | A | - | - |  |  | - | - | 6.5 | A | - | - |  | B |
| Eastbound Off Ramp |  | SB Approach | - | - | 9.9 | A | - | - |  |  | - | - | 12.4 | B | - | - |  |  |
|  | Stop <br> Controlled | EB Approach | - | - | 1.0 | A | - | - | 1.4 | A | - | - | 1.8 | A | - | - | 2.7 | A |
| Triangle Lane N |  | WB Approach | - | - | 0.9 | A | 0.8 | A |  |  | - | - | 2.4 | A | 1.1 | A |  |  |
|  |  | SB Approach | - | - | - | - | 10.1 | B |  |  | - | - | - | - | 22.3 | C |  |  |
| TH 282 (2nd Street W) \& Business Access | Stop <br> Controlled | EB Approach | - | - | 0.5 | A | 0.4 | A | 2.1 | A | - | - | 1.3 | A | 1.0 | A | 4.1 | A |
|  |  | WB Approach | 18.4 | C | 2.9 | A | - | - |  |  | 40.3 | E | 3.4 | A | - | - |  |  |
|  |  | NB Approach | - | - | - | - | 10.2 | B |  |  | - | - | - | - | 22.8 | C |  |  |
| TH 282 (2nd Street W) \& Creek Lane | Roundabout | EB Approach | 4.9 | A | 4.9 | A | 4.9 | A | 5.6 | A | 7.1 | A | 7.1 | A | 7.1 | A | 7.1 | A |
|  |  | WB Approach | 5.3 | A | 5.3 | A | 5.3 | A |  |  | 6.2 | A | 6.2 | A | 6.2 | A |  |  |
|  |  | NB Approach | 9.0 | A | 9.0 | A | 9.0 | A |  |  | 10.9 | B | 10.9 | B | 10.9 | B |  |  |
|  |  | SB Approach | 5.5 | A | 5.5 | A | 5.5 | A |  |  | 6.0 | A | 6.0 | A | 6.0 | A |  |  |
| Creek Ln N/Th 169 Eastbound On Ramp \& Triangle Lane N | Stop <br> Controlled | EB Approach | 9.7 | A | 8.8 | A | 3.0 | A | 3.0 | A | 8.9 | A | 7.4 | A | 3.6 | A | 2.8 | A |
|  |  | WB Approach | 8.7 | A | 10.6 | B | 5.0 | A |  |  | 7.6 | A | 8.7 | A | 3.7 | A |  |  |
|  |  | NB Approach | 2.2 | A | 1.0 | A | 0.2 | A |  |  | 2.6 | A | 1.3 | A | 0.6 | A |  |  |

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Table 8: Design Year (2040) Capacity Analysis Summary (Concept 3)

|  |  |  |  |  |  | PE | HOUR |  |  |  |  |  |  | P | HOUR |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | tersection |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | $\stackrel{\text { ® }}{0}$ | $\begin{aligned} & 0 \\ & 0 \\ & \hline \end{aligned}$ | $\frac{\widetilde{O}}{\stackrel{\circ}{0}}$ | $\stackrel{\sim}{0}$ | $\frac{\widetilde{3}}{\stackrel{\pi}{0}}$ | $\stackrel{\sim}{0}$ | $\frac{\pi}{0}$ | $0$ | $\frac{\pi}{0}$ | on | $\frac{\widetilde{O}}{\stackrel{O}{0}}$ | O | $\frac{\widetilde{0}}{\text { O}}$ | $0$ | $\frac{\widetilde{0}}{\stackrel{\omega}{0}}$ | O |
|  |  | EB Approach | 22.4 | C | 29.3 | C | 8.0 | A |  |  | 42.7 | D | 43.0 | D | 17.6 | B |  |  |
| CR 9 (Quaker Avenue) \& 190th | Signalized | WB Approach | 22.0 | C | 30.5 | C | 8.8 | A | 14.0 | B | 36.5 | D | 39.5 | D | 6.7 | A | 195 | B |
| Street W/Valley View Drive | Signalized | NB Approach | 15.7 | B | 12.9 | B | 3.7 | A | 14.0 | B | 25.5 | C | 8.5 | A | 3.0 | A | 19.5 | B |
|  |  | SB Approach | 15.3 | B | 16.0 | B | 4.3 | A |  |  | 14.0 | B | 21.0 | C | 7.2 | A |  |  |
|  |  | NW Approach | 4.6 | A | 4.6 | A | 4.6 | A |  |  | 5.0 | A | 5.0 | A | 5.0 | A |  |  |
| CR 9 (Quaker Avenue) \& TH <br> 169 Westbound On/Off | Roundabout | SW Approach | 5.6 | A | 5.6 | A | 5.6 | A | 43 | A | 5.8 | A | 5.8 | A | 5.8 | A | 8 | A |
| 169 Wesbound On/Off | Roundabout | NB Approach | 4.2 | A | 4.2 | A | 4.2 | A | 4.3 | A | 4.5 | A | 4.5 | A | 4.5 | A | 8.8 | A |
|  |  | SB Approach | 4.0 | A | 4.0 | A | 4.0 | A |  |  | 13.4 | B | 13.4 | B | 13.4 | B |  |  |
| CR 9 (Quaker Avenue)/TH 282 |  | EB Approach | 48.8 | D | - | - | 15.5 | B |  |  | 50.4 | D | - | - | 25.9 | C |  |  |
| (2nd StreetW) \& TH 169 | Signalized | NB Approach | - | - | 16.6 | B | 4.7 | A | 17.9 | B | - | - | 10.6 | B | 2.7 | A | 12.3 | B |
| Eastbound On/Off Ramp |  | SB Approach | 28.9 | C | 10.1 | B | - | - |  |  | 25.6 | C | 6.9 | A | - | - |  |  |
|  |  | EB Approach | - | - | 1.0 | A | - | - |  |  | - | - | 1.1 | A | - | - |  |  |
| Triangle Lane N | Controlled | WB Approach | - | - | 3.8 | A | 1.3 | A | 3.3 | A | - | - | 3.4 | A | 2.3 | A | 3.2 | A |
|  |  | SB Approach | - | - | - | - | 14.3 | B |  |  | - | - | - | - | 25.7 | D |  |  |
|  |  | EB Approach | - | - | 0.5 | A | 0.4 | A |  |  | - | - | 1.2 | A | 0.9 | A |  |  |
| Business Access |  | WB Approach | 11.0 | B | 2.5 | A | - | - | 1.8 | A | 22.4 | C | 3.4 | A | - | - | 3.4 | A |
|  |  | NB Approach | - | - | - | - | 7.9 | A |  |  | - | - | - | - | 18.6 | C |  |  |
| TH 282 (2nd Street W) \& Creek Lane | Roundabout | EB Approach | 3.7 | A | 3.7 | A | 3.7 | A | 4.5 | A | 5.1 | A | 5.1 | A | 5.1 | A | 5.2 | A |
|  |  | WB Approach | 4.1 | A | 4.1 | A | 4.1 | A |  |  | 4.4 | A | 4.4 | A | 4.4 | A |  |  |
|  |  | NB Approach | 7.5 | A | 7.5 | A | 7.5 | A |  |  | 8.9 | A | 8.9 | A | 8.9 | A |  |  |
|  |  | SB Approach | 5.9 | A | 5.9 | A | 5.9 | A |  |  | 6.3 | A | 6.3 | A | 6.3 | A |  |  |
| Creek Ln N \& Triangle Lane N | Stop <br> Controlled | EB Approach | - | - | - | - | - | - | 1.0 | A | - | - | - | - | - | - | 0.7 | A |
|  |  | WB Approach | 9.6 | A | 9.6 | A | 9.6 | A |  |  | 9.0 | - | 9.0 | A | 9.0 | A |  |  |
|  |  | NB Approach | - | - | - | - | - | - |  |  | - | - | - | - | - | - |  |  |



EXHIBIT 14

CONCEPT 1 - DESIGN YEAR (2040) DELAY AND LOS
TH 169 / TH 282 / CR 9 INTERCHANGE CONCEPT DESIGN
 CONCEPT 2 - DESIGN YEAR (2040) DELAY AND LOS
 CONCEPT 3 - DESIGN YEAR (2040) DELAY AND LOS

## Design Year (2040) Build Queue Analysis

Design Year (2040) Build conditions vehicle queuing was reviewed based on the SimTraffic and RODEL analysis for all three concepts. Queue lengths are the $95^{\text {th }}$ Percentile Queue as calculated in SimTraffic and RODEL. SimTraffic reports the queue in feet where as RODEL reports queue in number of vehicles ( 25 feet per vehicle was assumed).

Table 9 provides a summary of Design Year (2040) Build AM and PM peak hour queue lengths based on the Synchro/SimTraffic and RODEL analysis for Concept 1. Based on the analysis, the southbound right turn at TH 282 \& Triangle Lane North and northbound right from the TH 282 \& Business Access have queue lengths that extend beyond the southern Holiday and McDonald's access points and into the existing Radermacher's parking lot, respectively. The access to McDonald's and Holiday is experiencing impacts under existing conditions and since the M cDonald's access is a one-way entry access and Holiday has two access points no major impacts are anticipated at TH 282 \& Triangle Lane North. The northbound queue extending into Radermacher's is experienced under existing conditions. Even though it is an existing condition, as part of the conversion to a $3 / 4$ intersection, modifications within the parking lot should be considered to improve operations near this access. The southbound through movement at the CR 9 \& TH 169 Westbound Ramps is operating at an acceptable level of service and will result in a moving queue so no major concerns occur at this location except that long-term queuing over the railroad tracks for a Concept 1 scenario that is not grade separated long term is a potential long-term safety concern.

Table 10 provides a summary of Design Year (2040) Build AM and PM peak hour queue lengths based on the Synchro/SimTraffic and RODEL analysis for Concept 2. Based on the analysis, all turn lanes are anticipated to accommodate the 95th percentile queue except for the northbound left-turn lane and southbound right-turn lane at the intersection of CR $9 \&$ TH 169 Westbound Ramps. The northbound and southbound storage lengths at this intersection have room to be extended to accommodate the queue so that modification will be made to Concept 2 if it is the locally preferred alternative. Based on the analysis, the southbound right turn at TH 282 \& Triangle Lane North and northbound right from the TH 282 \& Business Access have queue lengths that extend beyond the southern Holiday and McDonald's access points and into the existing Radermacher's parking lot, respectively. The access to McDonald's and Holiday is experiencing impacts under existing conditions and since the McDonald's access is a one-way entry access and Holiday has two access points no major impacts are anticipated at TH 282 \& Triangle Lane North. The northbound queue extending into Radermacher's is experienced under existing conditions. Even though it is an existing condition, as part of the conversion to a $3 / 4$ intersection, modifications within the parking lot should be considered to improve operations near this access.

Table 9: Design Year (2040) 95 ${ }^{\text {th }}$ Percentile Queue Summary (Concept 1)

| Intersection | Lane | Storage <br> Lenght (it) | AM Peak | PM Peak |
| :---: | :---: | :---: | :---: | :---: |
| CR 9 (Quaker Avenue) \& 190th Street W/Valley View Drive | EB Left | 250 | 111 | 111 |
|  | EB Right | 250 | 108 | 161 |
|  | WB Left | 300 | 147 | 144 |
|  | WB Right | 300 | 45 | 37 |
|  | NB Left | 300 | 129 | 203 |
|  | NB Right | >500 | 71 | 47 |
|  | SB Left | 280 | 58 | 63 |
|  | SB Right | 275 | 31 | 86 |
| CR 9 (Quaker Avenue) \& TH 169 Westbound On/Off Ramp/Frontage Rd | NW | 120 | 29 | 42 |
|  | SW | >500 | 21 | 25 |
|  | NB | 360 | 108 | 100 |
|  | SB | $>500$ | 79 | 554 |
| CR 9 (Quaker Avenue)/TH 282 (2nd Street W) \& TH 169 Eastbound Off Ramp | EB Left | 280 | 258 | 112 |
|  | EB Right | 280 | 213 | 209 |
| TH 282 (2nd Street W) \& Triangle Lane N | WB Right | 150 | 20 | 6 |
|  | SB Right | 50 | 99 | 87 |
| TH 282 (2nd Street W) \& Business Access | EB Right | 135 | 16 | 10 |
|  | WB Left | 120 | 74 | 118 |
|  | NB Right | 50 | 59 | 123 |
| TH 282 (2nd Street W) \& Creek Lane | EB | 330 | 116 | 233 |
|  | WB | $>500$ | 120 | 161 |
|  | NB | 85 | 73 | 78 |
|  | SB | 90 | 14 | 16 |
| Creek Ln N/Th 169 Eastbound On Ramp \& Triangle Lane N | EB Left | 100 | 64 | 46 |
|  | NB Left | 160 | 7 | 33 |

Queue lengths are the 95th Percentile Queue as calculated in SimTraffic and RODEL. SimTraffic reports the queue in feet where as RODEL reports queue in number of vehicles ( 25 feet per vehicle is assumed).

Table 10: Design Year (2040) 95 ${ }^{\text {th }}$ Percentile Queue Summary (Concept 2)

| Intersection | Lane | Storage <br> Length (ti) | AM Peak | PM Peak |
| :---: | :---: | :---: | :---: | :---: |
| CR 9 (Quaker Avenue) \& 190th Street W/Valley View Drive | EB Left | 250 | 101 | 125 |
|  | EB Right | 250 | 123 | 229 |
|  | WB Left | 300 | 108 | 66 |
|  | WB Right | 300 | 44 | 41 |
|  | NB Left | 300 | 129 | 199 |
|  | NB Right | >500 | 58 | 14 |
|  | SB Left | 280 | 51 | 103 |
|  | SB Right | 275 | 34 | 96 |
| CR 9 (Quaker Avenue) \& TH 169 Westbound On/Off Ramp/Frontage Rd | EB Left | 280 | 147 | 164 |
|  | EB Right | 280 | 70 | 152 |
|  | WB Left | 265 | 114 | 154 |
|  | WB Right | 265 | 30 | 38 |
|  | NB Left | 290 | 199 | 385 |
|  | NB Right | 290 | 27 | 32 |
|  | SB Left | 225 | 46 | 154 |
|  | SB Right | 280 | 61 | 417 |
| CR 9 (Quaker Avenue)/TH 282 (2nd Street W) \& TH 169 Eastbound Off Ramp | EB Left | 280 | 270 | 145 |
|  | EB Right | 280 | 181 | 246 |
| TH 282 (2nd Street W) \& Triangle Lane N | WB Right | 150 | 4 | 26 |
|  | SB Right | 50 | 85 | 126 |
| TH 282 (2nd Street W) \& Business Access | EB Right | 135 | 11 | 29 |
|  | WB Left | 120 | 60 | 118 |
|  | NB Right | 50 | 65 | 135 |
| TH 282 (2nd Street W) \& Creek Lane | EB | 330 | 116 | 233 |
|  | WB | >500 | 120 | 161 |
|  | NB | 85 | 73 | 78 |
|  | SB | 90 | 14 | 16 |
| Creek Ln N/Th 169 Eastbound On Ramp \& Triangle Lane $N$ | EB Left | 100 | 67 | 48 |
|  | NB Left | 160 | 4 | 7 |

Queue lengths are the 95th Percentile Queue as calculated in SimTraffic and RODEL. SimTraffic reports the queue in feet where as RODEL reports queue in number of vehicles ( 25 feet per vehicle is assumed).

Table 11 provides a summary of Design Year (2040) Build AM and PM peak hour queue lengths based on the Synchro/SimTraffic and RODEL analysis for Concept 3. Based on the analysis, all turn lanes are anticipated to accommodate the $95^{\text {th }}$ percentile queue except for the southbound approach at the intersection of CR $9 \&$ TH 169 Westbound Ramps and the southbound left-turn lane, eastbound left-turn lane, and northbound right-turn lane at the intersection of CR $9 \&$ TH 169 Eastbound Ramps. The southbound left-turn lane, eastbound left-turn lane, and northbound right-turn lane at this intersection have room to be extended to accommodate the queue so that modification will be made to Concept 3 if
it is the locally preferred alternative. The southbound through movement at the CR 9 \& TH 169 Westbound Ramps is operating at an acceptable level of service and will result in a moving queue so no major concerns occur at this location except that long-term queuing over the railroad tracks is anticipated and given that the railroad crossing cannot be grade separated in the future due to the close spacing between the roundabout at the Westbound TH 169 Ramps and railroad tracks results in a potential long-term safety concern. Based on the analysis, the southbound right turn at TH 282 \& Triangle Lane North and northbound right from the TH 282 \& Business Access have queue lengths that extend beyond the southern Holiday and McDonald's access points and into the existing Radermacher's parking lot, respectively. The access to McDonald's and Holiday is experiencing impacts under existing conditions and since the McDonald's access is a one-way entry access and Holiday has two access points no major impacts are anticipated at TH 282 \& Triangle Lane North. The northbound queue extending into Radermacher's is experienced under existing conditions. Even though it is an existing condition, as part of the conversion to a $3 / 4$ intersection, modifications within the parking lot should be considered to improve operations near this access.

Table 11: Design Year (2040) 95 ${ }^{\text {th }}$ Percentile Queue Summary (Concept 3)

| Intersection | Lane | Storage <br> Length (it) | AM Peak | PM Peak |
| :---: | :---: | :---: | :---: | :---: |
| CR 9 (Quaker Avenue) \& 190th Street W/Valley View Drive | EB Left | 250 | 104 | 129 |
|  | EB Right | 250 | 114 | 177 |
|  | WB Left | 300 | 151 | 131 |
|  | WB Right | 300 | 40 | 40 |
|  | NB Left | 300 | 147 | 205 |
|  | NB Right | $>500$ | 68 | 57 |
|  | SB Left | 280 | 51 | 55 |
|  | SB Right | 275 | 32 | 98 |
| CR 9 (Quaker Avenue) \& TH 169 Westbound On/Off Ramp/Frontage Rd | NW | 120 | 29 | 42 |
|  | SW | >500 | 21 | 25 |
|  | NB | 360 | 108 | 100 |
|  | SB | >500 | 79 | 554 |
| CR 9 (Quaker Avenue)/TH 282 (2nd Street W) \& TH 169 Eastbound On/Off Ramp | EB Left | 280 | 313 | 107 |
|  | EB Right | 280 | 195 | 227 |
|  | NB Right | 160 | 177 | 118 |
|  | SB Left | 155 | 186 | 198 |
| TH 282 (2nd StreetW) \& Triangle Lane N | WB Right | 150 | 38 | 68 |
|  | SB Right | 50 | 120 | 135 |
| TH 282 (2nd Street W) \& Business Access | EB Right | 135 | 4 | 18 |
|  | WB Left | 110 | 54 | 92 |
|  | NB Right | 50 | 59 | 123 |
| TH 282 (2nd Street W) \& Creek Lane | EB | 330 | 62 | 127 |
|  | WB | >500 | 88 | 105 |
|  | NB | 85 | 58 | 60 |
|  | SB | 90 | 16 | 18 |
| Creek Ln N \& Triangle Lane N | WB | 50 | 31 | 31 |

Queue lengths are the 95th Percentile Queue as calculated in SimTraffic and RODEL. SimTraffic reports the queue in feet where as RODEL reports queue in number of vehicles ( 25 feet per vehicle is assumed).

## Conclusions and Recommendations

This traffic analysis was completed as part of a joint project between the City, Scott County and MnDOT, and included traffic engineering, concept design, and stakeholder engagement services for the TH 169 / TH 282 / CR 9 interchange area. As part of the traffic engineering services, an operations analysis was performed at critical intersections within the study area to support interchange concept development and determine the most appropriate intersection control and geometry to accommodate existing and future traffic. The traffic analysis included a summary of historic crash data along the study corridor, intersection capacity analysis for Existing and Design Year conditions, and a discussion on potential roadway and intersection improvement alternatives.

The conclusions of the analysis are summarized below:

- Analysis of existing traffic operations show that all intersections are currently operating at an acceptable LOS during the weekday AM and PM peak hours. Additionally, all individual movements are operating at LOS D or better for both the AM and PM peak hours except for the eastbound and westbound lefts at TH 169 and TH 282, which are operating at LOS E during the AM and PM peak hours.
- The review of the existing crash data shows that the intersections of TH 169 / CR 9 / TH 282 and TH 282 \& Triangle Lane North have a critical index of greater than 1.0, meaning that these two intersections are worse than the normal, expected range (i.e. there is a crash issue at these intersections today). The crash data indicates that two contributing factors are having a traffic signal on a high-speed, high-volume facility (TH 169) and the queuing from this signal and the associated impacts due to the inadequate intersection spacing between Triangle Lane North and TH 169.
- An analysis of forecast 2040 No-Action conditions shows the following intersections are anticipated to operate at an overall LOSE or LOS F during the AM and PM peak hours:
- CR $9 \& 190^{\text {th }}$ Street West/Valley View Drive (PM peak hour)
- CR 9 \& Frontage Road (AM and PM peak hours)
- TH 169 / CR 9 / TH 282 (PM peak hour)
- TH 282 \& Triangle Lane North (PM peak hour)
- Creek Lane North \& Triangle Lane North (AM peak hour)
- TH 169 \& Creek Lane North (PM peak hour)

Due the significant number of intersection that are anticipated to operate below the acceptable LOS for Design Year (2040) No-Action conditions, improvements along the study corridor will be necessary to provide acceptable LOS into the future. The continued deterioration of LOS between today and future conditions is also anticipated to result in additional crash concerns along the corridor.

- Several interchange and roadway concepts were considered through the planning process, and based on input from the City, County and MnDOT, the following three (3) preferred concepts were considered as part of the traffic analysis:
- Concept 1 - Roundabout / Split Diamond
- Concept 2 - Folded Diamond / Split Diamond
- Concept 3 - Diamond Interchange with TH 169 over TH 282 \& CR 9
- There were no significant differences between the three concepts from a traffic operations perspective.
- All concepts will reasonably serve 2040 traffic from operations and safety perspective. Other screening criteria will need to be used to decide on the locally preferred interchange alternative.


## Appendix

1. Existing Year (2017) SimTraffic Reports
2. Design Year (2040) No-Action SimTraffic Reports
3. Design Year (2040) Concept 1 SimTraffic Reports
4. Design Year (2040) Concept 1 RODEL Reports
5. Design Year (2040) Concept 2 SimTraffic Reports
6. Design Year (2040) Concept 2 RODEL Reports
7. Design Year (2040) Concept 3 SimTraffic Reports
8. Design Year (2040) Concept 3 RODEL Reports

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## 1. EXISTING YEAR (2017) SIMTRAFFIC REPORTS

## 1: TH 282/CR 9 \& TH 169 Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 2.4 | 0.3 | 2.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 58.9 | 27.0 | 6.4 | 57.7 | 28.9 | 3.1 | 26.0 | 33.7 | 22.0 | 29.1 | 39.5 |

1: TH 282/CR 9 \& TH 169 Performance by movement

| Movement | All |
| :--- | ---: |
| Denied Del/Veh (s) | 0.4 |
| Total Del/Veh (s) | 30.2 |

2: Driveway/Triangle Lane \& TH 282 Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 | 0.2 | 0.2 |
| Total Del/Veh (s) | 6.8 | 2.9 | 1.9 | 4.4 | 0.4 | 0.4 | 17.9 | 17.9 | 3.2 | 17.3 | 17.0 |

2. Driveway/Triangle Lane \& TH 282 Performance by movement

| Movement | All |
| :--- | :--- |
| Denied Del/Veh (s) | 0.0 |
| Total Del/Veh (s) | 3.5 |

3: Rademachers Driveway \& TH 282 Performance by movement

| Movement | EBT | EBR | WBL | WBT | NBL | NBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 | 0.0 |
| Total Del/Veh (s) | 0.7 | 0.6 | 3.7 | 0.6 | 10.8 | 3.5 | 1.0 |

4: Creek Lane \& TH 282 Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.0 | 3.5 | 0.5 | 0.3 | 3.7 | 0.7 | 3.6 | 4.2 | 0.2 |
| Total Del/Veh (s) | 2.9 | 0.4 | 2.6 | 2.8 | 0.6 | 0.2 | 12.7 | 11.2 | 1.7 | 9.5 | 10.3 |

## 4: Creek Lane \& TH 282 Performance by movement

| Movement | All |
| :--- | :---: |
| Denied Del/Veh (s) | 1.2 |
| Total Del/Veh (s) | 3.7 |

5: Creek Lane \& Triangle Lane/Park Entrance Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.1 | 0.2 | 0.2 | 0.1 | 0.1 | 0.1 | 0.2 | 0.1 | 0.2 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 6.7 | 6.2 | 4.7 | 3.4 | 4.4 | 5.0 | 1.9 | 1.0 | 0.3 | 1.2 | 0.1 | 0.1 |

## 5: Creek Lane \& Triangle Lane/Park Entrance Performance by movement

| Movement | All |
| :--- | :---: |
| Denied Del/Veh (s) | 0.1 |
| Total Del/Veh (s) | 3.1 |

## 6: Creek Lane \& TH 169 Performance by movement

| Movement | EBT | EBR | WBT | NBT | NBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.1 | 0.1 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 12.0 | 5.4 | 0.5 | 1.2 | 15.5 | 8.4 |

7: CR 9 \& Frontage Road Performance by movement

| Movement | WBL | WBR | NBT | NBR | SBL | SBT | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.1 | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 10.8 | 4.7 | 1.8 | 1.5 | 2.8 | 1.3 | 2.4 |

8: CR 9 \& CR 57/Valley View Drive Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 0.2 | 0.1 | 0.2 | 0.1 | 0.2 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 9.3 | 12.1 | 4.2 | 8.9 | 11.2 | 3.9 | 3.6 | 1.3 | 1.6 | 1.2 | 0.4 |

8: CR 9 \& CR 57/Valley View Drive Performance by movement

| Movement | All |
| :--- | :--- |
| Denied Del/Veh (s) | 0.0 |
| Total Del/Veh $(\mathrm{s})$ | 2.3 |

9: CR 9 \& Ervin Industrial Boulevard Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.2 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.0 | 0.0 | 0.0 | 0.2 | 0.1 | 0.1 |
| Total Del/Veh (s) | 7.3 | 8.3 | 3.1 | 8.3 | 8.0 | 2.9 | 3.0 | 0.8 | 0.6 | 3.2 | 0.2 | 0.1 |

## 9: CR 9 \& Ervin Industrial Boulevard Performance by movement

| Movement | All |
| :--- | :---: |
| Denied Del/Veh (s) | 0.0 |
| Total Del/Veh (s) | 1.1 |

Total Network Performance

|  |  |
| :--- | ---: |
| Denied Del/Veh (s) | 0.8 |
| Total Del/Veh (s) | 34.1 |

## Intersection: 1: TH 282/CR 9 \& TH 169

| Movement | EB | EB | EB | EB | WB | WB | WB | WB | NB | NB | NB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | R | L | T | T | R | L | T | TR | L |
| Maximum Queue (ft) | 190 | 264 | 265 | 94 | 116 | 202 | 209 | 37 | 142 | 179 | 206 | 117 |
| Average Queue (ft) | 92 | 151 | 143 | 36 | 42 | 110 | 102 | 9 | 60 | 81 | 99 | 43 |
| 95th Queue (ft) | 162 | 236 | 234 | 66 | 94 | 172 | 169 | 31 | 115 | 149 | 183 | 88 |
| Link Distance (ft) |  | 2157 | 2157 |  |  | 924 | 924 |  |  | 362 | 362 | 174 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (ft) | 300 |  |  | 300 | 550 |  |  | 350 | 150 |  |  |  |
| Storage Blk Time (\%) |  | 0 | 0 |  |  |  |  |  | 0 | 1 |  |  |
| Queuing Penalty (veh) |  | 0 | 0 |  |  |  |  |  | 0 | 1 |  |  |

Intersection: 1: TH 282/CR 9 \& TH 169

| Movement | SB | SB |
| :--- | ---: | ---: |
| Directions Served | T | TR |
| Maximum Queue (ft) | 170 | 174 |
| Average Queue (ft) | 97 | 99 |
| 95th Queue (ft) | 157 | 166 |
| Link Distance (ft) | 174 | 174 |
| Upstream Blk Time (\%) | 0 | 1 |
| Queuing Penalty (veh) | 1 | 1 |
| Storage Bay Dist (ft) |  |  |
| Storage Blk Time (\%) |  |  |

## Intersection: 2: Driveway/Triangle Lane \& TH 282

| Movement | EB | EB | WB | WB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LT | TR | L | T | R | LTR | LTR |
| Maximum Queue (ft) | 137 | 41 | 27 | 4 | 23 | 41 | 128 |
| Average Queue (ft) | 41 | 2 | 2 | 0 | 1 | 12 | 47 |
| 95th Queue (ft) | 97 | 27 | 15 | 3 | 11 | 36 | 94 |
| Link Distance (ft) | 362 | 362 |  | 383 |  | 241 | 315 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |
| Storage Bay Dist (ft) |  |  | 200 |  | 100 |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |

## Intersection: 3: Rademachers Driveway \& TH 282

| Movement | EB | EB | WB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | TR | L | L | R |
| Maximum Queue (ft) | 8 | 4 | 36 | 43 | 30 |
| Average Queue (ft) | 0 | 0 | 6 | 15 | 12 |
| 95th Queue (ft) | 6 | 3 | 28 | 42 | 35 |
| Link Distance (ft) | 383 | 383 |  | 256 | 256 |
| Upstream Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  | 100 |  |  |
| Storage Bay Dist (ft) |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |

Intersection: 4: Creek Lane \& TH 282

| Movement | EB | EB | EB | WB | WB | NB | NB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | R | L | TR | L | T | L | TR |
| Maximum Queue (ft) | 18 | 4 | 106 | 52 | 4 | 113 | 88 | 38 | 31 |
| Average Queue (ft) | 1 | 0 | 23 | 17 | 0 | 50 | 42 | 11 | 13 |
| 95th Queue (ft) | 12 | 4 | 80 | 46 | 4 | 87 | 68 | 35 | 37 |
| Link Distance (ft) |  | 322 | 322 |  | 566 |  | 403 |  | 358 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (ft) | 100 |  |  | 200 |  | 100 |  | 100 |  |
| Storage BIk Time (\%) |  |  |  |  |  | 1 | 0 |  |  |
| Queuing Penalty (veh) |  |  |  |  |  | 2 | 0 |  |  |

## Intersection: 5: Creek Lane \& Triangle Lane/Park Entrance

| Movement | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LTR | LTR | LTR |
| Maximum Queue (ft) | 71 | 35 | 34 | 6 |
| Average Queue (ft) | 32 | 13 | 2 | 1 |
| 95th Queue (ft) | 58 | 37 | 18 | 8 |
| Link Distance (ft) | 359 | 92 | 336 | 111 |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

## Intersection: 6: Creek Lane \& TH 169

| Movement | EB | EB | NB |
| :--- | ---: | ---: | ---: |
| Directions Served | T | T | R |
| Maximum Queue (tt) | 43 | 54 | 120 |
| Average Queue (ft) | 2 | 4 | 62 |
| 95th Queue (ft) | 17 | 29 | 114 |
| Link Distance (tt) | 924 | 924 | 111 |
| Upstream Blk Time (\%) |  |  | 2 |
| Queuing Penalty (veh) |  | 4 |  |
| Storage Bay Dist (tt) |  |  |  |
| Storage Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |

## Intersection: 7: CR 9 \& Frontage Road

| Movement | WB | NB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LR | TR | LT | T | T |
| Maximum Queue (ft) | 70 | 7 | 28 | 10 | 18 |
| Average Queue (ft) | 36 | 0 | 2 | 0 | 1 |
| 95th Queue (ft) | 61 | 5 | 13 | 5 | 13 |
| Link Distance (ft) | 766 | 174 |  | 1086 | 1086 |
| Upstream Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  | 100 |  |  |
| Storage Bay Dist (ft) |  |  |  |  |  |

## Intersection: 8: CR 9 \& CR 57/Valley View Drive

| Movement | EB | WB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LTR | LT | TR | LT | TR |
| Maximum Queue (ft) | 95 | 54 | 50 | 11 | 9 | 3 |
| Average Queue (ft) | 44 | 24 | 8 | 0 | 0 | 0 |
| 95th Queue (ft) | 72 | 49 | 33 | 8 | 5 | 2 |
| Link Distance (ft) | 796 | 393 | 1086 | 1086 | 657 | 657 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |

Intersection: 9: CR 9 \& Ervin Industrial Boulevard

| Movement | EB | WB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LTR | LT | TR | LT | TR |
| Maximum Queue (ft) | 44 | 40 | 45 | 18 | 16 | 4 |
| Average Queue ( ft ) | 17 | 14 | 5 | 1 | 1 | 0 |
| 95th Queue (ft) | 43 | 36 | 27 | 10 | 10 | 3 |
| Link Distance ( ft ) | 404 | 462 | 657 | 657 | 421 | 421 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |

## Network Summary

Network wide Queuing Penalty: 9

## 1: TH 282/CR 9 \& TH 169 Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 2.9 | 0.2 | 2.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 73.1 | 38.6 | 7.8 | 64.4 | 34.0 | 4.4 | 34.5 | 29.4 | 15.7 | 27.7 | 44.3 |

1: TH 282/CR 9 \& TH 169 Performance by movement

| Movement | All |
| :--- | ---: |
| Denied Del/Veh (s) | 0.2 |
| Total Del/Veh (s) | 34.7 |

2: Driveway/Triangle Lane \& TH 282 Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 | 0.2 | 0.2 |
| Total Del/Veh (s) | 9.4 | 4.6 | 2.4 | 4.5 | 0.6 | 0.5 | 16.1 | 24.2 | 8.3 | 24.3 | 22.1 |

2: Driveway/Triangle Lane \& TH 282 Performance by movement

| Movement | All |
| :--- | :--- |
| Denied Del/Veh (s) | 0.0 |
| Total Del/Veh (s) | 5.0 |

3: Rademachers Driveway \& TH 282 Performance by movement

| Movement | EBT | EBR | WBL | WBT | NBL | NBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 | 0.0 |
| Total Del/Veh (s) | 1.2 | 0.6 | 7.2 | 0.6 | 19.1 | 4.2 | 2.1 |

4: Creek Lane \& TH 282 Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.0 | 3.4 | 0.6 | 0.7 | 3.8 | 0.6 | 3.8 | 4.1 | 0.1 |
| Total Del/Veh (s) | 3.3 | 0.7 | 2.4 | 4.8 | 0.7 | 0.2 | 20.4 | 13.5 | 1.7 | 14.9 | 16.4 |

## 4: Creek Lane \& TH 282 Performance by movement

| Movement | All |
| :--- | :---: |
| Denied Del/Veh (s) | 1.0 |
| Total Del/Veh (s) | 3.5 |

5: Creek Lane \& Triangle Lane/Park Entrance Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.1 | 0.2 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 5.0 | 6.5 | 2.9 | 3.9 | 4.8 | 2.5 | 2.0 | 0.5 | 0.2 | 1.0 | 0.2 | 0.1 |

## 5: Creek Lane \& Triangle Lane/Park Entrance Performance by movement

| Movement | All |
| :--- | :--- |
| Denied Del/Veh (s) | 0.1 |
| Total Del/Veh (s) | 2.2 |

## 6: Creek Lane \& TH 169 Performance by movement

| Movement | EBT | EBR | WBT | NBT | NBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.2 | 0.0 | 0.0 | 0.1 |
| Total Del/Veh (s) | 10.8 | 4.5 | 0.9 | 0.2 | 7.9 | 4.6 |

## 7: CR 9 \& Frontage Road Performance by movement

| Movement | WBL | WBR | NBT | NBR | SBL | SBT | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.1 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 22.6 | 4.2 | 1.7 | 1.7 | 3.5 | 6.4 | 5.4 |

8: CR 9 \& CR 57/Valley View Drive Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 0.1 | 0.1 | 0.2 | 0.1 | 0.1 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 8.7 | 13.6 | 4.9 | 11.3 | 12.3 | 6.5 | 6.7 | 1.3 | 1.1 | 1.6 | 0.6 |

8: CR 9 \& CR 57/Valley View Drive Performance by movement

| Movement | All |
| :--- | :--- |
| Denied Del/Veh (s) | 0.0 |
| Total Del/Veh $(\mathrm{s})$ | 2.3 |

9: CR 9 \& Ervin Industrial Boulevard Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 0.1 | 0.2 | 0.1 | 0.1 | 0.1 | 0.1 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 |
| Total Del/Veh (s) | 6.4 | 11.4 | 3.6 | 7.7 | 8.5 | 2.8 | 3.8 | 0.5 | 0.4 | 0.9 | 0.3 |

## 9: CR 9 \& Ervin Industrial Boulevard Performance by movement

| Movement | All |
| :--- | :--- |
| Denied Del/Veh $(\mathrm{s})$ | 0.1 |
| Total Del/Veh $(\mathrm{s})$ | 0.8 |

Total Network Performance

|  |  |
| :--- | ---: |
| Denied Del/Veh (s) | 0.7 |
| Total Del/Veh (s) | 38.4 |

## Intersection: 1: TH 282/CR 9 \& TH 169

| Movement | EB | EB | EB | EB | WB | WB | WB | WB | NB | NB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | T | T | R | L | T | T | R | L | T | TR | L |
| Maximum Queue (ft) | 96 | 240 | 236 | 98 | 200 | 349 | 362 | 60 | 199 | 286 | 214 | 107 |
| Average Queue ( ft$)$ | 27 | 135 | 124 | 38 | 90 | 207 | 201 | 23 | 121 | 81 | 81 | 43 |
| 95th Queue (ft) | 70 | 209 | 206 | 74 | 165 | 310 | 312 | 51 | 199 | 198 | 158 | 90 |
| Link Distance (ft) |  | 2157 | 2157 |  |  | 924 | 924 |  |  | 362 | 362 | 174 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (ft) | 300 |  |  | 300 | 550 |  |  | 350 | 150 |  |  |  |
| Storage Blk Time (\%) |  | 0 |  |  |  |  | 0 |  | 7 | 1 |  |  |
| Queuing Penalty (veh) |  | 0 |  |  |  |  | 0 |  | 9 | 1 |  |  |

Intersection: 1: TH 282/CR 9 \& TH 169

| Movement | SB | SB |
| :--- | ---: | ---: |
| Directions Served | T | TR |
| Maximum Queue (ft) | 200 | 195 |
| Average Queue (ft) | 159 | 158 |
| 95th Queue (ft) | 215 | 211 |
| Link Distance (ft) | 174 | 174 |
| Upstream Blk Time (\%) | 16 | 15 |
| Queuing Penalty (veh) | 36 | 35 |
| Storage Bay Dist (ft) |  |  |
| Storage Blk Time (\%) |  |  |

## Intersection: 2: Driveway/Triangle Lane \& TH 282

| Movement | EB | EB | WB | WB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LT | TR | L | T | R | LTR | LTR |
| Maximum Queue (ft) | 210 | 130 | 22 | 4 | 17 | 37 | 176 |
| Average Queue (ft) | 68 | 7 | 1 | 0 | 1 | 12 | 58 |
| 95th Queue (ft) | 160 | 58 | 11 | 0 | 9 | 35 | 123 |
| Link Distance (ft) | 362 | 362 |  | 383 |  | 241 | 315 |
| Upstream Blk Time (\%) |  |  |  |  |  |  | 0 |
| Queuing Penalty (veh) |  |  |  |  |  |  | 0 |
| Storage Bay Dist (ft) |  |  | 200 |  | 100 |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |  |

Intersection: 3: Rademachers Driveway \& TH 282

| Movement | WB | NB | NB |
| :--- | ---: | ---: | ---: |
| Directions Served | L | L | R |
| Maximum Queue (ft) | 68 | 66 | 65 |
| Average Queue (ft) | 25 | 32 | 28 |
| 95th Queue (ft) | 57 | 60 | 53 |
| Link Distance (ft) |  | 256 | 256 |
| Upstream Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |
| Storage Bay Dist (ft) | 100 |  |  |
| Storage Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |

Intersection: 4: Creek Lane \& TH 282

| Movement | EB | EB | WB | NB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | R | L | L | T | R | L | TR |
| Maximum Queue (ft) | 24 | 99 | 74 | 125 | 57 | 52 | 42 | 36 |
| Average Queue (ft) | 1 | 12 | 27 | 54 | 26 | 3 | 15 | 13 |
| 95th Queue (ft) | 9 | 55 | 60 | 96 | 53 | 24 | 41 | 39 |
| Link Distance ( ft ) |  | 322 |  |  | 403 |  |  | 358 |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |
| Storage Bay Dist (ft) | 100 |  | 200 | 100 |  | 100 | 100 |  |
| Storage Blk Time (\%) |  |  |  | 3 |  | 0 |  |  |
| Queuing Penalty (veh) |  |  |  | 3 |  | 0 |  |  |

## Intersection: 5: Creek Lane \& Triangle Lane/Park Entrance

| Movement | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LTR | LTR | LTR |
| Maximum Queue (ft) | 65 | 30 | 23 | 6 |
| Average Queue (ft) | 30 | 11 | 2 | 0 |
| 95th Queue (ft) | 52 | 35 | 12 | 4 |
| Link Distance (ft) | 359 | 92 | 336 | 111 |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

## Intersection: 6: Creek Lane \& TH 169

| Movement | EB | EB | NB |
| :--- | ---: | ---: | ---: |
| Directions Served | T | T | R |
| Maximum Queue (tt) | 18 | 6 | 56 |
| Average Queue (ft) | 1 | 0 | 22 |
| 95th Queue (ft) | 8 | 4 | 43 |
| Link Distance (tt) | 924 | 924 | 111 |
| Upstream Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |
| Storage Bay Dist (tt) |  |  |  |
| Storage Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |

## Intersection: 7: CR 9 \& Frontage Road

| Movement | WB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LR | LT | T | T |
| Maximum Queue (ft) | 79 | 17 | 169 | 178 |
| Average Queue (ft) | 31 | 1 | 41 | 47 |
| 95th Queue (ft) | 64 | 9 | 126 | 139 |
| Link Distance (ft) | 766 |  | 1086 | 1086 |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  | 100 |  |  |
| Storage Blk Time (\%) |  |  | 3 |  |
| Queuing Penalty (veh) |  |  | 6 |  |

## Intersection: 8: CR 9 \& CR 57/Valley View Drive

| Movement | EB | WB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LTR | LT | TR | LT | TR |
| Maximum Queue (ft) | 78 | 69 | 101 | 10 | 24 | 9 |
| Average Queue (ft) | 35 | 29 | 35 | 0 | 1 | 0 |
| 95th Queue (ft) | 60 | 58 | 79 | 0 | 8 | 4 |
| Link Distance (ft) | 796 | 393 | 1086 | 1086 | 657 | 657 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |

Intersection: 9: CR 9 \& Ervin Industrial Boulevard

| Movement | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LTR | LT | LT |
| Maximum Queue (tt) | 57 | 31 | 40 | 6 |
| Average Queue (tt) | 27 | 11 | 4 | 0 |
| 95th Queue (ft) | 49 | 32 | 22 | 4 |
| Link Distance (t) | 404 | 462 | 657 | 421 |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

## Network Summary

Network wide Queuing Penalty: 91

## Kimley»"Horn

2. DESIGN YEAR (2040) NO-ACTION SIMTRAFFIC REPORTS

## 1: TH 282/CR 9 \& TH 169 Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 1.9 | 0.6 | 1.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 75.3 | 58.8 | 21.8 | 77.5 | 43.9 | 8.9 | 58.7 | 41.0 | 40.5 | 60.4 | 72.2 |

1: TH 282/CR 9 \& TH 169 Performance by movement

| Movement | All |
| :--- | ---: |
| Denied Del/Veh (s) | 0.4 |
| Total Del/Veh (s) | 52.0 |

2: Driveway/Triangle Lane \& TH 282 Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 | 883.1 | 938.7 |
| Total Del/Veh (s) | 28.9 | 13.1 | 5.7 | 10.5 | 1.5 | 1.0 | 148.4 | 143.1 | 93.9 | 444.2 | 429.3 |

## 2: Driveway/Triangle Lane \& TH 282 Performance by movement

| Movement | All |
| :--- | ---: |
| Denied Del/Veh (s) | 93.3 |
| Total Del/Veh (s) | 32.2 |

3: Rademachers Driveway \& TH 282 Performance by movement

| Movement | EBT | EBR | WBL | WBT | NBL | NBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 | 0.0 |
| Total Del/Veh (s) | 4.7 | 0.8 | 12.0 | 2.1 | 56.1 | 15.4 | 4.8 |

4: Creek Lane \& TH 282 Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.0 | 3.6 | 2.0 | 2.0 | 3.7 | 1.0 | 3.5 | 4.1 | 0.1 |
| Total Del/Veh (s) | 52.3 | 19.6 | 2.1 | 50.4 | 23.3 | 17.4 | 34.3 | 25.7 | 2.3 | 22.8 | 27.0 |

## 4: Creek Lane \& TH 282 Performance by movement

| Movement | All |
| :--- | ---: |
| Denied Del/Veh (s) | 1.4 |
| Total Del/Veh (s) | 22.7 |

5: Creek Lane \& Triangle Lane/Park Entrance Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 196.8 | 134.8 | 205.3 | 0.1 | 9.7 | 0.1 | 4.0 | 5.8 | 7.6 | 0.0 | 0.0 |
| Total Del/Veh (s) | 411.3 | 285.0 | 409.3 | 35.8 | 86.2 | 191.9 | 74.4 | 94.5 | 85.0 | 1.1 | 0.1 |

## 5: Creek Lane \& Triangle Lane/Park Entrance Performance by movement

| Movement | All |
| :--- | ---: |
| Denied Del/Veh (s) | 78.6 |
| Total Del/Veh $(\mathrm{s})$ | 195.8 |

## 6: Creek Lane \& TH 169 Performance by movement

| Movement | EBT | EBR | WBT | NBT | NBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.2 | 0.0 | 0.3 | 0.1 |
| Total Del/Veh (s) | 17.5 | 8.9 | 0.9 | 24.9 | 91.6 | 16.0 |

7: CR 9 \& Frontage Road Performance by movement

| Movement | WBL | WBR | NBT | NBR | SBL | SBT | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 1499.8 | 1729.9 | 0.0 | 0.0 | 0.0 | 0.0 | 126.3 |
| Total Del/Veh (s) | 2439.1 | 2201.0 | 1.9 | 2.0 | 42.3 | 60.0 | 94.9 |

8: CR 9 \& CR 57/Valley View Drive Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 0.4 | 0.4 | 0.4 | 0.2 | 0.2 | 0.2 | 0.0 | 0.0 | 0.0 | 0.4 | 0.3 |
| Total Del/Veh (s) | 56.6 | 59.3 | 44.9 | 39.8 | 39.5 | 32.4 | 36.3 | 23.3 | 17.2 | 44.6 | 23.6 |

8: CR 9 \& CR 57/Valley View Drive Performance by movement

| Movement | All |
| :--- | ---: |
| Denied Del/Veh (s) | 0.2 |
| Total Del/Veh $(\mathrm{s})$ | 31.2 |

Total Network Performance

|  |  |
| :--- | ---: |
| Denied Del/Veh (s) | 80.4 |
| Total Del/Veh (s) | 122.0 |

## Intersection: 1: TH 282/CR 9 \& TH 169

| Movement | EB | EB | EB | EB | WB | WB | WB | WB | NB | NB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | T | T | R | L | T | T | R | L | T | TR | L |
| Maximum Queue (ft) | 398 | 697 | 675 | 400 | 224 | 341 | 337 | 124 | 200 | 356 | 349 | 181 |
| Average Queue ( ft ) | 248 | 400 | 397 | 179 | 96 | 215 | 213 | 48 | 165 | 216 | 233 | 134 |
| 95th Queue (ft) | 432 | 668 | 666 | 423 | 187 | 307 | 310 | 88 | 231 | 355 | 338 | 205 |
| Link Distance (ft) |  | 2157 | 2157 |  |  | 924 | 924 |  |  | 362 | 362 | 174 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  | 0 | 0 | 12 |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  | 2 | 1 | 41 |
| Storage Bay Dist (ft) | 300 |  |  | 300 | 550 |  |  | 350 | 150 |  |  |  |
| Storage Blk Time (\%) | 3 | 21 | 20 |  |  |  | 0 |  | 23 | 13 |  |  |
| Queuing Penalty (veh) | 19 | 56 | 70 |  |  |  | 1 |  | 62 | 38 |  |  |

Intersection: 1: TH 282/CR 9 \& TH 169

| Movement | SB | SB |
| :--- | ---: | ---: |
| Directions Served | T | TR |
| Maximum Queue (ft) | 217 | 204 |
| Average Queue (ft) | 184 | 181 |
| 95th Queue (ft) | 203 | 196 |
| Link Distance (ft) | 174 | 174 |
| Upstream Blk Time (\%) | 67 | 59 |
| Queuing Penalty (veh) | 223 | 198 |
| Storage Bay Dist (ft) |  |  |
| Storage Blk Time (\%) |  |  |

## Intersection: 2: Driveway/Triangle Lane \& TH 282

| Movement | EB | EB | WB | WB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LT | TR | L | T | R | LTR | LTR |
| Maximum Queue (ft) | 373 | 360 | 28 | 74 | 66 | 101 | 345 |
| Average Queue (ft) | 192 | 107 | 6 | 5 | 4 | 37 | 324 |
| 95th Queue (ft) | 374 | 317 | 23 | 45 | 34 | 89 | 363 |
| Link Distance (ft) | 362 | 362 |  | 383 |  | 241 | 315 |
| Upstream Blk Time (\%) | 1 | 1 |  |  |  |  | 94 |
| Queuing Penalty (veh) | 4 | 4 |  |  |  |  | 0 |
| Storage Bay Dist (ft) |  |  | 200 |  | 100 |  |  |
| Storage Blk Time (\%) |  |  |  | 0 |  |  |  |
| Queuing Penalty (veh) |  |  |  | 0 |  |  |  |

## Intersection: 3: Rademachers Driveway \& TH 282

| Movement | EB | EB | WB | WB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | TR | L | T | L | R |
| Maximum Queue (ft) | 292 | 126 | 64 | 27 | 103 | 68 |
| Average Queue (ft) | 72 | 4 | 22 | 0 | 37 | 25 |
| 95th Queue (ft) | 214 | 55 | 54 | 0 | 79 | 57 |
| Link Distance (ft) | 383 | 383 |  | 322 | 256 | 256 |
| Upstream Blk Time (\%) | 0 |  |  |  |  |  |
| Queuing Penalty (veh) | 0 |  |  |  |  |  |
| Storage Bay Dist (ft) |  |  | 100 |  |  |  |
| Storage Blk Time (\%) |  |  |  | 0 |  |  |
| Queuing Penalty (veh) |  |  |  | 0 |  |  |

Intersection: 4: Creek Lane \& TH 282

| Movement | EB | EB | EB | WB | WB | NB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | T | R | L | TR | L | T | R | L | TR |
| Maximum Queue (ft) | 199 | 340 | 84 | 300 | 585 | 198 | 280 | 63 | 38 | 60 |
| Average Queue (ft) | 54 | 265 | 10 | 122 | 348 | 120 | 52 | 4 | 7 | 13 |
| 95th Queue (ft) | 140 | 419 | 51 | 268 | 566 | 199 | 173 | 30 | 28 | 42 |
| Link Distance (ft) |  | 322 | 322 |  | 566 |  | 403 |  | 358 |  |
| Upstream BIk Time (\%) |  | 7 |  |  | 3 |  |  |  |  |  |
| Queuing Penalty (veh) |  | 34 |  |  | 0 |  |  |  |  |  |
| Storage Bay Dist (ft) | 100 |  |  | 200 |  | 100 |  | 100 | 100 |  |
| Storage Blk Time (\%) | 0 | 24 |  | 0 | 20 | 19 | 0 | 0 |  |  |
| Queuing Penalty (veh) | 2 | 12 |  | 1 | 24 | 19 | 1 | 0 |  |  |

## Intersection: 5: Creek Lane \& Triangle Lane/Park Entrance

| Movement | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LTR | LTR | LTR |
| Maximum Queue (ft) | 360 | 78 | 276 | 6 |
| Average Queue (ft) | 260 | 21 | 116 | 0 |
| 95th Queue (ft) | 473 | 65 | 273 | 4 |
| Link Distance (ft) | 359 | 92 | 336 | 111 |
| Upstream Blk Time (\%) | 48 | 5 | 6 |  |
| Queuing Penalty (veh) | 0 | 0 | 0 |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

## Intersection: 6: Creek Lane \& TH 169

| Movement | EB | EB | NB |
| :--- | ---: | ---: | ---: |
| Directions Served | T | T | R |
| Maximum Queue (tt) | 79 | 112 | 128 |
| Average Queue (tt) | 27 | 33 | 113 |
| 95th Queue (tt) | 63 | 84 | 131 |
| Link Distance (t) | 924 | 924 | 111 |
| Upstream Blk Time (\%) |  |  | 69 |
| Queuing Penalty (veh) |  | 124 |  |
| Storage Bay Dist (ft) |  |  |  |
| Storage Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |

## Intersection: 7: CR 9 \& Frontage Road

| Movement | WB | NB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LR | TR | LT | T | T |
| Maximum Queue (ft) | 785 | 28 | 200 | 621 | 559 |
| Average Queue (ft) | 765 | 1 | 122 | 289 | 252 |
| 95th Queue (ft) | 797 | 12 | 265 | 582 | 509 |
| Link Distance (ft) | 766 | 174 |  | 1086 | 1086 |
| Upstream Blk Time (\%) | 83 |  |  |  |  |
| Queuing Penalty (veh) | 0 |  |  |  |  |
| Storage Bay Dist (ft) |  |  | 100 |  |  |
| Storage Blk Time (\%) |  |  | 4 | 55 |  |
| Queuing Penalty (veh) |  |  | 12 | 171 |  |

## Intersection: 8: CR 9 \& CR 57/Valley View Drive

| Movement | EB | WB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LTR | LT | TR | LT | TR |
| Maximum Queue (ft) | 560 | 233 | 399 | 368 | 300 | 255 |
| Average Queue (ft) | 294 | 127 | 225 | 209 | 162 | 94 |
| 95th Queue (ft) | 508 | 206 | 360 | 340 | 279 | 210 |
| Link Distance (ft) | 796 | 392 | 1086 | 1086 | 295 | 295 |
| Upstream Blk Time (\%) | 0 |  |  |  | 1 | 0 |
| Queuing Penalty (veh) | 0 |  |  |  | 0 | 0 |
| Storage Bay Dist (ft) |  |  |  |  |  |  |

## Network Summary

Network wide Queuing Penalty: 1120

## 1: TH 282/CR 9 \& TH 169 Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 2.2 | 0.3 | 2.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.3 |
| Total Del/Veh (s) | 113.6 | 60.4 | 26.7 | 201.7 | 127.8 | 62.4 | 124.8 | 46.1 | 42.1 | 55.8 | 65.5 |

1: TH 282/CR 9 \& TH 169 Performance by movement

| Movement | All |
| :--- | ---: |
| Denied Del/Veh (s) | 0.3 |
| Total Del/Veh (s) | 87.1 |

2: Driveway/Triangle Lane \& TH 282 Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 55.9 | 149.3 | 111.1 | 1619.7 | 1271.0 | 1641.3 |
| Total Del/Veh (s) | 40.0 | 20.1 | 7.3 | 20.5 | 31.3 | 14.7 | 661.9 | 546.0 | 458.1 | 1573.3 | 1870.7 | 1507.1 |

2: Driveway/Triangle Lane \& TH 282 Performance by movement

| Movement | All |
| :--- | ---: |
| Denied Del/Veh (s) | 123.2 |
| Total Del/Veh (s) | 57.4 |

3: Rademachers Driveway \& TH 282 Performance by movement

| Movement | EBT | EBR | WBL | WBT | NBL | NBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.0 | 0.0 | 751.1 | 732.9 | 45.7 |
| Total Del/Veh (s) | 5.9 | 0.7 | 26.2 | 18.3 | 1021.6 | 52.6 | 30.5 |

4: Creek Lane \& TH 282 Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.0 | 59.4 | 61.1 | 56.9 | 86.0 | 124.8 | 76.2 | 4.0 | 0.3 |
| Total Del/Veh (s) | 94.2 | 16.1 | 2.0 | 59.8 | 40.9 | 35.5 | 163.7 | 83.7 | 43.2 | 42.5 | 62.8 |

## 4: Creek Lane \& TH 282 Performance by movement

| Movement | All |
| :--- | ---: |
| Denied Del/Veh (s) | 36.6 |
| Total Del/Veh (s) | 40.9 |

5: Creek Lane \& Triangle Lane/Park Entrance Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 0.1 | 0.1 | 0.2 | 0.1 | 0.2 | 0.1 | 0.1 | 0.1 | 0.1 | 0.0 | 0.0 |
| Total Del/Veh (s) | 5.3 | 6.0 | 2.9 | 3.0 | 4.9 | 2.2 | 1.9 | 0.7 | 0.3 | 0.9 | 0.2 |

## 5: Creek Lane \& Triangle Lane/Park Entrance Performance by movement

| Movement | All |
| :--- | :---: |
| Denied Del/Veh (s) | 0.1 |
| Total Del/Veh (s) | 2.3 |

## 6: Creek Lane \& TH 169 Performance by movement

| Movement | EBT | EBR | WBT | NBT | NBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 4.1 | 0.0 | 0.0 | 2.6 |
| Total Del/Veh (s) | 15.1 | 7.8 | 67.0 | 1.0 | 17.0 | 47.4 |

7: CR 9 \& Frontage Road Performance by movement

| Movement | WBL | WBR | NBT | NBR | SBL | SBT | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 1879.8 | 1978.0 | 0.0 | 0.0 | 0.0 | 3.3 | 212.4 |
| Total Del/Veh (s) | 3396.9 | 3066.1 | 1.8 | 1.9 | 273.5 | 295.5 | 234.4 |

8: CR 9 \& CR 57/Valley View Drive Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 99.0 | 124.9 | 107.1 | 0.2 | 0.2 | 0.2 | 0.0 | 0.0 | 0.0 | 984.8 | 941.7 |
| Total Del/Veh (s) | 110.2 | 116.7 | 124.6 | 54.5 | 50.6 | 35.7 | 84.6 | 14.9 | 14.5 | 142.1 | 132.8 |

8: CR 9 \& CR 57/Valley View Drive Performance by movement

|  | All |
| :--- | ---: |
| Movement | 510.0 |
| Denied Del/Veh (s) | 91.4 |

Total Network Performance

|  |  |
| :--- | :--- |
| Denied Del/Veh (s) | 313.2 |
| Total Del/Veh (s) | 234.3 |

## Intersection: 1: TH 282/CR 9 \& TH 169

| Movement | EB | EB | EB | EB | WB | WB | WB | WB | NB | NB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | T | T | R | L | T | T | R | L | T | TR | L |
| Maximum Queue (ft) | 336 | 509 | 476 | 366 | 650 | 952 | 960 | 450 | 200 | 398 | 400 | 174 |
| Average Queue ( ft ) | 103 | 293 | 282 | 129 | 518 | 835 | 836 | 302 | 199 | 371 | 282 | 91 |
| 95th Queue (ft) | 237 | 463 | 453 | 286 | 838 | 1105 | 1103 | 616 | 202 | 405 | 459 | 160 |
| Link Distance (ft) |  | 2157 | 2157 |  |  | 924 | 924 |  |  | 362 | 362 | 174 |
| Upstream Blk Time (\%) |  |  |  |  |  | 19 | 18 |  | 40 | 2 | 1 |  |
| Queuing Penalty (veh) |  |  |  |  |  | 168 | 164 |  |  | 219 | 11 | 8 |
| Storage Bay Dist (ft) | 300 |  |  | 300 | 550 |  |  | 350 | 150 |  |  |  |
| Storage Blk Time (\%) | 0 | 8 | 7 | 0 | 11 | 45 | 56 |  | 78 | 11 |  |  |
| Queuing Penalty (veh) | 0 | 6 | 22 | 2 | 78 | 98 | 92 |  | 235 | 40 |  |  |

Intersection: 1: TH 282/CR 9 \& TH 169

| Movement | SB | SB |
| :--- | ---: | ---: |
| Directions Served | T | TR |
| Maximum Queue (ft) | 201 | 205 |
| Average Queue (ft) | 181 | 181 |
| 95th Queue (ft) | 193 | 195 |
| Link Distance (ft) | 174 | 174 |
| Upstream Blk Time (\%) | 72 | 68 |
| Queuing Penalty (veh) | 380 | 361 |
| Storage Bay Dist (ft) |  |  |
| Storage Blk Time (\%) |  |  |

## Intersection: 2: Driveway/Triangle Lane \& TH 282

| Movement | EB | EB | WB | WB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LT | TR | L | T | R | LTR | LTR |
| Maximum Queue (ft) | 388 | 410 | 245 | 399 | 200 | 218 | 342 |
| Average Queue (ft) | 264 | 203 | 25 | 349 | 39 | 122 | 318 |
| 95th Queue (ft) | 478 | 473 | 145 | 519 | 168 | 259 | 337 |
| Link Distance (ft) | 362 | 362 |  | 383 |  | 241 | 315 |
| Upstream Blk Time (\%) | 8 | 6 |  | 22 |  | 18 | 100 |
| Queuing Penalty (veh) | 63 | 45 |  | 231 |  | 0 | 0 |
| Storage Bay Dist (ft) |  |  | 200 |  | 100 |  |  |
| Storage Blk Time (\%) |  |  |  | 42 |  |  |  |
| Queuing Penalty (veh) |  |  |  | 36 |  |  |  |

## Intersection: 3: Rademachers Driveway \& TH 282

| Movement | EB | EB | WB | WB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | TR | L | T | L | R |
| Maximum Queue (ft) | 345 | 195 | 200 | 339 | 270 | 228 |
| Average Queue (ft) | 81 | 11 | 73 | 233 | 227 | 94 |
| 95th Queue (ft) | 277 | 108 | 185 | 454 | 315 | 276 |
| Link Distance (ft) | 383 | 383 |  | 322 | 256 | 256 |
| Upstream BIk Time (\%) | 0 | 0 |  | 13 | 70 | 27 |
| Queuing Penalty (veh) | 4 | 0 |  | 144 | 0 | 0 |
| Storage Bay Dist (ft) |  |  | 100 |  |  |  |
| Storage Blk Time (\%) |  |  | 2 | 28 |  |  |
| Queuing Penalty (veh) |  |  | 17 | 24 |  |  |

Intersection: 4: Creek Lane \& TH 282

| Movement | EB | EB | EB | WB | WB | NB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | T | R | L | TR | L | T | R | L | TR |
| Maximum Queue (ft) | 199 | 336 | 67 | 300 | 607 | 200 | 392 | 144 | 69 | 134 |
| Average Queue (ft) | 70 | 259 | 6 | 138 | 496 | 153 | 181 | 29 | 24 | 52 |
| 95th Queue (ft) | 165 | 400 | 38 | 320 | 713 | 238 | 481 | 103 | 60 | 112 |
| Link Distance (ft) |  | 322 | 322 |  | 566 |  | 403 |  | 358 |  |
| Upstream Blk Time (\%) |  | 6 |  |  | 25 |  | 25 |  |  |  |
| Queuing Penalty (veh) |  | 42 |  |  | 0 |  | 0 |  |  |  |
| Storage Bay Dist (ft) | 100 |  |  | 200 |  | 100 |  | 100 | 100 |  |
| Storage Blk Time (\%) | 10 | 22 |  | 0 | 35 | 57 | 0 | 3 |  | 6 |
| Queuing Penalty (veh) | 121 | 18 |  | 0 | 35 | 69 | 0 | 6 | 2 |  |

## Intersection: 5: Creek Lane \& Triangle Lane/Park Entrance

| Movement | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LTR | LTR | LTR |
| Maximum Queue (ft) | 70 | 35 | 22 | 10 |
| Average Queue (ft) | 31 | 13 | 1 | 0 |
| 95th Queue (ft) | 52 | 38 | 10 | 5 |
| Link Distance (ft) | 359 | 92 | 336 | 111 |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

## Intersection: 6: Creek Lane \& TH 169

| Movement | EB | EB | WB | WB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | T | T | R |
| Maximum Queue (ft) | 64 | 72 | 1101 | 1077 | 90 |
| Average Queue (ft) | 8 | 10 | 495 | 479 | 30 |
| 95th Queue (ft) | 40 | 42 | 1428 | 1393 | 65 |
| Link Distance (ft) | 924 | 924 | 1667 | 1667 | 111 |
| Upstream Blk Time (\%) |  |  | 5 | 5 | 0 |
| Queuing Penalty (veh) |  |  | 0 | 0 | 0 |
| Storage Bay Dist (ft) |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |

## Intersection: 7: CR 9 \& Frontage Road

| Movement | WB | NB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LR | TR | LT | T | T |
| Maximum Queue (ft) | 782 | 21 | 200 | 1130 | 1134 |
| Average Queue (ft) | 772 | 1 | 147 | 1100 | 1100 |
| 95th Queue (ft) | 783 | 13 | 285 | 1119 | 1119 |
| Link Distance (ft) | 766 | 174 |  | 1086 | 1086 |
| Upstream Blk Time (\%) | 100 |  |  | 33 | 32 |
| Queuing Penalty (veh) | 0 |  |  | 240 | 236 |
| Storage Bay Dist (ft) |  |  | 100 |  |  |
| Storage Blk Time (\%) |  |  | 0 | 78 |  |
| Queuing Penalty (veh) |  |  | 2 | 394 |  |

## Intersection: 8: CR 9 \& CR 57/Valley View Drive

| Movement | EB | WB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LTR | LT | TR | LT | TR |
| Maximum Queue (tt) | 701 | 244 | 401 | 352 | 347 | 361 |
| Average Queue (ft) | 462 | 103 | 216 | 121 | 329 | 331 |
| 95th Queue (ft) | 830 | 203 | 427 | 282 | 339 | 348 |
| Link Distance (tt) | 796 | 393 | 1086 | 1086 | 312 | 312 |
| Upstream Blk Time (\%) | 17 |  |  |  | 91 | 77 |
| Queuing Penalty (veh) | 0 |  |  |  | 0 | 0 |
| Storage Bay Dist (tt) |  |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |
| Network Summary |  |  |  |  |  |  |

## Kimley»"Horn

## 3. DESIGN YEAR (2040) CONCEPT 1 SIMTRAFFIC REPORTS

## 1: Site Access \& TH 282 Performance by movement

| Movement | EBT | EBR | WBL | WBT | NBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.2 | 0.1 | 0.1 | 0.0 |
| Total Del/Veh (s) | 0.5 | 0.4 | 18.8 | 4.0 | 8.9 | 2.6 |

5: Creek Ln N \& Triangle Ln N Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.1 | 0.0 | 0.1 | 0.1 | 0.1 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 8.9 | 7.6 | 3.1 | 6.2 | 6.6 | 4.7 | 2.2 | 0.9 | 0.3 | 2.9 |

8: CR 9 \& CR 57/Valley View Drive Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 3.5 | 1.1 | 3.5 | 3.7 | 0.7 | 3.7 | 0.0 | 0.0 | 0.0 | 3.2 | 0.2 |
| Total Del/Veh (s) | 22.8 | 33.1 | 7.5 | 21.3 | 25.7 | 8.7 | 13.5 | 12.5 | 3.4 | 15.3 | 16.4 |

8: CR 9 \& CR 57/Valley View Drive Performance by movement

| Movement | All |
| :--- | ---: |
| Denied Del/Veh (s) | 1.3 |
| Total Del/Veh (s) | 13.6 |

9: TH 282 \& Triangle Ln N Performance by movement

| Movement | EBT | WBT | WBR | SBT | SBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 0.8 | 1.3 | 1.4 | 0.4 | 16.4 | 1.8 |

## 29: TH 169 EB Off-Ramp \& CR 9 Performance by movement

| Movement | EBL | EBR | NBT | SBT | All |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 3.3 | 1.0 | 0.0 | 0.0 | 0.5 |
| Total Del/Veh (s) | 45.1 | 17.2 | 4.2 | 5.7 | 10.9 |

Total Zone Performance

|  |  |
| :--- | :---: |
| Denied Del/Veh (s) | 2.0 |
| Total Del/Veh (s) | 21.3 |

Intersection: 1: Site Access \& TH 282

| Movement | EB | EB | EB | WB | WB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | R | L | T | R |
| Maximum Queue (ft) | 9 | 4 | 35 | 103 | 10 | 74 |
| Average Queue (ft) | 0 | 0 | 2 | 32 | 0 | 33 |
| 95th Queue (ft) | 3 | 3 | 16 | 74 | 8 | 59 |
| Link Distance (ft) | 239 | 239 |  |  | 452 | 195 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  | 135 | 200 |  |  |
| Storage Bay Dist (ft) |  |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |

Intersection: 5: Creek Ln N \& Triangle Ln N

| Movement | EB | EB | WB | NB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | LTR | L |
| Maximum Queue (ft) | 84 | 56 | 31 | 10 |
| Average Queue (ft) | 35 | 32 | 12 | 1 |
| 95th Queue (ft) | 64 | 51 | 36 | 7 |
| Link Distance (ft) | 808 | 808 | 174 |  |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  | 100 |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

## Intersection: 8: CR 9 \& CR 57/Valley View Drive

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | R | L | T | R | L | T | R | L | T | T |
| Maximum Queue (ft) | 132 | 69 | 146 | 176 | 69 | 58 | 191 | 338 | 84 | 76 | 152 | 148 |
| Average Queue (ft) | 61 | 20 | 61 | 86 | 21 | 19 | 74 | 133 | 34 | 26 | 71 | 64 |
| 95th Queue (ft) | 111 | 50 | 108 | 147 | 53 | 45 | 129 | 250 | 71 | 58 | 123 | 118 |
| Link Distance (ft) |  | 783 |  |  | 903 |  |  | 1152 | 1152 |  | 1263 | 1263 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (ft) | 250 |  | 250 | 300 |  | 300 | 300 |  |  | 275 |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |  | 0 |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  | 1 |  |  |  |  |

## Intersection: 8: CR 9 \& CR 57/Valley View Drive

| Movement | SB |
| :--- | ---: |
| Directions Served | R |
| Maximum Queue (ft) | 40 |
| Average Queue (ft) | 13 |
| 95th Queue (ft) | 31 |
| Link Distance (ft) |  |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) | 275 |
| Storage Blk Time (\%) |  |
| Queuing Penalty (veh) |  |

## Intersection: 9: TH 282 \& Triangle Ln N

| Movement | WB | WB | SB |
| :--- | ---: | ---: | ---: |
| Directions Served | T | T | R |
| Maximum Queue (ft) | 17 | 44 | 141 |
| Average Queue (ft) | 1 | 2 | 48 |
| 95th Queue (ft) | 12 | 20 | 99 |
| Link Distance (ft) | 239 | 239 | 808 |
| Upstream Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |
| Storage Bay Dist (ft) | 0 |  |  |
| Storage Blk Time (\%) |  | 0 |  |

Intersection: 29: TH 169 EB Off-Ramp \& CR 9

| Movement | EB | EB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | R | T | T | T | T |
| Maximum Queue (ft) | 283 | 302 | 109 | 223 | 206 | 224 |
| Average Queue (ft) | 165 | 113 | 26 | 81 | 64 | 69 |
| 95th Queue (ft) | 258 | 213 | 76 | 170 | 154 | 157 |
| Link Distance (ft) |  | 845 | 212 | 212 | 303 | 303 |
| Upstream Blk Time (\%) |  |  | 0 | 0 |  |  |
| Queuing Penalty (veh) |  |  | 0 | 2 |  |  |
| Storage Bay Dist (ft) | 300 |  |  |  |  |  |
| Storage Blk Time (\%) | 0 | 0 |  |  |  |  |
| Queuing Penalty (veh) | 1 | 0 |  |  |  |  |

Zone Summary
Zone wide Queuing Penalty: 3

## 1: Site Access \& TH 282 Performance by movement

| Movement | EBT | EBR | WBL | WBT | NBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.4 | 0.1 | 0.2 | 0.1 |
| Total Del/Veh (s) | 1.2 | 0.9 | 34.7 | 3.5 | 20.9 | 3.8 |

5: Creek Ln N \& Triangle Ln N Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 8.5 | 8.6 | 3.3 | 10.7 | 5.6 | 4.9 | 2.5 | 1.1 | 0.6 | 2.6 |

8: CR 9 \& CR 57/Valley View Drive Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 3.5 | 1.0 | 3.5 | 3.8 | 0.5 | 3.8 | 0.0 | 0.0 | 0.0 | 2.4 | 0.4 |
| Total Del/Veh (s) | 37.8 | 44.2 | 15.6 | 39.5 | 40.2 | 6.8 | 23.4 | 8.7 | 2.3 | 13.8 | 22.0 |

8: CR 9 \& CR 57/Valley View Drive Performance by movement

| Movement | All |
| :--- | ---: |
| Denied Del/Veh (s) | 1.1 |
| Total Del/Veh (s) | 19.5 |

9: TH 282 \& Triangle Ln N Performance by movement

| Movement | EBT | WBT | WBR | SBT | SBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 1.3 | 1.1 | 1.2 | 0.3 | 13.1 | 1.6 |

## 29: TH 169 EB Off Ramp \& CR 9 Performance by movement

| Movement | EBL | EBR | NBT | SBT | All |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 3.5 | 0.5 | 0.0 | 0.0 | 0.1 |
| Total Del/Veh (s) | 50.2 | 21.5 | 3.8 | 10.7 | 10.5 |

Total Zone Performance

|  |  |
| :--- | ---: |
| Denied Del/Veh (s) | 1.4 |
| Total Del/Veh (s) | 25.9 |

Intersection: 1: Site Access \& TH 282

| Movement | EB | EB | EB | WB | WB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | R | L | T | R |
| Maximum Queue (ft) | 88 | 98 | 18 | 141 | 5 | 163 |
| Average Queue (ft) | 6 | 5 | 1 | 58 | 0 | 64 |
| 95th Queue (ft) | 44 | 41 | 10 | 118 | 4 | 123 |
| Link Distance (ft) | 239 | 239 |  |  | 452 | 195 |
| Upstream Blk Time (\%) |  | 0 |  |  |  | 0 |
| Queuing Penalty (veh) |  | 0 |  |  |  | 0 |
| Storage Bay Dist (ft) |  |  | 135 | 200 |  |  |
| Storage Blk Time (\%) |  | 0 |  | 0 |  |  |
| Queuing Penalty (veh) |  | 0 |  | 0 |  |  |

## Intersection: 5: Creek Ln N \& Triangle Ln N

| Movement | EB | EB | WB |
| :--- | ---: | ---: | ---: |
| Directions Served | L | TR | LTR |
| Maximum Queue (ft) | 52 | 72 | 35 |
| Average Queue (ft) | 23 | 34 | 10 |
| 95th Queue (ft) | 46 | 56 | 33 |
| Link Distance (ft) | 808 | 808 | 120 |
| Upstream Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |
| Storage Bay Dist (ft) |  |  |  |
| Storage Blk Time (\%) |  |  |  |

## Intersection: 8: CR 9 \& CR 57/Valley View Drive

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | R | L | T | R | L | T | R | L | T | T |
| Maximum Queue (ft) | 135 | 96 | 210 | 173 | 85 | 44 | 260 | 264 | 60 | 95 | 339 | 338 |
| Average Queue (ft) | 57 | 31 | 90 | 78 | 32 | 15 | 117 | 97 | 18 | 23 | 177 | 187 |
| 95th Queue (ft) | 111 | 70 | 161 | 144 | 70 | 37 | 203 | 202 | 47 | 63 | 283 | 296 |
| Link Distance (ft) |  | 783 |  |  | 903 |  |  | 1153 | 1153 |  | 1263 | 1263 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (ft) | 250 |  | 250 | 300 |  | 300 | 300 |  |  | 275 |  |  |
| Storage Blk Time (\%) |  |  | 0 |  |  |  | 0 | 0 |  |  | 1 | 1 |
| Queuing Penalty (veh) |  |  | 0 |  |  |  | 0 | 0 |  |  | 1 | 1 |

Intersection: 8: CR 9 \& CR 57/Valley View Drive

| Movement | SB |
| :--- | ---: |
| Directions Served | R |
| Maximum Queue (ft) | 244 |
| Average Queue (ft) | 26 |
| 95th Queue ( ft ) | 86 |
| Link Distance (ft) |  |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist ( ft ) | 275 |
| Storage Blk Time (\%) | 0 |
| Queuing Penalty (veh) | 0 |

## Intersection: 9: TH 282 \& Triangle Ln N

| Movement | WB | SB |
| :--- | ---: | ---: |
| Directions Served | T | R |
| Maximum Queue (ft) | 12 | 114 |
| Average Queue (ft) | 0 | 44 |
| 95th Queue (ft) | 6 | 87 |
| Link Distance (ft) | 239 | 808 |
| Upstream Blk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |
| Storage Bay Dist (ft) |  |  |
| Storage Blk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |

Intersection: 29: TH 169 EB Off Ramp \& CR 9

| Movement | EB | EB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | R | T | T | T | T |
| Maximum Queue (ft) | 150 | 237 | 160 | 178 | 320 | 323 |
| Average Queue (ft) | 53 | 123 | 45 | 63 | 181 | 181 |
| 95th Queue (ft) | 112 | 209 | 119 | 136 | 350 | 354 |
| Link Distance (ft) |  | 845 | 212 | 212 | 303 | 303 |
| Upstream Blk Time (\%) |  |  |  | 0 | 2 | 1 |
| Queuing Penalty (veh) |  |  |  | 0 | 12 | 10 |
| Storage Bay Dist (ft) | 300 |  |  |  |  |  |
| Storage Blk Time (\%) |  | 0 |  |  |  |  |
| Queuing Penalty (veh) |  | 0 |  |  |  |  |

Zone Summary
Zone wide Queuing Penalty: 25

## Kimley»"Horn

4. DESIGN YEAR (2040) CONCEPT 1 RODEL REPORTS

## Scheme Summary

## Control Data

Control Data and Model Parameters

| TH 169 \& 2nd St Interchange | 2040 PHF Flow Profile (veh) |
| :--- | :--- |
| 2nd St/Creek Ln 2040 AM peak hour | 7.5 min Time Slice |
| Rodel-Win1 | Queuing Delays (sec) |
| Right Hand Drive | Daylight conditions |
| AM Peak Hour | Peak 60/15 min Results |
| Full Geometry | Output flows: Vehicles |
| English Units (ft) | $50 \%$ Confidence Level |

## Available Data

| Entry Capacity Calibrated | No |
| :--- | :---: |
| Entry Capacity Modified | No |
| Crosswalks | No |
| Flows Factored | No |
| Approach/Exit Road Capacity Calibrated | No |
| Accidents | No |
| Accident Costs | No |
| Bypass Model | Yes |
| Bypass Calibration | No |
| Global Results | Yes |

2040 AM Peak
50\% Confidence Level
Daylight conditions

Project: TH 169 \& 2nd St Interchange Scheme: 2nd St/Creek Ln 2040 AM peak hour Rodel-Win1 - Full Geometry

## Operational Data

## Main Geometry (ft)

Approach and Entry Geometry

| Leg | Leg Names | Approach <br> Bearing <br> (deg) | Grade <br> Separation <br> $\mathbf{G}$ | Half Width <br> $\mathbf{V}$ | Approach <br> Lanes <br> $\mathbf{n}$ | Entry <br> Width <br> $\mathbf{E}$ | Entry <br> Lanes <br> $\mathbf{n}$ | Flare <br> Length <br> $\mathbf{L}^{\prime}$ | Entry <br> Radius <br> $\mathbf{R}$ | Entry <br> Angle <br> $\boldsymbol{?}$ |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 0 | 0 | 24.00 | 2 | 28.00 | 2 | 164.00 | 66.00 | 30.00 |
| 2 | Creek Ln EB | 90 | 0 | 12.00 | 1 | 14.00 | 1 | 164.00 | 66.00 | 30.00 |
| 3 | 2nd St NB | 180 | 0 | 24.00 | 2 | 28.00 | 2 | 164.00 | 66.00 | 30.00 |
| 4 | Creek Ln WB | 270 | 0 | 12.00 | 1 | 14.00 | 1 | 164.00 | 66.00 | 30.00 |

Circulating and Exit Geometry

| Leg | Leg Names | Inscribed <br> Diameter <br> D | Circulating <br> Width <br> C | Circulating <br> Lanes <br> nc | Exit <br> Width <br> Ex | Exit <br> Lanes <br> nex | Exit <br> Half Width <br> Vx | Exit Half <br> Width Lanes <br> nvx |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 164.00 | 15.00 | 1 | 28.00 | 2 | 24.00 | 2 |
| 2 | Creek Ln EB | 164.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |
| 3 | 2nd St NB | 164.00 | 15.00 | 1 | 14.00 | 1 | 12.00 | 1 |
| 4 | Creek Ln WB | 164.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |

Capacity Modifiers and Capacity Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity |  | Entry Calibration |  | Approach Road |  |  | Exit Road |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Capacity + or - | XWalk <br> Factor | Intercept + or - | Slope Factor | V <br> (ft) | Default Capacity | Calib Capacity | $\begin{gathered} \text { V } \\ (\mathrm{ft}) \end{gathered}$ | Default Capacity | Calib Capacity |
|  | 2nd St SB | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 24.00 | 3584 | 0 |
| 2 | Creek Ln EB | 0 | 1.000 | 0 | 1.000 | 20.00 | 1792 | 0 | 12.00 | 1792 | 0 |
| 3 | 2nd St NB | 0 | 1.000 | 0 | 1.000 | 20.00 | 3584 | 0 | 12.00 | 1792 | 0 |
| 4 | Creek Ln WB | 0 | 1.000 | 0 | 1.000 | 20.00 | 1792 | 0 | 12.00 | 1792 | 0 |

## Bypass Geometry

Bypass Approach Geometry (ft)

| Leg | Leg Names | Bypass <br> Type | Bypass <br> Flows | V | nv | Vb | nvb | Vt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | Yield | 240 | 24 | 2 | 12 | 1 | 24 |

Bypass Entry and Exit Geometry (ft)

| Leg | Leg Names | Eb | neb | Lb | Lt | Rb | Phib | Leg | Leg Names |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2nd St SB | 12 | 1 | 0 | 130 | 66.00005 <br> 914 | 30 | 2 | Creek Ln EB |
| nex | 1 | Nmx |  |  |  |  |  |  |  |

Bypass Entry Capacity Modifiers and Calibration (veh/hr)

| Leg | Leg Names | Capacity <br> + or - | Eross Walk <br> Factor | Intercept <br> + or - | Calibration <br> Slope |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2nd St SB | 0 | 1.000 | 0 | 1.000 |

## Traffic Flow Data (veh/hr)

## 2040 AM Peak Peak Hour Flows

| Leg | Leg Names | Turning Flows |  |  |  |  | Flow Modifiers |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks \% | Flow Factor | Peak Hour Factor |
| 1 | 2nd St SB | 45 | 255 | 765 | 0 | 240 | 5.0 | 1.00 | 0.9 |
| 2 | Creek Ln EB | 0 | 170 | 100 | 60 | 0 | 5.0 | 1.00 | 0.9 |
| 3 | 2nd St NB | 0 | 120 | 730 | 85 | 0 | 5.0 | 1.00 | 0.9 |
| 4 | Creek Ln WB | 0 | 75 | 15 | 20 | 0 | 5.0 | 1.00 | 0.9 |

## Operational Results

## 2040 AM Peak - 60 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | 2nd St SB | Yield | 1065 | 240 | 210 | 210 | 964 | 1985 | 952 | 0.5449 | 0.2561 |
| 2 | Creek Ln EB | None | 330 |  | 1140 |  | 375 | 693 |  | 0.4905 |  |
| 3 | 2nd St NB | None | 935 |  | 570 |  | 900 | 1632 |  | 0.5839 |  |
| 4 | Creek Ln WB | None | 110 |  | 1064 |  | 440 | 720 |  | 0.1561 |  |

Delays, Queues and Level of Service

| Leg | Leg Names |  | Bypass | Average Delay (sec) |  | $95 \%$ Queue (veh) |  | Level of Service <br> Type |  | Entry |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |  |  |
| 1 | 2nd St SB | Yield | 4.88 | 5.00 | 4.90 | 4.64 | 1.03 | A | A | A |
| 2 | Creek Ln EB | None | 9.01 |  | 9.01 | 2.91 |  | A | A |  |
| 3 | 2nd St NB | None | 5.31 |  | 5.31 | 4.79 |  | A | A |  |
| 4 | Creek Ln WB | None | 5.51 |  | 5.51 | 0.54 | A |  |  |  |

## 2040 AM Peak - 15 minutes

Flows and Capacity

| Leg | Leg Names | Bypass <br> Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit <br> Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | 2nd St SB | Yield | 1183 | 267 | 233 | 233 | 1069 | 1963 | 941 | 0.6093 | 0.2865 |
| 2 | Creek Ln EB | None | 367 |  | 1265 |  | 416 | 649 |  | 0.5763 |  |
| 3 | 2nd St NB | None | 1039 |  | 631 |  | 998 | 1571 |  | 0.6690 |  |
| 4 | Creek Ln WB | None | 122 |  | 1180 |  | 488 | 679 |  | 0.1821 |  |

Delays, Queues and Level of Service

| Leg | Leg Names |  | Bypass | Average Delay (sec) |  | $95 \%$ Queue (veh) |  | Level of Service <br> Type |  | Entry |
| :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |  |  |
| 1 | 2nd St SB | Yield | 5.20 | 5.03 | 5.17 | 4.64 | 1.03 | A | A | A |
| 2 | Creek Ln EB | None | 10.04 |  | 10.04 | 2.91 |  | B | B |  |
| 3 | 2nd St NB | None | 5.98 |  | 5.98 | 4.79 |  | A |  |  |
| 4 | Creek Ln WB | None | 5.68 |  | 5.68 | 0.54 | A | A |  |  |

2040 AM Peak 50\% Confidence Level Daylight conditions

Project: TH 169 \& 2nd St Interchange Scheme: 2nd St/Creek Ln 2040 AM peak hour Rodel-Win1 - Full Geometry

## Approach Flow Profile

2040 AM Peak - Approach Flows (Veh / Hour)

| Time Slice | 2nd St SB | Creek Ln EB | 2nd St NB | Creek Ln WB |
| :--- | :---: | :---: | :---: | :---: |
| $0.0-7.5$ | 157.08 | 39.72 | 112.55 | 13.24 |
| $7.5-15.0$ | 157.08 | 39.72 | 112.55 | 13.24 |
| $15.0-22.5$ | 157.08 | 39.72 | 112.55 | 13.24 |
| $22.5-30.0$ | 181.25 | 45.83 | 129.86 | 15.28 |
| $30.0-37.5$ | 181.25 | 45.83 | 129.86 | 15.28 |
| $37.5-45.0$ | 157.08 | 39.72 | 112.55 | 13.24 |
| $45.0-52.5$ | 157.08 | 39.72 | 112.55 | 13.24 |
| $52.5-60.0$ | 157.08 | 39.72 | 112.55 | 13.24 |
| Peak 15 min | 181.25 | 45.83 | 129.86 | 15.28 |
| Peak 60 min | 163.12 | 41.25 | 116.88 | 13.75 |

## Exit Flow Profile

2040 AM Peak - Exit Flows (Veh / Hour)

| Time Slice | 2nd St SB | Creek Ln EB | 2nd St NB | Creek Ln WB |
| :--- | :---: | :---: | :---: | :---: |
| $0.0-7.5$ | 115.96 | 45.06 | 108.19 | 52.88 |
| $7.5-15.0$ | 116.15 | 45.14 | 108.33 | 52.96 |
| $15.0-22.5$ | 116.16 | 45.14 | 108.33 | 52.96 |
| $22.5-30.0$ | 133.30 | 51.92 | 124.55 | 60.82 |
| $30.0-37.5$ | 134.00 | 52.08 | 124.99 | 61.10 |
| $37.5-45.0$ | 116.52 | 45.25 | 108.56 | 53.11 |
| $45.0-52.5$ | 116.17 | 45.14 | 108.34 | 52.97 |
| $52.5-60.0$ | 116.16 | 45.14 | 108.33 | 52.96 |
| $0-60$ | 964 | 375 | 900 | 440 |
| $\%$ Trucks | 5.00 | 5.00 | 5.00 | 5.00 |

2040 AM Peak
50\% Confidence Level
Daylight conditions

Project: TH 169 \& 2nd St Interchange Scheme: 2nd St/Creek Ln 2040 AM peak hour

Rodel-Win1 - Full Geometry

## Economics

## Economic Input Data

## 2040 - Vehicle Delay Parameters

| Peaks | Peak / Day | Days / Year | Delay Cost <br> (\$ / hour) |
| :---: | :---: | :---: | :---: |
| AM Peak | 1 | 325 | 15.00 |
| OFF Peak | 14 | 325 | 15.00 |
| PM Peak | 1 | 325 | 15.00 |

2040 - Accident Severity Proportions and Costs

| Accident Type | Proportion (\%) | Cost (\$) |
| :--- | :---: | :---: |
| Fatal Vehicle Accident | 0.3 | 0 |
| Incapacitating Vehicle Accident | 17.7 | 0 |
| Non-incapacitating Vehicle Accident | 82 | 0 |
| Damage Only Vehicle Accident | 100 | 0 |
| Pedestrian Injury Accident | 100 | 0 |

## Economics - Results Data

2040 Delay and Accident Costs

|  | Delay Costs <br> Delays <br> Veh.hrs | Costs <br> (\$) | Accident <br> Types | Accident Costs <br> Annual <br> Accidents | Accident <br> Costs | Total Costs <br> Cost <br> Type | Costs <br> (\$/year) |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM | 1348.31 | 20225 | Vehicles Injury | 0.00 | 0 | Vehicle Delay Cost | 20225 |
| OFF | 0.00 | 0 | Vehicles DO | 0.00 | 0 | Vehicle Injury Acc Cost | 0 |
| PM | 0.00 | 0 | Pedestrians | 0.00 | 0 | Vehicle DO Acc Cost | 0 |
|  |  |  |  |  |  | Pedestrian Accident Cost | 0 |
|  |  |  |  |  |  | Total Accident Cost | 0 |
| Total | 1348.31 | 20225 | Totals | 0.00 | 0 | TOTAL COST | 20225 |

## Global Results

## Performance and Accidents

2040 AM Peak Global Performance

| Parameter | Units | Entries | Bypasses | Total |
| :--- | :---: | :---: | :---: | :---: |
| Arrive Flows | $\mathrm{veh} / \mathrm{hr}$ | 2440 | 240 | 2680 |
| Capacity | $\mathrm{veh} / \mathrm{hr}$ | 5031 | 952 | 5983 |
| Average Delay | $\mathrm{sec} / \mathrm{veh}$ | 5.63 | 5.00 | 5.57 |
| L.O.S. (Signal) | $\mathrm{A}-\mathrm{F}$ | A | A | A |
| L.O.S. (Unsig) | $\mathrm{A}-\mathrm{F}$ | A | A | A |
| Total Delay | veh.hrs | 3.82 | 0.33 | 4.15 |

## Scheme Summary

## Control Data

## Control Data and Model Parameters

| TH 169 \& 2nd St Interchange | 2040 PHF Flow Profile (veh) |
| :--- | :--- |
| 2nd St/Creek Ln 2040 PM peak hour | 7.5 min Time Slice |
| Rodel-Win1 | Queuing Delays (sec) |
| Right Hand Drive | Daylight conditions |
| PM Peak Hour | Peak 60/15 min Results |
| Full Geometry | Output flows: Vehicles |
| English Units (ft) | $50 \%$ Confidence Level |

## Available Data

| Entry Capacity Calibrated | No |
| :--- | :---: |
| Entry Capacity Modified | No |
| Crosswalks | No |
| Flows Factored | No |
| Approach/Exit Road Capacity Calibrated | No |
| Accidents | No |
| Accident Costs | No |
| Bypass Model | Yes |
| Bypass Calibration | No |
| Global Results | Yes |

## Operational Data

Main Geometry (ft)

## Approach and Entry Geometry

| Leg | Leg Names | Approach <br> Bearing <br> (deg) | Grade <br> Separation <br> $\mathbf{G}$ | Half Width <br> $\mathbf{V}$ | Approach <br> Lanes <br> $\mathbf{n}$ | Entry <br> Width <br> $\mathbf{E}$ | Entry <br> Lanes <br> $\mathbf{n}$ | Flare <br> Length <br> $\mathbf{L}^{\prime}$ | Entry <br> Radius <br> $\mathbf{R}$ | Entry <br> Angle <br> $\boldsymbol{?}$ |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 0 | 0 | 24.00 | 2 | 28.00 | 2 | 164.00 | 66.00 | 30.00 |
| 2 | Creek Ln EB | 90 | 0 | 12.00 | 1 | 14.00 | 1 | 164.00 | 66.00 | 30.00 |
| 3 | 2nd St NB | 180 | 0 | 24.00 | 2 | 28.00 | 2 | 164.00 | 66.00 | 30.00 |
| 4 | Creek Ln WB | 270 | 0 | 12.00 | 1 | 14.00 | 1 | 164.00 | 66.00 | 30.00 |

Circulating and Exit Geometry

| Leg | Leg Names | Inscribed <br> Diameter <br> D | Circulating <br> Width <br> C | Circulating <br> Lanes <br> $\mathbf{n c}$ | Exit <br> Width <br> Ex | Exit <br> Lanes <br> nex | Exit <br> Half Width <br> Vx | Exit Half <br> Width Lanes <br> nvx |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 164.00 | 15.00 | 1 | 28.00 | 2 | 24.00 | 2 |
| 2 | Creek Ln EB | 164.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |
| 3 | 2nd St NB | 164.00 | 15.00 | 1 | 14.00 | 1 | 12.00 | 1 |
| 4 | Creek Ln WB | 164.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |

Capacity Modifiers and Capacity Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity |  | Entry Calibration |  | Approach Road |  |  | Exit Road |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Capacity + or - | XWalk Factor | Intercept + or - | Slope Factor | V <br> (ft) | Default Capacity | Calib Capacity | V <br> (ft) | Default Capacity | Calib Capacity |
| 1 | 2nd St SB | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 24.00 | 3584 | 0 |
| 2 | Creek Ln EB | 0 | 1.000 | 0 | 1.000 | 20.00 | 1792 | 0 | 12.00 | 1792 | 0 |
| 3 | 2nd St NB | 0 | 1.000 | 0 | 1.000 | 20.00 | 3584 | 0 | 12.00 | 1792 | 0 |
| 4 | Creek Ln WB | 0 | 1.000 | 0 | 1.000 | 20.00 | 1792 | 0 | 12.00 | 1792 | 0 |

## Bypass Geometry

Bypass Approach Geometry (ft)

| Leg | Leg Names | Bypass <br> Type | Bypass <br> Flows | V | nv | Vb | nvb | Vt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | Yield | 410 | 24 | 2 | 12 | 1 | 24 |

Bypass Entry and Exit Geometry (ft)

| Leg | Leg Names | Eb | neb | Lb | Lt | Rb | Phib | Leg | Leg Names | Exit Lanes <br> nex |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2nd St SB | 12 | 1 | 0 | 130 | 66.00008 <br> 87 | 30 | 2 | Creek Ln EB | 1 |

Bypass Entry Capacity Modifiers and Calibration (veh/hr)

| Leg | Leg Names | Capacity <br> + or - | Entry Capacity <br> Cross Walk <br> Factor | Intercept <br> + or - | Salibration <br> Factor |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 0 | 1.000 | 0 | 1.000 |

## Traffic Flow Data (veh/hr)

2040 PM Peak Peak Hour Flows

| Leg | Leg Names | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks <br> $\%$ | Flow Modifiers <br> Flow <br> Factor | Peak Hour <br> Factor |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 85 | 325 | 980 | 0 | 410 | 5.0 | 1.00 | 0.9 |
| 2 | Creek Ln EB | 0 | 145 | 40 | 90 | 0 | 5.0 | 1.00 | 0.9 |
| 3 | 2nd St NB | 0 | 100 | 840 | 95 | 0 | 5.0 | 1.00 | 0.9 |
| 4 | Creek Ln WB | 0 | 75 | 15 | 30 | 0 | 5.0 | 1.00 | 0.9 |

## Operational Results

## 2040 PM Peak - 60 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit <br> Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | 2nd St SB | Yield | 1390 | 410 | 190 | 190 | 1100 | 2005 | 962 | 0.7075 | 0.4343 |
| 2 | Creek Ln EB | None | 275 |  | 1465 |  | 525 | 578 |  | 0.4946 |  |
| 3 | 2nd St NB | None | 1035 |  | 595 |  | 1145 | 1607 |  | 0.6576 |  |
| 4 | Creek Ln WB | None | 120 |  | 1170 |  | 460 | 683 |  | 0.1800 |  |

Delays, Queues and Level of Service

| Leg | Leg Names |  | Bypass | Average Delay (sec) |  |  | $95 \%$ Queue (veh) |  | Level of Service <br> Type |  |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |  |  |
| 1 | 2nd St SB | Yield | 7.13 | 6.44 | 6.97 | 9.31 | 2.33 | A | A | A |
| 2 | Creek Ln EB | None | 10.90 |  | 10.90 | 3.11 |  | B | B |  |
| 3 | 2nd St NB | None | 6.17 |  | 6.17 | 6.44 |  | A |  |  |
| 4 | Creek Ln WB | None | 5.97 |  | 5.97 | 0.65 | A | A |  |  |

## 2040 PM Peak - 15 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit <br> Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | 2nd St SB | Yield | 1544 | 456 | 211 | 211 | 1217 | 1985 | 952 | 0.7907 | 0.4852 |
| 2 | Creek Ln EB | None | 306 |  | 1622 |  | 582 | 522 |  | 0.5996 |  |
| 3 | 2nd St NB | None | 1150 |  | 658 |  | 1267 | 1545 |  | 0.7548 |  |
| 4 | Creek Ln WB | None | 133 |  | 1295 |  | 509 | 638 |  | 0.2116 |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass Type | Average Delay (sec) |  |  | 95\% Queue (veh) |  | Level of Service |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | 2nd St SB | Yield | 8.10 | 6.69 | 7.78 | 9.31 | 2.33 | A | A | A |
| 2 | Creek Ln EB | None | 12.62 |  | 12.62 | 3.11 |  | B |  | B |
| 3 | 2nd St NB | None | 7.22 |  | 7.22 | 6.44 |  | A |  | A |
| 4 | Creek Ln WB | None | 6.21 |  | 6.21 | 0.65 |  | A |  | A |

2040 PM Peak
50\% Confidence Level
Daylight conditions

Project: TH 169 \& 2nd St Interchange
Scheme: 2nd St/Creek Ln 2040 PM peak hour
Rodel-Win1 - Full Geometry

## Approach Flow Profile

2040 PM Peak - Approach Flows (Veh / Hour)

| Time Slice | 2nd St SB | Creek Ln EB | 2nd St NB | Creek Ln WB |
| :--- | :---: | :---: | :---: | :---: |
| $0.0-7.5$ | 216.67 | 33.10 | 124.58 | 14.44 |
| $7.5-15.0$ | 216.67 | 33.10 | 124.58 | 14.44 |
| $15.0-22.5$ | 216.67 | 33.10 | 124.58 | 14.44 |
| $22.5-30.0$ | 250.00 | 38.19 | 143.75 | 16.67 |
| $30.0-37.5$ | 250.00 | 38.19 | 143.75 | 16.67 |
| $37.5-45.0$ | 216.67 | 33.10 | 124.58 | 14.44 |
| $45.0-52.5$ | 216.67 | 33.10 | 124.58 | 14.44 |
| $52.5-60.0$ | 216.67 | 33.10 | 143.58 | 14.44 |
| Peak 15 min | 250.00 | 38.19 | 129.38 | 16.67 |
| Peak 60 min | 225.00 | 34.38 | 15.00 |  |

## Exit Flow Profile

2040 PM Peak - Exit Flows (Veh / Hour)

| Time Slice | 2nd St SB | Creek Ln EB | 2nd St NB | Creek Ln WB |
| :--- | :---: | :---: | :---: | :---: |
| $0.0-7.5$ | 132.13 | 63.03 | 137.53 | 55.25 |
| $7.5-15.0$ | 132.39 | 63.19 | 137.81 | 55.36 |
| $15.0-22.5$ | 132.40 | 63.19 | 137.82 | 55.37 |
| $22.5-30.0$ | 151.62 | 72.61 | 157.88 | 63.41 |
| $30.0-37.5$ | 152.72 | 72.90 | 158.97 | 63.87 |
| $37.5-45.0$ | 133.58 | 63.50 | 138.97 | 55.85 |
| $45.0-52.5$ | 132.43 | 63.20 | 137.84 | 55.38 |
| $52.5-60.0$ | 132.41 | 63.20 | 137.83 | 55.37 |
| $0-60$ | 1100 | 525 | 1145 | 460 |
| $\%$ Trucks | 5.00 | 5.00 | 5.00 | 5.00 |

## Economics

## Economic Input Data

2040 - Vehicle Delay Parameters

| Peaks | Peak / Day | Days / Year | Delay Cost <br> (\$ / hour) |
| :---: | :---: | :---: | :---: |
| AM Peak | 1 | 325 | 15.00 |
| OFF Peak | 14 | 325 | 15.00 |
| PM Peak | 1 | 325 | 15.00 |

2040 - Accident Severity Proportions and Costs

| Accident Type | Proportion (\%) | Cost (\$) |
| :--- | :---: | :---: |
| Fatal Vehicle Accident | 0.3 | 0 |
| Incapacitating Vehicle Accident | 17.7 | 0 |
| Non-incapacitating Vehicle Accident | 82 | 0 |
| Damage Only Vehicle Accident | 100 | 0 |
| Pedestrian Injury Accident | 100 | 0 |

## Economics - Results Data

2040 Delay and Accident Costs

|  | Delay Costs <br> Delays <br> Veh.hrs | Costs <br> $(\$)$ | Accident <br> Types | Accident Costs <br> Annual <br> Accidents | Accident <br> Costs | Total Costs <br> Cost <br> Type | Costs <br> (\$/year) |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM | 0.00 | 0 | Vehicles Injury | 0.00 | 0 | Vehicle Delay Cost | 30666 |
| OFF | 0.00 | 0 | Vehicles DO | 0.00 | 0 | Vehicle Injury Acc Cost | 0 |
| PM | 2044.40 | 30666 | Pedestrians | 0.00 | 0 | Vehicle DO Acc Cost | 0 |
|  |  |  |  |  |  | Pedestrian Accident Cost | 0 |
|  |  |  |  |  |  | Total Accident Cost | 0 |
| Total | 2044.40 | 30666 | Totals | 0.00 | 0 | TOTAL COST | 30666 |

## Global Results

## Performance and Accidents

2040 PM Peak Global Performance

| Parameter | Units | Entries | Bypasses | Total |
| :--- | :---: | :---: | :---: | :---: |
| Arrive Flows | $\mathrm{veh} / \mathrm{hr}$ | 2820 | 410 | 3230 |
| Capacity | $\mathrm{veh} / \mathrm{hr}$ | 4873 | 962 | 5835 |
| Average Delay | $\mathrm{sec} / \mathrm{veh}$ | 7.09 | 6.44 | 7.01 |
| L.O.S. (Signal) | $\mathrm{A}-\mathrm{F}$ | A | A | A |
| L.O.S. (Unsig) | $\mathrm{A}-\mathrm{F}$ | A | A | A |
| Total Delay | veh.hrs | 5.56 | 0.73 | 6.29 |

## Scheme Summary

## Control Data

## Control Data and Model Parameters

| TH 169 \& 2nd St Interchange | 2040 PHF Flow Profile (veh) |
| :--- | :--- |
| WB ramps/2nd St/Frontage Rd 2040 AM Peak | 7.5 min Time Slice |
| Rodel-Win1 | Queuing Delays (sec) |
| Right Hand Drive | Daylight conditions |
| AM Peak Hour | Peak 60/15 min Results |
| Full Geometry | Output flows: Vehicles |
| English Units (ft) | $50 \%$ Confidence Level |

## Available Data

| Entry Capacity Calibrated | No |
| :--- | :---: |
| Entry Capacity Modified | No |
| Crosswalks | No |
| Flows Factored | No |
| Approach/Exit Road Capacity Calibrated | No |
| Accidents | No |
| Accident Costs | No |
| Bypass Model | No |
| Bypass Calibration | No |
| Global Results | Yes |

## Operational Data

## Main Geometry (ft)

## Approach and Entry Geometry

| Leg | Leg Names | Approach <br> Bearing <br> (deg) | Grade <br> Separation <br> $\mathbf{G}$ | Half Width <br> $\mathbf{V}$ | Approach <br> Lanes <br> $\mathbf{n}$ | Entry <br> Width <br> $\mathbf{E}$ | Entry <br> Lanes <br> $\mathbf{n}$ | Flare <br> Length <br> $\mathbf{L}^{\prime}$ | Entry <br> Radius <br> $\mathbf{R}$ | Entry <br> Angle <br> $?$ |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 0 | 0 | 24.00 | 2 | 28.00 | 2 | 131.00 | 66.00 | 30.00 |
| 2 | WB on ramp | 90 | 0 | 12.00 | 1 | 14.00 | 1 | 131.00 | 66.00 | 30.00 |
| 3 | 2nd St NB | 180 | 0 | 24.00 | 2 | 28.00 | 2 | 131.00 | 66.00 | 30.00 |
| 4 | WB off ramp | 270 | 0 | 24.00 | 2 | 28.00 | 2 | 131.00 | 66.00 | 30.00 |
| 5 | Frontage SWB | 315 | 0 | 12.00 | 1 | 14.00 | 1 | 131.00 | 66.00 | 30.00 |

## Circulating and Exit Geometry

| Leg | Leg Names | Inscribed <br> Diameter <br> D | Circulating <br> Width <br> C | Circulating <br> Lanes <br> nc | Exit <br> Width <br> Ex | Exit <br> Lanes <br> nex | Exit <br> Half Width <br> Vx | Exit Half <br> Width Lanes <br> nvx |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 230.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |
| 2 | WB on ramp | 230.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |
| 3 | 2nd St NB | 230.00 | 15.00 | 1 | 28.00 | 2 | 24.00 | 2 |
| 4 | WB off ramp | 230.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |
| 5 | Frontage SWB | 230.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |

Capacity Modifiers and Capacity Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity |  | Entry Calibration |  | Approach Road |  |  | Exit Road |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Capacity + or - | XWalk <br> Factor | Intercept + or - | Slope Factor | V <br> (ft) | Default Capacity | Calib Capacity | V (ft) | Default Capacity | Calib Capacity |
| 1 | 2nd St SB | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 12.00 | 1792 | 0 |
| 2 | WB on ramp | 0 | 1.000 | 0 | 1.000 | 24.00 | 1792 | 0 | 12.00 | 1792 | 0 |
| 3 | 2nd St NB | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 24.00 | 3584 | 0 |
| 4 | WB off ramp | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 12.00 | 1792 | 0 |
| 5 | Frontage SWB | 0 | 1.000 | 0 | 1.000 | 24.00 | 1792 | 0 | 12.00 | 1792 | 0 |

## Traffic Flow Data (veh/hr)

2040 AM Peak Peak Hour Flows

| Leg | Leg Names | U-Turn | Exit-4 | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks <br> $\%$ | Flow Modifiers <br> Flow <br> Factor | Peak Hour <br> Factor |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 0 | 30 | 0 | 700 | 150 | 0 | 5.0 | 1.00 | 0.9 |
| 2 | WB on ramp | 0 | 0 | 0 | 0 | 1 | 0 | 5.0 | 1.00 | 0.9 |
| 3 | 2nd St NB | 0 | 280 | 770 | 110 | 0 | 0 | 5.0 | 1.00 | 0.9 |
| 4 | WB off ramp | 0 | 110 | 0 | 170 | 5 | 0 | 5.0 | 1.00 | 0.9 |
| 5 | Frontage SWB | 0 | 0 | 130 | 25 | 10 | 0 | 5.0 | 1.00 | 0.9 |

## Operational Results

## 2040 AM Peak - 60 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | 2nd St SB | None | 880 |  | 545 |  | 950 | 1869 |  | 0.4776 |  |
| 2 | WB on ramp | None | 1 |  | 970 |  | 455 | 812 |  | 0.0013 |  |
| 3 | 2nd St NB | None | 1160 |  | 30 |  | 941 | 2165 |  | 0.5430 |  |
| 4 | WB off ramp | None | 285 |  | 1190 |  | 0 | 1490 |  | 0.1950 |  |
| 5 | Frontage SWB | None | 165 |  | 1330 |  | 145 | 759 |  | 0.2222 |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass Type | Average Delay (sec) |  |  | 95\% Queue (veh) |  | Level of Service |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | 2nd St SB | None | 3.98 |  | 3.98 | 3.14 |  | A |  | A |
| 2 | WB on ramp | None | 0.00 |  | 0.00 | 0.00 |  | A |  | A |
| 3 | 2nd St NB | None | 4.22 |  | 4.22 | 4.30 |  | A |  | A |
| 4 | WB off ramp | None | 4.55 |  | 4.55 | 1.15 |  | A |  | A |
| 5 | Frontage SWB | None | 5.64 |  | 5.64 | 0.84 |  | A |  | A |

## 2040 AM Peak - 15 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | 2nd St SB | None | 978 |  | 605 |  | 1055 | 1834 |  | 0.5378 |  |
| 2 | WB on ramp | None | 1 |  | 1077 |  | 505 | 780 |  | 0.0014 |  |
| 3 | 2nd St NB | None | 1289 |  | 33 |  | 1045 | 2162 |  | 0.6015 |  |
| 4 | WB off ramp | None | 317 |  | 1321 |  | 0 | 1413 |  | 0.2264 |  |
| 5 | Frontage SWB | None | 183 |  | 1477 |  | 161 | 715 |  | 0.2597 |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass Type | Average Delay (sec) |  |  | 95\% Queue (veh) |  | Level of Service |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | 2nd St SB | None | 4.21 |  | 4.21 | 3.14 |  | A |  | A |
| 2 | WB on ramp | None | 0.00 |  | 0.00 | 0.00 |  | A |  | A |
| 3 | 2nd St NB | None | 4.44 |  | 4.44 | 4.30 |  | A |  | A |
| 4 | WB off ramp | None | 4.70 |  | 4.70 | 1.15 |  | A |  | A |
| 5 | Frontage SWB | None | 5.88 |  | 5.88 | 0.84 |  | A |  | A |

## Approach Flow Profile

2040 AM Peak - Approach Flows (Veh / Hour)

| Time Slice | 2nd St SB | WB on ramp | 2nd St NB | WB off ramp | Frontage SWB |
| :--- | :---: | :---: | :---: | :---: | :---: |
| $0.0-7.5$ | 105.93 | 0.12 | 139.63 | 34.31 | 19.86 |
| $7.5-15.0$ | 105.93 | 0.12 | 139.63 | 34.31 | 19.86 |
| $15.0-22.5$ | 105.93 | 0.12 | 139.63 | 34.31 | 19.86 |
| $22.5-30.0$ | 122.22 | 0.14 | 161.11 | 39.58 | 22.92 |
| $30.0-37.5$ | 122.22 | 0.14 | 161.11 | 39.58 | 22.92 |
| $37.5-45.0$ | 105.93 | 0.12 | 139.63 | 34.31 | 19.86 |
| $45.0-52.5$ | 105.93 | 0.12 | 139.63 | 34.31 | 19.86 |
| $52.5-60.0$ | 105.93 | 0.12 | 139.63 | 34.31 | 19.86 |
| Peak 15 min | 122.22 | 0.14 | 161.11 | 39.58 | 22.92 |
| Peak 60 min | 110.00 | 0.12 | 145.00 | 35.63 | 20.63 |

## Exit Flow Profile

2040 AM Peak - Exit Flows (Veh / Hour)

| Time Slice | 2nd St SB | WB on ramp | 2nd St NB | WB off ramp | Frontage SWB |
| :--- | :---: | :---: | :---: | :---: | :---: |
| $0.0-7.5$ | 114.24 | 54.71 | 113.15 | 0.00 | 17.44 |
| $7.5-15.0$ | 114.35 | 54.77 | 113.26 | 0.00 | 17.45 |
| $15.0-22.5$ | 114.35 | 113.27 | 0.00 | 17.45 |  |
| $22.5-30.0$ | 131.77 | 63.11 | 130.52 | 0.00 | 20.11 |
| $30.0-37.5$ | 131.94 | 63.19 | 130.69 | 0.00 | 20.14 |
| $37.5-45.0$ | 114.52 | 54.85 | 113.44 | 0.00 | 17.48 |
| $45.0-52.5$ | 114.36 | 54.77 | 113.27 | 0.00 | 17.45 |
| $52.5-60.0$ | 114.35 | 455 | 941 | 0.00 | 17.45 |
| $0-60$ | 950 | 5.00 | 5.00 | 0.00 | 145 |
| $\%$ Trucks |  |  |  | 5.00 |  |

## Economics

## Economic Input Data

2040 - Vehicle Delay Parameters

| Peaks | Peak / Day | Days / Year | Delay Cost <br> $(\$ /$ hour $)$ |
| :---: | :---: | :---: | :---: |
| AM Peak | 1 | 325 | 15.00 |
| OFF Peak | 14 | 325 | 15.00 |
| PM Peak | 1 | 325 | 15.00 |

2040 - Accident Severity Proportions and Costs

| Accident Type | Proportion (\%) | Cost (\$) |
| :--- | :---: | :---: |
| Fatal Vehicle Accident | 0.3 | 0 |
| Incapacitating Vehicle Accident | 17.7 | 0 |
| Non-incapacitating Vehicle Accident | 82 | 0 |
| Damage Only Vehicle Accident | 100 | 0 |
| Pedestrian Injury Accident | 100 | 0 |

## Economics - Results Data

## 2040 Delay and Accident Costs

| Peak | Delay Costs <br> Delays <br> Veh.hrs | Costs <br> (\$) | Accident <br> Types | Accident Costs <br> Annual <br> Accidents | Accident <br> Costs | Total Costs <br> Cost <br> Type | Costs <br> (\$/year) |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM | 958.87 | 14383 | Vehicles Injury | 0.00 | 0 | Vehicle Delay Cost | 14383 |
| OFF | 0.00 | 0 | Vehicles DO | 0.00 | 0 | Vehicle Injury Acc Cost | 0 |
| PM | 0.00 | 0 | Pedestrians | 0.00 | 0 | Vehicle DO Acc Cost | 0 |
|  |  |  |  |  | Pedestrian Accident Cost | 0 |  |
|  |  |  |  |  | Total Accident Cost | 0 |  |
| Total | 958.87 | 14383 | Totals | 0.00 | 0 | TOTAL COST | 14383 |

## Global Results

## Performance and Accidents

2040 AM Peak Global Performance

| Parameter | Units | Entries | Bypasses |
| :--- | :---: | :---: | :---: |
| Arrive Flows | $\mathrm{veh} / \mathrm{hr}$ | 2491 |  |
| Capacity | $\mathrm{veh} / \mathrm{hr}$ | 7095 | 2491 |
| Average Delay | $\mathrm{sec} / \mathrm{veh}$ | 4.26 | 7095 |
| L.O.S. (Signal) | $\mathrm{A}-\mathrm{F}$ | A | 4.26 |
| L.O.S. (Unsig) | $\mathrm{A}-\mathrm{F}$ | A | A |
| Total Delay | veh.hrs | 2.95 | A |

## Scheme Summary

## Control Data

## Control Data and Model Parameters

| TH 169 \& 2nd St Interchange | 2040 PHF Flow Profile (veh) |
| :--- | :--- |
| WB ramps/2nd St/Frontage Rd 2040 PM Peak | 7.5 min Time Slice |
| Rodel-Win1 | Queuing Delays (sec) |
| Right Hand Drive | Daylight conditions |
| PM Peak Hour | Peak 60/15 min Results |
| Full Geometry | Output flows: Vehicles |
| English Units (ft) | $50 \%$ Confidence Level |

## Available Data

| Entry Capacity Calibrated | No |
| :--- | :---: |
| Entry Capacity Modified | No |
| Crosswalks | No |
| Flows Factored | No |
| Approach/Exit Road Capacity Calibrated | No |
| Accidents | No |
| Accident Costs | No |
| Bypass Model | No |
| Bypass Calibration | No |
| Global Results | Yes |

## Operational Data

## Main Geometry (ft)

## Approach and Entry Geometry

| Leg | Leg Names | Approach <br> Bearing <br> (deg) | Grade <br> Separation <br> $\mathbf{G}$ | Half Width <br> $\mathbf{V}$ | Approach <br> Lanes <br> $\mathbf{n}$ | Entry <br> Width <br> $\mathbf{E}$ | Entry <br> Lanes <br> $\mathbf{n}$ | Flare <br> Length <br> $\mathbf{L}^{\prime}$ | Entry <br> Radius <br> $\mathbf{R}$ | Entry <br> Angle <br> $?$ |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 0 | 0 | 24.00 | 2 | 28.00 | 2 | 131.00 | 66.00 | 30.00 |
| 2 | WB on ramp | 90 | 0 | 12.00 | 1 | 14.00 | 1 | 131.00 | 66.00 | 30.00 |
| 3 | 2nd St NB | 180 | 0 | 24.00 | 2 | 28.00 | 2 | 131.00 | 66.00 | 30.00 |
| 4 | WB off ramp | 270 | 0 | 24.00 | 2 | 28.00 | 2 | 131.00 | 66.00 | 30.00 |
| 5 | Frontage SWB | 315 | 0 | 12.00 | 1 | 14.00 | 1 | 131.00 | 66.00 | 30.00 |

## Circulating and Exit Geometry

| Leg | Leg Names | Inscribed <br> Diameter <br> D | Circulating <br> Width <br> C | Circulating <br> Lanes <br> nc | Exit <br> Width <br> Ex | Exit <br> Lanes <br> nex | Exit <br> Half Width <br> Vx | Exit Half <br> Width Lanes <br> nvx |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 230.00 | 30.00 | 2 | 28.00 | 2 | 24.00 | 2 |
| 2 | WB on ramp | 230.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |
| 3 | 2nd St NB | 230.00 | 15.00 | 1 | 28.00 | 2 | 24.00 | 2 |
| 4 | WB off ramp | 230.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |
| 5 | Frontage SWB | 230.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |

Capacity Modifiers and Capacity Calibration (veh/hr)

| Leg | Leg Names |  | Entry Capacity <br> Capacity <br> + or - |  | XWalk <br> Factor | Entry Calibration <br> Intercept <br> + or - |  | Slope <br> Factor | Approach Road <br> (ft)   Default <br> Capacity Calib <br> Capacity V <br> (ft) Exit Road <br> Default <br> Capacity Calib <br> Capacity <br> 1        2nd St SB | 0 | 1.000 |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 1.000 | 24.00 | 3584 | 0 | 24.00 | 3584 | 0 |  |  |  |  |
| 2 | WB on ramp | 0 | 1.000 | 0 | 1.000 | 24.00 | 1792 | 0 | 12.00 | 1792 | 0 |
| 3 | 2nd St NB | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 24.00 | 3584 | 0 |
| 4 | WB off ramp | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 12.00 | 1792 | 0 |
| 5 | Frontage SWB | 0 | 1.000 | 0 | 1.000 | 24.00 | 1792 | 0 | 12.00 | 1792 | 0 |

## Traffic Flow Data (veh/hr)

2040 PM Peak Peak Hour Flows

| Leg | Leg Names | U-Turn | Exit-4 | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks <br> $\%$ | Flow Modifiers <br> Flow <br> Factor | Peak Hour <br> Factor |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 0 | 30 | 0 | 1075 | 350 | 0 | 5.0 | 1.00 | 0.9 |
| 2 | WB on ramp | 0 | 0 | 0 | 0 | 1 | 0 | 5.0 | 1.00 | 0.9 |
| 3 | 2nd St NB | 0 | 370 | 555 | 110 | 0 | 0 | 5.0 | 1.00 | 0.9 |
| 4 | WB off ramp | 0 | 220 | 0 | 160 | 5 | 0 | 5.0 | 1.00 | 0.9 |
| 5 | Frontage SWB | 0 | 0 | 130 | 40 | 20 | 0 | 5.0 | 1.00 | 0.9 |

## Operational Results

## 2040 PM Peak - 60 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | 2nd St SB | None | 1455 |  | 760 |  | 735 | 1743 |  | 0.8649 |  |
| 2 | WB on ramp | None | 1 |  | 1454 |  | 760 | 669 |  | 0.0015 |  |
| 3 | 2nd St NB | None | 1035 |  | 30 |  | 1426 | 2165 |  | 0.4847 |  |
| 4 | WB off ramp | None | 385 |  | 1065 |  | 0 | 1563 |  | 0.2510 |  |
| 5 | Frontage SWB | None | 190 |  | 1305 |  | 145 | 767 |  | 0.2533 |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass Type | Average Delay (sec) |  |  | 95\% Queue (veh) |  | Level of Service |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | 2nd St SB | None | 13.37 |  | 13.37 | 22.16 |  | B |  | B |
| 2 | WB on ramp | None | 0.00 |  | 0.00 | 0.00 |  | A |  | A |
| 3 | 2nd St NB | None | 4.48 |  | 4.48 | 3.99 |  | A |  | A |
| 4 | WB off ramp | None | 4.95 |  | 4.95 | 1.68 |  | A |  | A |
| 5 | Frontage SWB | None | 5.79 |  | 5.79 | 1.00 |  | A |  | A |

## 2040 PM Peak - 15 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | 2nd St SB | None | 1617 |  | 843 |  | 816 | 1694 |  | 0.9852 |  |
| 2 | WB on ramp | None | 1 |  | 1599 |  | 838 | 626 |  | 0.0018 |  |
| 3 | 2nd St NB | None | 1150 |  | 33 |  | 1567 | 2163 |  | 0.5368 |  |
| 4 | WB off ramp | None | 428 |  | 1181 |  | 0 | 1495 |  | 0.2892 |  |
| 5 | Frontage SWB | None | 211 |  | 1448 |  | 160 | 723 |  | 0.2955 |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass Type | Average Delay (sec) |  |  | 95\% Queue (veh) |  | Level of Service |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | 2nd St SB | None | 18.01 |  | 18.01 | 22.16 |  | C |  | C |
| 2 | WB on ramp | None | 0.00 |  | 0.00 | 0.00 |  | A |  | A |
| 3 | 2nd St NB | None | 4.63 |  | 4.63 | 3.99 |  | A |  | A |
| 4 | WB off ramp | None | 5.12 |  | 5.12 | 1.68 |  | A |  | A |
| 5 | Frontage SWB | None | 6.06 |  | 6.06 | 1.00 |  | A |  | A |

## Approach Flow Profile

2040 PM Peak - Approach Flows (Veh / Hour)

| Time Slice | 2nd St SB | WB on ramp | 2nd St NB | WB off ramp | Frontage SWB |
| :--- | :---: | :---: | :---: | :---: | :---: |
| $0.0-7.5$ | 175.14 | 0.12 | 124.58 | 46.34 | 22.87 |
| $7.5-15.0$ | 175.14 | 0.12 | 124.58 | 46.34 | 22.87 |
| $15.0-22.5$ | 175.14 | 0.12 | 124.58 | 46.34 | 22.87 |
| $22.5-30.0$ | 202.08 | 0.14 | 143.75 | 53.47 | 26.39 |
| $30.0-37.5$ | 202.08 | 0.14 | 143.75 | 53.47 | 26.39 |
| $37.5-45.0$ | 175.14 | 0.12 | 124.58 | 46.34 | 22.87 |
| $45.0-52.5$ | 175.14 | 0.12 | 124.58 | 46.34 | 22.87 |
| $52.5-60.0$ | 175.14 | 0.12 | 124.58 | 46.34 | 22.87 |
| Peak 15 min | 202.08 | 0.14 | 143.75 | 53.47 | 26.39 |
| Peak 60 min | 181.88 | 0.12 | 129.38 | 48.13 | 23.75 |

## Exit Flow Profile

2040 PM Peak - Exit Flows (Veh / Hour)

| Time Slice | 2nd St SB | WB on ramp | 2nd St NB | WB off ramp | Frontage SWB |
| :--- | :---: | :---: | :---: | :---: | :---: |
| $0.0-7.5$ | 88.38 | 91.24 | 171.02 | 0.00 | 17.42 |
| $7.5-15.0$ | 88.47 | 91.46 | 171.59 | 0.00 | 17.45 |
| $15.0-22.5$ | 88.47 | 91.47 | 171.63 | 0.00 | 17.45 |
| $22.5-30.0$ | 101.82 | 104.21 | 194.21 | 0.00 | 20.00 |
| $30.0-37.5$ | 102.08 | 105.39 | 197.55 | 0.00 | 20.12 |
| $37.5-45.0$ | 88.73 | 93.03 | 176.10 | 0.00 | 17.61 |
| $45.0-52.5$ | 88.48 | 91.51 | 171.72 | 0.00 | 17.46 |
| $52.5-60.0$ | 88.47 | 760 | 171.67 | 0.00 | 17.45 |
| $0-60$ | 735 | 5.00 | 5.00 | 0 | 145 |
| $\%$ Trucks | 5.00 |  | 0.00 | 5.00 |  |

## Economics

## Economic Input Data

2040 - Vehicle Delay Parameters

| Peaks | Peak / Day | Days / Year | Delay Cost <br> (\$ /hour) |
| :---: | :---: | :---: | :---: |
| AM Peak | 1 | 325 | 15.00 |
| OFF Peak | 14 | 325 | 15.00 |
| PM Peak | 1 | 325 | 15.00 |

2040 - Accident Severity Proportions and Costs

| Accident Type | Proportion (\%) | Cost (\$) |
| :--- | :---: | :---: |
| Fatal Vehicle Accident | 0.3 | 0 |
| Incapacitating Vehicle Accident | 17.7 | 0 |
| Non-incapacitating Vehicle Accident | 82 | 0 |
| Damage Only Vehicle Accident | 100 | 0 |
| Pedestrian Injury Accident | 100 | 0 |

## Economics - Results Data

## 2040 Delay and Accident Costs

| Peak | Delay Costs <br> Delays <br> Veh.hrs | Costs <br> (\$) | Accident <br> Types | Accident Costs <br> Annual <br> Accidents | Accident <br> Costs | Total Costs <br> Cost <br> Type | Costs <br> (\$/year) |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM | 0.00 | 0 | Vehicles Injury | 0.00 | 0 | Vehicle Delay Cost | 36683 |
| OFF | 0.00 | 0 | Vehicles DO | 0.00 | 0 | Vehicle Injury Acc Cost | 0 |
| PM | 2445.53 | 36683 | Pedestrians | 0.00 | 0 | Vehicle DO Acc Cost | 0 |
|  |  |  |  |  |  | Pedestrian Accident Cost | 0 |
|  |  |  |  |  |  | Total Accident Cost | 0 |
| Total | 2445.53 | 36683 | Totals | 0.00 | 0 | TOTAL COST | 36683 |

## Global Results

## Performance and Accidents

2040 PM Peak Global Performance

| Parameter | Units | Entries | Bypasses |
| :--- | :---: | :---: | :---: |
| Arrive Flows | $\mathrm{veh} / \mathrm{hr}$ | 3066 |  |
| Capacity | $\mathrm{veh} / \mathrm{hr}$ | 6908 | 3066 |
| Average Delay | $\mathrm{sec} / \mathrm{veh}$ | 8.84 | 6908 |
| L.O.S. (Signal) | $\mathrm{A}-\mathrm{F}$ | A | 8.84 |
| L.O.S. (Unsig) | $\mathrm{A}-\mathrm{F}$ | A | A |
| Total Delay | veh.hrs | 7.52 | A |

## Kimley»"Horn

5. DESIGN YEAR (2040) CONCEPT 2 SIMTRAFFIC REPORTS

## 1: Site Access \& TH 282 Performance by movement

| Movement | EBT | EBR | WBL | WBT | NBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.0 |
| Total Del/Veh (s) | 0.5 | 0.4 | 18.4 | 2.9 | 10.2 | 2.1 |

5: Creek Ln N \& Triangle Ln N Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.1 | 0.1 | 0.0 | 0.1 | 0.1 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 9.7 | 8.8 | 3.0 | 8.7 | 10.6 | 5.0 | 2.2 | 1.0 | 0.2 | 3.0 |

8: CR 9 \& CR 57/Valley View Drive Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 3.5 | 1.0 | 3.5 | 3.8 | 0.5 | 3.7 | 0.0 | 0.0 | 0.0 | 3.1 | 0.2 |
| Total Del/Veh (s) | 21.2 | 29.0 | 7.5 | 21.6 | 29.9 | 9.8 | 13.8 | 12.4 | 3.7 | 13.7 | 15.9 |

## 8: CR 9 \& CR 57/Valley View Drive Performance by movement

| Movement | All |
| :--- | ---: |
| Denied Del/Veh (s) | 1.2 |
| Total Del/Veh (s) | 13.2 |

9: TH 282 \& Triangle Ln N Performance by movement

| Movement | EBT | WBT | WBR | SBT | SBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 1.0 | 0.9 | 0.8 | 0.4 | 10.1 | 1.4 |

17: CR 9 \& TH 169 WB On/Off Ramp/Frontage Rd Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 3.3 | 0.5 | 3.4 | 3.5 | 0.4 | 3.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 21.9 | 22.3 | 8.6 | 22.1 | 30.0 | 8.0 | 24.4 | 12.6 | 2.3 | 18.0 | 19.2 |

17: CR 9 \& TH 169 WB On/Off Ramp/Frontage Rd Performance by movement

| Movement | All |
| :--- | ---: |
| Denied Del/Veh (s) | 0.6 |
| Total Del/Veh (s) | 16.1 |

## 29: TH 282/CR 9 \& TH 169 EB Off Ramp Performance by movement

| Movement | EBL | EBR | NBT | SBT | All |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 3.3 | 1.0 | 0.0 | 0.0 | 0.5 |
| Total Del/Veh (s) | 44.3 | 15.4 | 3.9 | 9.9 | 12.1 |

# SimTraffic Performance Report 

TH 169/ TH 282/ CR 9 Interchange Jordan MN
Total Zone Performance

|  |  |
| :--- | ---: |
| Denied Del/veh (s) | 2.2 |
| Total Del/Veh $(\mathrm{s})$ | 30.9 |

Intersection: 1: Site Access \& TH 282

| Movement | EB | EB | WB | NB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | T | R | L | R |
| Maximum Queue (ft) | 4 | 18 | 70 | 77 |
| Average Queue (ft) | 0 | 1 | 26 | 35 |
| 95th Queue (ft) | 3 | 11 | 60 | 65 |
| Link Distance (ft) | 239 |  |  | 195 |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  | 135 | 200 |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

Intersection: 5: Creek Ln N \& Triangle Ln N

| Movement | EB | EB | WB | NB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | LTR | L |
| Maximum Queue (ft) | 88 | 65 | 40 | 5 |
| Average Queue (ft) | 37 | 33 | 15 | 0 |
| 95th Queue (ft) | 67 | 51 | 41 | 4 |
| Link Distance (ft) | 808 | 808 | 263 |  |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  | 100 |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

## Intersection: 8: CR 9 \& CR 57/Valley View Drive

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | R | L | T | R | L | T | R | L | T | T |
| Maximum Queue (ft) | 127 | 79 | 166 | 121 | 66 | 58 | 153 | 367 | 78 | 58 | 141 | 133 |
| Average Queue (ft) | 59 | 26 | 66 | 60 | 21 | 18 | 71 | 126 | 27 | 25 | 73 | 62 |
| 95th Queue (ft) | 101 | 62 | 123 | 108 | 54 | 44 | 129 | 268 | 58 | 51 | 126 | 113 |
| Link Distance (ft) |  | 784 |  |  | 908 |  |  | 652 | 652 |  | 1263 | 1263 |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (ft) | 250 |  | 250 | 300 |  | 300 | 300 |  |  | 275 |  |  |
| Storage Blk Time (\%) |  |  | 0 |  |  |  |  | 0 |  |  |  |  |
| Queuing Penalty (veh) |  |  | 0 |  |  |  |  | 0 |  |  |  |  |

Intersection: 8: CR 9 \& CR 57/Valley View Drive

| Movement | SB |
| :--- | ---: |
| Directions Served | R |
| Maximum Queue (ft) | 44 |
| Average Queue (ft) | 15 |
| 95th Queue (ft) | 34 |
| Link Distance (ft) |  |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) | 275 |
| Storage Blk Time (\%) |  |
| Queuing Penalty (veh) |  |

## Intersection: 9: TH 282 \& Triangle Ln N

| Movement | WB | SB |
| :--- | ---: | ---: |
| Directions Served | T | R |
| Maximum Queue (ft) | 5 | 101 |
| Average Queue (ft) | 0 | 46 |
| 95th Queue (ft) | 4 | 85 |
| Link Distance (ft) | 239 | 808 |
| Upstream Blk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |
| Storage Bay Dist (ft) |  |  |
| Storage Blk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |

## Intersection: 17: CR 9 \& TH 169 WB On/Off Ramp/Frontage Rd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB | NB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | R | L | T | R | L | T | T | R | L | T |
| Maximum Queue (t) | 190 | 29 | 80 | 146 | 51 | 33 | 246 | 322 | 210 | 40 | 55 | 192 |
| Average Queue (t) | 80 | 3 | 41 | 64 | 22 | 9 | 102 | 133 | 50 | 8 | 20 | 102 |
| 95th Queue (t) | 147 | 17 | 70 | 114 | 49 | 30 | 199 | 264 | 144 | 27 | 46 | 167 |
| Link Distance (tt) |  | 1068 |  |  | 1045 |  |  | 745 | 745 |  |  | 652 |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (tt) | 275 |  | 275 | 250 |  | 250 | 300 |  |  | 300 | 275 |  |
| Storage Blk Time (\%) | 0 |  |  |  |  |  |  | 1 | 0 |  |  |  |
| Queuing Penalty (veh) | 0 |  |  |  |  |  |  | 3 | 0 |  |  |  |

## Intersection: 17: CR 9 \& TH 169 WB On/Off Ramp/Frontage Rd

| Movement | SB | SB |
| :--- | ---: | ---: |
| Directions Served | T | R |
| Maximum Queue (ft) | 192 | 76 |
| Average Queue (ft) | 111 | 29 |
| 95th Queue (ft) | 169 | 61 |
| Link Distance (ft) | 652 |  |
| Upstream Blk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |
| Storage Bay Dist (ft) | 275 |  |
| Storage Blk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |

## Intersection: 29: TH 282/CR 9 \& TH 169 EB Off Ramp

| Movement | EB | EB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | R | T | T | T | T |
| Maximum Queue (ft) | 298 | 218 | 177 | 146 | 212 | 226 |
| Average Queue (ft) | 173 | 105 | 64 | 40 | 96 | 108 |
| 95th Queue (ft) | 270 | 181 | 133 | 98 | 177 | 192 |
| Link Distance (ft) |  | 839 | 210 | 210 | 745 | 745 |
| Upstream Blk Time (\%) |  |  |  | 0 |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |
| Storage Bay Dist (ft) | 300 |  |  |  |  |  |
| Storage Blk Time (\%) | 0 |  |  |  |  |  |
| Queuing Penalty (veh) | 1 |  |  |  |  |  |
|  |  |  |  |  |  |  |

## 1: Site Access \& TH 282 Performance by movement

| Movement | EBT | EBR | WBL | WBT | NBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.3 | 0.1 | 0.2 | 0.1 |
| Total Del/Veh (s) | 1.3 | 1.0 | 40.3 | 3.4 | 22.8 | 4.1 |

5: Creek Ln N \& Triangle Ln N Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 8.9 | 7.4 | 3.6 | 7.6 | 8.7 | 3.7 | 2.6 | 1.3 | 0.6 | 2.8 |

8: CR 9 \& CR 57/Valley View Drive Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 3.5 | 1.0 | 3.6 | 3.9 | 0.4 | 3.9 | 0.0 | 0.0 | 0.0 | 2.3 | 0.4 |
| Total Del/Veh (s) | 46.3 | 40.6 | 23.0 | 43.2 | 41.7 | 7.1 | 26.0 | 9.9 | 1.8 | 12.9 | 22.0 |

## 8: CR 9 \& CR 57/Valley View Drive Performance by movement

| Movement | All |
| :--- | ---: |
| Denied Del/Veh (s) | 1.1 |
| Total Del/Veh (s) | 21.0 |

9: TH 282 \& Triangle Ln N Performance by movement

| Movement | EBT | WBT | WBR | SBT | SBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 1.8 | 2.4 | 1.1 | 0.3 | 22.3 | 2.7 |

17: CR 9 \& TH 169 WB On/Off Ramp/Frontage Rd Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 3.3 | 0.9 | 3.2 | 3.5 | 0.5 | 3.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 33.7 | 32.5 | 18.5 | 37.6 | 45.2 | 7.4 | 83.9 | 23.2 | 4.8 | 33.4 | 58.4 |

17: CR 9 \& TH 169 WB On/Off Ramp/Frontage Rd Performance by movement

| Movement | All |
| :--- | ---: |
| Denied Del/Veh (s) | 0.6 |
| Total Del/Veh (s) | 43.8 |

## 29: TH 282/CR 9 \& TH 169 EB Off Ramp Performance by movement

| Movement | EBL | EBR | NBT | SBT | All |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 3.5 | 0.5 | 0.0 | 0.0 | 0.1 |
| Total Del/Veh (s) | 49.7 | 28.6 | 6.5 | 12.4 | 13.3 |

Total Zone Performance

|  |  |
| :--- | ---: |
| Denied Del/Veh (s) | 1.6 |
| Total Del/Veh (s) | 58.2 |

Intersection: 1: Site Access \& TH 282

| Movement | EB | EB | EB | WB | WB | WB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | R | L | T | T | R |
| Maximum Queue (ft) | 32 | 75 | 59 | 141 | 44 | 54 | 158 |
| Average Queue (ft) | 2 | 5 | 4 | 62 | 2 | 2 | 72 |
| 95th Queue (ft) | 14 | 38 | 29 | 118 | 35 | 34 | 135 |
| Link Distance (ft) | 239 | 239 |  |  | 452 | 452 | 195 |
| Upstream Blk Time (\%) |  |  |  |  |  |  | 0 |
| Queuing Penalty (veh) |  |  |  |  |  |  | 0 |
| Storage Bay Dist (ft) |  |  | 135 | 200 |  |  |  |
| Storage Blk Time (\%) |  | 0 | 0 | 0 | 0 |  |  |
| Queuing Penalty (veh) |  | 0 | 0 | 0 | 0 |  |  |

Intersection: 5: Creek Ln N \& Triangle Ln N

| Movement | EB | EB | WB | NB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | LTR | L |
| Maximum Queue (tt) | 64 | 64 | 44 | 10 |
| Average Queue (tt) | 24 | 35 | 13 | 1 |
| 95th Queue (ft) | 48 | 56 | 40 | 7 |
| Link Distance (ft) | 808 | 808 | 161 |  |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

## Intersection: 8: CR 9 \& CR 57/Valley View Drive

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | R | L | T | R | L | T | R | L | T | T |
| Maximum Queue (ft) | 163 | 244 | 278 | 83 | 83 | 57 | 233 | 256 | 27 | 142 | 364 | 394 |
| Average Queue (ft) | 63 | 39 | 121 | 33 | 36 | 19 | 114 | 94 | 3 | 38 | 178 | 192 |
| 95th Queue (ft) | 125 | 138 | 229 | 66 | 73 | 41 | 199 | 211 | 14 | 103 | 315 | 347 |
| Link Distance (ft) |  | 784 |  |  | 908 |  |  | 652 | 652 |  | 1263 | 1263 |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (ft) | 250 |  | 250 | 300 |  | 300 | 300 |  |  | 275 |  |  |
| Storage Blk Time (\%) |  | 0 | 2 |  |  |  |  |  |  |  | 2 | 2 |
| Queuing Penalty (veh) |  | 0 | 2 |  |  |  |  |  |  |  | 2 | 3 |

Intersection: 8: CR 9 \& CR 57/Valley View Drive

| Movement | SB |
| :--- | ---: |
| Directions Served | R |
| Maximum Queue (ft) | 203 |
| Average Queue (ft) | 25 |
| 95th Queue (ft) | 96 |
| Link Distance ( ft ) |  |
| Upstream BIk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) | 275 |
| Storage Blk Time (\%) | 0 |
| Queuing Penalty (veh) | 0 |

Intersection: 9: TH 282 \& Triangle Ln N

| Movement | EB | WB | WB | WB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | T | R | R |
| Maximum Queue (ft) | 6 | 140 | 121 | 25 | 144 |
| Average Queue (ft) | 0 | 20 | 10 | 2 | 55 |
| 95th Queue (ft) | 5 | 107 | 80 | 26 | 126 |
| Link Distance (ft) | 210 | 239 | 239 |  | 808 |
| Upstream Blk Time (\%) |  | 0 | 0 |  |  |
| Queuing Penalty (veh) |  | 2 | 0 |  |  |
| Storage Bay Dist (ft) |  |  |  | 100 |  |
| Storage Blk Time (\%) |  |  | 0 |  |  |
| Queuing Penalty (veh) |  |  | 0 |  |  |

## Intersection: 17: CR 9 \& TH 169 WB On/Off Ramp/Frontage Rd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB | NB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | R | L | T | R | L | T | T | R | L | T |
| Maximum Queue (ft) | 199 | 37 | 186 | 175 | 84 | 42 | 325 | 660 | 573 | 51 | 222 | 631 |
| Average Queue (ft) | 90 | 3 | 92 | 86 | 33 | 14 | 248 | 345 | 194 | 10 | 33 | 379 |
| 95th Queue (ft) | 164 | 19 | 152 | 154 | 70 | 38 | 385 | 803 | 645 | 32 | 154 | 630 |
| Link Distance (ft) |  | 1068 |  |  | 1045 |  |  | 745 | 745 |  |  | 652 |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  | 4 | 1 |  |  | 2 |
| Queuing Penalty (veh) |  |  |  |  |  |  |  | 23 | 3 |  |  | 12 |
| Storage Bay Dist (ft) | 300 |  | 300 | 260 |  | 260 | 300 |  |  | 300 | 300 |  |
| Storage Blk Time (\%) |  |  |  | 0 |  |  | 23 | 0 |  |  |  | 20 |
| Queuing Penalty (veh) |  |  |  | 0 |  |  | 65 | 0 |  |  |  | 6 |

## Intersection: 17: CR 9 \& TH 169 WB On/Off Ramp/Frontage Rd

| Movement | SB | SB |
| :--- | ---: | ---: |
| Directions Served | T | R |
| Maximum Queue (ft) | 641 | 325 |
| Average Queue (ft) | 392 | 221 |
| 95th Queue (ft) | 645 | 417 |
| Link Distance (ft) | 652 |  |
| Upstream Blk Time (\%) | 2 |  |
| Queuing Penalty (veh) | 17 |  |
| Storage Bay Dist (ft) |  | 300 |
| Storage Blk Time (\%) | 20 | 0 |
| Queuing Penalty (veh) | 70 | 1 |

## Intersection: 29: TH 282/CR 9 \& TH 169 EB Off Ramp

| Movement | EB | EB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | R | T | T | T | T |
| Maximum Queue (ft) | 208 | 282 | 200 | 194 | 427 | 438 |
| Average Queue (ft) | 61 | 148 | 98 | 52 | 145 | 157 |
| 95th Queue (ft) | 145 | 246 | 223 | 169 | 343 | 360 |
| Link Distance (ft) |  | 839 | 210 | 210 | 745 | 745 |
| Upstream Blk Time (\%) |  |  | 4 | 1 |  |  |
| Queuing Penalty (veh) |  |  | 20 | 5 |  |  |
| Storage Bay Dist (ft) | 300 |  |  |  |  |  |
| Storage Blk Time (\%) |  | 1 |  |  |  |  |
| Queuing Penalty (veh) | 0 |  |  |  |  |  |

## Kimley»Horn

6. DESIGN YEAR (2040) CONCEPT 2 RODEL REPORTS

## Scheme Summary

## Control Data

Control Data and Model Parameters

| TH 169 \& 2nd St Interchange | 2040 PHF Flow Profile (veh) |
| :--- | :--- |
| 2nd St/Creek Ln 2040 AM peak hour | 7.5 min Time Slice |
| Rodel-Win1 | Queuing Delays (sec) |
| Right Hand Drive | Daylight conditions |
| AM Peak Hour | Peak 60/15 min Results |
| Full Geometry | Output flows: Vehicles |
| English Units (ft) | $50 \%$ Confidence Level |

## Available Data

| Entry Capacity Calibrated | No |
| :--- | :---: |
| Entry Capacity Modified | No |
| Crosswalks | No |
| Flows Factored | No |
| Approach/Exit Road Capacity Calibrated | No |
| Accidents | No |
| Accident Costs | No |
| Bypass Model | Yes |
| Bypass Calibration | No |
| Global Results | Yes |

2040 AM Peak
50\% Confidence Level
Daylight conditions

Project: TH 169 \& 2nd St Interchange Scheme: 2nd St/Creek Ln 2040 AM peak hour Rodel-Win1 - Full Geometry

## Operational Data

## Main Geometry (ft)

Approach and Entry Geometry

| Leg | Leg Names | Approach <br> Bearing <br> (deg) | Grade <br> Separation <br> $\mathbf{G}$ | Half Width <br> $\mathbf{V}$ | Approach <br> Lanes <br> $\mathbf{n}$ | Entry <br> Width <br> $\mathbf{E}$ | Entry <br> Lanes <br> $\mathbf{n}$ | Flare <br> Length <br> $\mathbf{L}^{\prime}$ | Entry <br> Radius <br> $\mathbf{R}$ | Entry <br> Angle <br> $\boldsymbol{?}$ |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 0 | 0 | 24.00 | 2 | 28.00 | 2 | 164.00 | 66.00 | 30.00 |
| 2 | Creek Ln EB | 90 | 0 | 12.00 | 1 | 14.00 | 1 | 164.00 | 66.00 | 30.00 |
| 3 | 2nd St NB | 180 | 0 | 24.00 | 2 | 28.00 | 2 | 164.00 | 66.00 | 30.00 |
| 4 | Creek Ln WB | 270 | 0 | 12.00 | 1 | 14.00 | 1 | 164.00 | 66.00 | 30.00 |

Circulating and Exit Geometry

| Leg | Leg Names | Inscribed <br> Diameter <br> D | Circulating <br> Width <br> C | Circulating <br> Lanes <br> nc | Exit <br> Width <br> Ex | Exit <br> Lanes <br> nex | Exit <br> Half Width <br> Vx | Exit Half <br> Width Lanes <br> nvx |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 164.00 | 15.00 | 1 | 28.00 | 2 | 24.00 | 2 |
| 2 | Creek Ln EB | 164.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |
| 3 | 2nd St NB | 164.00 | 15.00 | 1 | 14.00 | 1 | 12.00 | 1 |
| 4 | Creek Ln WB | 164.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |

Capacity Modifiers and Capacity Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity |  | Entry Calibration |  | Approach Road |  |  | Exit Road |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Capacity + or - | XWalk <br> Factor | Intercept + or - | Slope Factor | V <br> (ft) | Default Capacity | Calib Capacity | $\begin{gathered} \text { V } \\ (\mathrm{ft}) \end{gathered}$ | Default Capacity | Calib Capacity |
|  | 2nd St SB | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 24.00 | 3584 | 0 |
| 2 | Creek Ln EB | 0 | 1.000 | 0 | 1.000 | 20.00 | 1792 | 0 | 12.00 | 1792 | 0 |
| 3 | 2nd St NB | 0 | 1.000 | 0 | 1.000 | 20.00 | 3584 | 0 | 12.00 | 1792 | 0 |
| 4 | Creek Ln WB | 0 | 1.000 | 0 | 1.000 | 20.00 | 1792 | 0 | 12.00 | 1792 | 0 |

## Bypass Geometry

Bypass Approach Geometry (ft)

| Leg | Leg Names | Bypass <br> Type | Bypass <br> Flows | V | nv | Vb | nvb | Vt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | Yield | 240 | 24 | 2 | 12 | 1 | 24 |

Bypass Entry and Exit Geometry (ft)

| Leg | Leg Names | Eb | neb | Lb | Lt | Rb | Phib | Leg | Leg Names |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2nd St SB | 12 | 1 | 0 | 130 | 66.00005 <br> 914 | 30 | 2 | Creek Ln EB |
| nex | 1 | Nmx |  |  |  |  |  |  |  |

Bypass Entry Capacity Modifiers and Calibration (veh/hr)

| Leg | Leg Names | Capacity <br> + or - | Eross Walk <br> Factor | Intercept <br> + or - | Calibration <br> Slope |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2nd St SB | 0 | 1.000 | 0 | 1.000 |

## Traffic Flow Data (veh/hr)

## 2040 AM Peak Peak Hour Flows

| Leg | Leg Names | Turning Flows |  |  |  |  | Flow Modifiers |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks \% | Flow Factor | Peak Hour Factor |
| 1 | 2nd St SB | 45 | 255 | 765 | 0 | 240 | 5.0 | 1.00 | 0.9 |
| 2 | Creek Ln EB | 0 | 170 | 100 | 60 | 0 | 5.0 | 1.00 | 0.9 |
| 3 | 2nd St NB | 0 | 120 | 730 | 85 | 0 | 5.0 | 1.00 | 0.9 |
| 4 | Creek Ln WB | 0 | 75 | 15 | 20 | 0 | 5.0 | 1.00 | 0.9 |

## Operational Results

## 2040 AM Peak - 60 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | 2nd St SB | Yield | 1065 | 240 | 210 | 210 | 964 | 1985 | 952 | 0.5449 | 0.2561 |
| 2 | Creek Ln EB | None | 330 |  | 1140 |  | 375 | 693 |  | 0.4905 |  |
| 3 | 2nd St NB | None | 935 |  | 570 |  | 900 | 1632 |  | 0.5839 |  |
| 4 | Creek Ln WB | None | 110 |  | 1064 |  | 440 | 720 |  | 0.1561 |  |

Delays, Queues and Level of Service

| Leg | Leg Names |  | Bypass | Average Delay (sec) |  | $95 \%$ Queue (veh) |  | Level of Service <br> Type |  | Entry |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |  |  |
| 1 | 2nd St SB | Yield | 4.88 | 5.00 | 4.90 | 4.64 | 1.03 | A | A | A |
| 2 | Creek Ln EB | None | 9.01 |  | 9.01 | 2.91 |  | A | A |  |
| 3 | 2nd St NB | None | 5.31 |  | 5.31 | 4.79 |  | A | A |  |
| 4 | Creek Ln WB | None | 5.51 |  | 5.51 | 0.54 | A |  |  |  |

## 2040 AM Peak - 15 minutes

Flows and Capacity

| Leg | Leg Names | Bypass <br> Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit <br> Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | 2nd St SB | Yield | 1183 | 267 | 233 | 233 | 1069 | 1963 | 941 | 0.6093 | 0.2865 |
| 2 | Creek Ln EB | None | 367 |  | 1265 |  | 416 | 649 |  | 0.5763 |  |
| 3 | 2nd St NB | None | 1039 |  | 631 |  | 998 | 1571 |  | 0.6690 |  |
| 4 | Creek Ln WB | None | 122 |  | 1180 |  | 488 | 679 |  | 0.1821 |  |

Delays, Queues and Level of Service

| Leg | Leg Names |  | Bypass | Average Delay (sec) |  | $95 \%$ Queue (veh) |  | Level of Service <br> Type |  | Entry |
| :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |  |  |
| 1 | 2nd St SB | Yield | 5.20 | 5.03 | 5.17 | 4.64 | 1.03 | A | A | A |
| 2 | Creek Ln EB | None | 10.04 |  | 10.04 | 2.91 |  | B | B |  |
| 3 | 2nd St NB | None | 5.98 |  | 5.98 | 4.79 |  | A |  |  |
| 4 | Creek Ln WB | None | 5.68 |  | 5.68 | 0.54 | A | A |  |  |

2040 AM Peak 50\% Confidence Level Daylight conditions

Project: TH 169 \& 2nd St Interchange Scheme: 2nd St/Creek Ln 2040 AM peak hour Rodel-Win1 - Full Geometry

## Approach Flow Profile

2040 AM Peak - Approach Flows (Veh / Hour)

| Time Slice | 2nd St SB | Creek Ln EB | 2nd St NB | Creek Ln WB |
| :--- | :---: | :---: | :---: | :---: |
| $0.0-7.5$ | 157.08 | 39.72 | 112.55 | 13.24 |
| $7.5-15.0$ | 157.08 | 39.72 | 112.55 | 13.24 |
| $15.0-22.5$ | 157.08 | 39.72 | 112.55 | 13.24 |
| $22.5-30.0$ | 181.25 | 45.83 | 129.86 | 15.28 |
| $30.0-37.5$ | 181.25 | 45.83 | 129.86 | 15.28 |
| $37.5-45.0$ | 157.08 | 39.72 | 112.55 | 13.24 |
| $45.0-52.5$ | 157.08 | 39.72 | 112.55 | 13.24 |
| $52.5-60.0$ | 157.08 | 39.72 | 112.55 | 13.24 |
| Peak 15 min | 181.25 | 45.83 | 129.86 | 15.28 |
| Peak 60 min | 163.12 | 41.25 | 116.88 | 13.75 |

## Exit Flow Profile

2040 AM Peak - Exit Flows (Veh / Hour)

| Time Slice | 2nd St SB | Creek Ln EB | 2nd St NB | Creek Ln WB |
| :--- | :---: | :---: | :---: | :---: |
| $0.0-7.5$ | 115.96 | 45.06 | 108.19 | 52.88 |
| $7.5-15.0$ | 116.15 | 45.14 | 108.33 | 52.96 |
| $15.0-22.5$ | 116.16 | 45.14 | 108.33 | 52.96 |
| $22.5-30.0$ | 133.30 | 51.92 | 124.55 | 60.82 |
| $30.0-37.5$ | 134.00 | 52.08 | 124.99 | 61.10 |
| $37.5-45.0$ | 116.52 | 45.25 | 108.56 | 53.11 |
| $45.0-52.5$ | 116.17 | 45.14 | 108.34 | 52.97 |
| $52.5-60.0$ | 116.16 | 45.14 | 108.33 | 52.96 |
| $0-60$ | 964 | 375 | 900 | 440 |
| $\%$ Trucks | 5.00 | 5.00 | 5.00 | 5.00 |

2040 AM Peak
50\% Confidence Level
Daylight conditions

Project: TH 169 \& 2nd St Interchange Scheme: 2nd St/Creek Ln 2040 AM peak hour

Rodel-Win1 - Full Geometry

## Economics

## Economic Input Data

## 2040 - Vehicle Delay Parameters

| Peaks | Peak / Day | Days / Year | Delay Cost <br> (\$ / hour) |
| :---: | :---: | :---: | :---: |
| AM Peak | 1 | 325 | 15.00 |
| OFF Peak | 14 | 325 | 15.00 |
| PM Peak | 1 | 325 | 15.00 |

2040 - Accident Severity Proportions and Costs

| Accident Type | Proportion (\%) | Cost (\$) |
| :--- | :---: | :---: |
| Fatal Vehicle Accident | 0.3 | 0 |
| Incapacitating Vehicle Accident | 17.7 | 0 |
| Non-incapacitating Vehicle Accident | 82 | 0 |
| Damage Only Vehicle Accident | 100 | 0 |
| Pedestrian Injury Accident | 100 | 0 |

## Economics - Results Data

2040 Delay and Accident Costs

|  | Delay Costs <br> Delays <br> Veh.hrs | Costs <br> (\$) | Accident <br> Types | Accident Costs <br> Annual <br> Accidents | Accident <br> Costs | Total Costs <br> Cost <br> Type | Costs <br> (\$/year) |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM | 1348.31 | 20225 | Vehicles Injury | 0.00 | 0 | Vehicle Delay Cost | 20225 |
| OFF | 0.00 | 0 | Vehicles DO | 0.00 | 0 | Vehicle Injury Acc Cost | 0 |
| PM | 0.00 | 0 | Pedestrians | 0.00 | 0 | Vehicle DO Acc Cost | 0 |
|  |  |  |  |  |  | Pedestrian Accident Cost | 0 |
|  |  |  |  |  |  | Total Accident Cost | 0 |
| Total | 1348.31 | 20225 | Totals | 0.00 | 0 | TOTAL COST | 20225 |

## Global Results

## Performance and Accidents

2040 AM Peak Global Performance

| Parameter | Units | Entries | Bypasses | Total |
| :--- | :---: | :---: | :---: | :---: |
| Arrive Flows | $\mathrm{veh} / \mathrm{hr}$ | 2440 | 240 | 2680 |
| Capacity | $\mathrm{veh} / \mathrm{hr}$ | 5031 | 952 | 5983 |
| Average Delay | $\mathrm{sec} / \mathrm{veh}$ | 5.63 | 5.00 | 5.57 |
| L.O.S. (Signal) | $\mathrm{A}-\mathrm{F}$ | A | A | A |
| L.O.S. (Unsig) | $\mathrm{A}-\mathrm{F}$ | A | A | A |
| Total Delay | veh.hrs | 3.82 | 0.33 | 4.15 |

## Scheme Summary

## Control Data

## Control Data and Model Parameters

| TH 169 \& 2nd St Interchange | 2040 PHF Flow Profile (veh) |
| :--- | :--- |
| 2nd St/Creek Ln 2040 PM peak hour | 7.5 min Time Slice |
| Rodel-Win1 | Queuing Delays (sec) |
| Right Hand Drive | Daylight conditions |
| PM Peak Hour | Peak 60/15 min Results |
| Full Geometry | Output flows: Vehicles |
| English Units (ft) | $50 \%$ Confidence Level |

## Available Data

| Entry Capacity Calibrated | No |
| :--- | :---: |
| Entry Capacity Modified | No |
| Crosswalks | No |
| Flows Factored | No |
| Approach/Exit Road Capacity Calibrated | No |
| Accidents | No |
| Accident Costs | No |
| Bypass Model | Yes |
| Bypass Calibration | No |
| Global Results | Yes |

## Operational Data

Main Geometry (ft)

## Approach and Entry Geometry

| Leg | Leg Names | Approach <br> Bearing <br> (deg) | Grade <br> Separation <br> $\mathbf{G}$ | Half Width <br> $\mathbf{V}$ | Approach <br> Lanes <br> $\mathbf{n}$ | Entry <br> Width <br> $\mathbf{E}$ | Entry <br> Lanes <br> $\mathbf{n}$ | Flare <br> Length <br> $\mathbf{L}^{\prime}$ | Entry <br> Radius <br> $\mathbf{R}$ | Entry <br> Angle <br> $\boldsymbol{?}$ |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 0 | 0 | 24.00 | 2 | 28.00 | 2 | 164.00 | 66.00 | 30.00 |
| 2 | Creek Ln EB | 90 | 0 | 12.00 | 1 | 14.00 | 1 | 164.00 | 66.00 | 30.00 |
| 3 | 2nd St NB | 180 | 0 | 24.00 | 2 | 28.00 | 2 | 164.00 | 66.00 | 30.00 |
| 4 | Creek Ln WB | 270 | 0 | 12.00 | 1 | 14.00 | 1 | 164.00 | 66.00 | 30.00 |

Circulating and Exit Geometry

| Leg | Leg Names | Inscribed <br> Diameter <br> D | Circulating <br> Width <br> C | Circulating <br> Lanes <br> $\mathbf{n c}$ | Exit <br> Width <br> Ex | Exit <br> Lanes <br> nex | Exit <br> Half Width <br> Vx | Exit Half <br> Width Lanes <br> nvx |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 164.00 | 15.00 | 1 | 28.00 | 2 | 24.00 | 2 |
| 2 | Creek Ln EB | 164.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |
| 3 | 2nd St NB | 164.00 | 15.00 | 1 | 14.00 | 1 | 12.00 | 1 |
| 4 | Creek Ln WB | 164.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |

Capacity Modifiers and Capacity Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity |  | Entry Calibration |  | Approach Road |  |  | Exit Road |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Capacity + or - | XWalk Factor | Intercept + or - | Slope Factor | V <br> (ft) | Default Capacity | Calib Capacity | V <br> (ft) | Default Capacity | Calib Capacity |
| 1 | 2nd St SB | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 24.00 | 3584 | 0 |
| 2 | Creek Ln EB | 0 | 1.000 | 0 | 1.000 | 20.00 | 1792 | 0 | 12.00 | 1792 | 0 |
| 3 | 2nd St NB | 0 | 1.000 | 0 | 1.000 | 20.00 | 3584 | 0 | 12.00 | 1792 | 0 |
| 4 | Creek Ln WB | 0 | 1.000 | 0 | 1.000 | 20.00 | 1792 | 0 | 12.00 | 1792 | 0 |

## Bypass Geometry

Bypass Approach Geometry (ft)

| Leg | Leg Names | Bypass <br> Type | Bypass <br> Flows | V | nv | Vb | nvb | Vt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | Yield | 410 | 24 | 2 | 12 | 1 | 24 |

Bypass Entry and Exit Geometry (ft)

| Leg | Leg Names | Eb | neb | Lb | Lt | Rb | Phib | Leg | Leg Names | Exit Lanes <br> nex |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2nd St SB | 12 | 1 | 0 | 130 | 66.00008 <br> 87 | 30 | 2 | Creek Ln EB | 1 |

Bypass Entry Capacity Modifiers and Calibration (veh/hr)

| Leg | Leg Names | Capacity <br> + or - | Entry Capacity <br> Cross Walk <br> Factor | Intercept <br> + or - | Salibration <br> Factor |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 0 | 1.000 | 0 | 1.000 |

## Traffic Flow Data (veh/hr)

2040 PM Peak Peak Hour Flows

| Leg | Leg Names | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks <br> $\%$ | Flow Modifiers <br> Flow <br> Factor | Peak Hour <br> Factor |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 85 | 325 | 980 | 0 | 410 | 5.0 | 1.00 | 0.9 |
| 2 | Creek Ln EB | 0 | 145 | 40 | 90 | 0 | 5.0 | 1.00 | 0.9 |
| 3 | 2nd St NB | 0 | 100 | 840 | 95 | 0 | 5.0 | 1.00 | 0.9 |
| 4 | Creek Ln WB | 0 | 75 | 15 | 30 | 0 | 5.0 | 1.00 | 0.9 |

## Operational Results

## 2040 PM Peak - 60 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit <br> Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | 2nd St SB | Yield | 1390 | 410 | 190 | 190 | 1100 | 2005 | 962 | 0.7075 | 0.4343 |
| 2 | Creek Ln EB | None | 275 |  | 1465 |  | 525 | 578 |  | 0.4946 |  |
| 3 | 2nd St NB | None | 1035 |  | 595 |  | 1145 | 1607 |  | 0.6576 |  |
| 4 | Creek Ln WB | None | 120 |  | 1170 |  | 460 | 683 |  | 0.1800 |  |

Delays, Queues and Level of Service

| Leg | Leg Names |  | Bypass | Average Delay (sec) |  |  | $95 \%$ Queue (veh) |  | Level of Service <br> Type |  |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |  |  |
| 1 | 2nd St SB | Yield | 7.13 | 6.44 | 6.97 | 9.31 | 2.33 | A | A | A |
| 2 | Creek Ln EB | None | 10.90 |  | 10.90 | 3.11 |  | B | B |  |
| 3 | 2nd St NB | None | 6.17 |  | 6.17 | 6.44 |  | A |  |  |
| 4 | Creek Ln WB | None | 5.97 |  | 5.97 | 0.65 | A | A |  |  |

## 2040 PM Peak - 15 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit <br> Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | 2nd St SB | Yield | 1544 | 456 | 211 | 211 | 1217 | 1985 | 952 | 0.7907 | 0.4852 |
| 2 | Creek Ln EB | None | 306 |  | 1622 |  | 582 | 522 |  | 0.5996 |  |
| 3 | 2nd St NB | None | 1150 |  | 658 |  | 1267 | 1545 |  | 0.7548 |  |
| 4 | Creek Ln WB | None | 133 |  | 1295 |  | 509 | 638 |  | 0.2116 |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass Type | Average Delay (sec) |  |  | 95\% Queue (veh) |  | Level of Service |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | 2nd St SB | Yield | 8.10 | 6.69 | 7.78 | 9.31 | 2.33 | A | A | A |
| 2 | Creek Ln EB | None | 12.62 |  | 12.62 | 3.11 |  | B |  | B |
| 3 | 2nd St NB | None | 7.22 |  | 7.22 | 6.44 |  | A |  | A |
| 4 | Creek Ln WB | None | 6.21 |  | 6.21 | 0.65 |  | A |  | A |

2040 PM Peak
50\% Confidence Level
Daylight conditions

Project: TH 169 \& 2nd St Interchange
Scheme: 2nd St/Creek Ln 2040 PM peak hour
Rodel-Win1 - Full Geometry

## Approach Flow Profile

2040 PM Peak - Approach Flows (Veh / Hour)

| Time Slice | 2nd St SB | Creek Ln EB | 2nd St NB | Creek Ln WB |
| :--- | :---: | :---: | :---: | :---: |
| $0.0-7.5$ | 216.67 | 33.10 | 124.58 | 14.44 |
| $7.5-15.0$ | 216.67 | 33.10 | 124.58 | 14.44 |
| $15.0-22.5$ | 216.67 | 33.10 | 124.58 | 14.44 |
| $22.5-30.0$ | 250.00 | 38.19 | 143.75 | 16.67 |
| $30.0-37.5$ | 250.00 | 38.19 | 143.75 | 16.67 |
| $37.5-45.0$ | 216.67 | 33.10 | 124.58 | 14.44 |
| $45.0-52.5$ | 216.67 | 33.10 | 124.58 | 14.44 |
| $52.5-60.0$ | 216.67 | 33.10 | 143.58 | 14.44 |
| Peak 15 min | 250.00 | 38.19 | 129.38 | 16.67 |
| Peak 60 min | 225.00 | 34.38 | 15.00 |  |

## Exit Flow Profile

2040 PM Peak - Exit Flows (Veh / Hour)

| Time Slice | 2nd St SB | Creek Ln EB | 2nd St NB | Creek Ln WB |
| :--- | :---: | :---: | :---: | :---: |
| $0.0-7.5$ | 132.13 | 63.03 | 137.53 | 55.25 |
| $7.5-15.0$ | 132.39 | 63.19 | 137.81 | 55.36 |
| $15.0-22.5$ | 132.40 | 63.19 | 137.82 | 55.37 |
| $22.5-30.0$ | 151.62 | 72.61 | 157.88 | 63.41 |
| $30.0-37.5$ | 152.72 | 72.90 | 158.97 | 63.87 |
| $37.5-45.0$ | 133.58 | 63.50 | 138.97 | 55.85 |
| $45.0-52.5$ | 132.43 | 63.20 | 137.84 | 55.38 |
| $52.5-60.0$ | 132.41 | 63.20 | 137.83 | 55.37 |
| $0-60$ | 1100 | 525 | 1145 | 460 |
| $\%$ Trucks | 5.00 | 5.00 | 5.00 | 5.00 |

## Economics

## Economic Input Data

2040 - Vehicle Delay Parameters

| Peaks | Peak / Day | Days / Year | Delay Cost <br> (\$ / hour) |
| :---: | :---: | :---: | :---: |
| AM Peak | 1 | 325 | 15.00 |
| OFF Peak | 14 | 325 | 15.00 |
| PM Peak | 1 | 325 | 15.00 |

2040 - Accident Severity Proportions and Costs

| Accident Type | Proportion (\%) | Cost (\$) |
| :--- | :---: | :---: |
| Fatal Vehicle Accident | 0.3 | 0 |
| Incapacitating Vehicle Accident | 17.7 | 0 |
| Non-incapacitating Vehicle Accident | 82 | 0 |
| Damage Only Vehicle Accident | 100 | 0 |
| Pedestrian Injury Accident | 100 | 0 |

## Economics - Results Data

2040 Delay and Accident Costs

|  | Delay Costs <br> Delays <br> Veh.hrs | Costs <br> $(\$)$ | Accident <br> Types | Accident Costs <br> Annual <br> Accidents | Accident <br> Costs | Total Costs <br> Cost <br> Type | Costs <br> (\$/year) |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM | 0.00 | 0 | Vehicles Injury | 0.00 | 0 | Vehicle Delay Cost | 30666 |
| OFF | 0.00 | 0 | Vehicles DO | 0.00 | 0 | Vehicle Injury Acc Cost | 0 |
| PM | 2044.40 | 30666 | Pedestrians | 0.00 | 0 | Vehicle DO Acc Cost | 0 |
|  |  |  |  |  |  | Pedestrian Accident Cost | 0 |
|  |  |  |  |  |  | Total Accident Cost | 0 |
| Total | 2044.40 | 30666 | Totals | 0.00 | 0 | TOTAL COST | 30666 |

## Global Results

## Performance and Accidents

2040 PM Peak Global Performance

| Parameter | Units | Entries | Bypasses | Total |
| :--- | :---: | :---: | :---: | :---: |
| Arrive Flows | $\mathrm{veh} / \mathrm{hr}$ | 2820 | 410 | 3230 |
| Capacity | $\mathrm{veh} / \mathrm{hr}$ | 4873 | 962 | 5835 |
| Average Delay | $\mathrm{sec} / \mathrm{veh}$ | 7.09 | 6.44 | 7.01 |
| L.O.S. (Signal) | $\mathrm{A}-\mathrm{F}$ | A | A | A |
| L.O.S. (Unsig) | $\mathrm{A}-\mathrm{F}$ | A | A | A |
| Total Delay | veh.hrs | 5.56 | 0.73 | 6.29 |

## Kimley»Horn

7. DESIGN YEAR (2040) CONCEPT 3 SIMTRAFFIC REPORTS

## 1: Site Access \& TH 282 Performance by movement

| Movement | EBT | EBR | WBL | WBT | NBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 | 0.0 |
| Total Del/Veh (s) | 0.5 | 0.4 | 11.0 | 2.5 | 7.9 | 1.8 |

5: Creek Ln N \& Triangle Ln N Performance by movement

| Movement | EBT | EBR | WBL | WBT | NBL | NBT | NBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.1 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 1.1 | 3.4 | 4.7 | 6.2 | 0.2 | 0.0 | 0.1 | 1.8 |

8: CR 9 \& CR 57/Valley View Drive Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 3.5 | 1.1 | 3.5 | 3.7 | 0.7 | 3.8 | 0.0 | 0.0 | 0.0 | 3.1 | 0.2 |
| Total Del/Veh (s) | 22.4 | 29.3 | 8.0 | 22.0 | 30.5 | 8.8 | 15.7 | 12.9 | 3.7 | 15.3 | 16.0 |

8: CR 9 \& CR 57/Valley View Drive Performance by movement

| Movement | All |
| :--- | ---: |
| Denied Del/Veh (s) | 1.3 |
| Total Del/Veh (s) | 14.0 |

9: TH 282 \& Triangle Ln N Performance by movement

| Movement | EBT | WBT | WBR | SBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 |
| Total Del/Veh (s) | 1.0 | 3.8 | 1.3 | 14.3 | 3.3 |

29: TH 282/CR 9 \& TH 169 EB Off Ramp/TH 169 EB On Ramp Performance by movement

| Movement | EBL | EBR | NBT | NBR | SBL | SBT | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.3 | 0.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 |
| Total Del/Veh (s) | 48.8 | 15.5 | 16.6 | 4.7 | 28.9 | 10.1 | 17.9 |

Total Zone Performance

|  |  |
| :--- | ---: |
| Denied Del/Veh (s) | 1.5 |
| Total Del/Veh (s) | 27.4 |

Intersection: 1: Site Access \& TH 282

| Movement | EB | WB | WB | WB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | R | L | T | T | R |
| Maximum Queue (ft) | 17 | 73 | 6 | 6 | 75 |
| Average Queue (ft) | 0 | 20 | 0 | 0 | 33 |
| 95th Queue (ft) | 4 | 54 | 5 | 4 | 59 |
| Link Distance (ft) |  |  | 452 | 452 | 195 |
| Upstream Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |
| Storage Bay Dist (ft) | 135 | 200 |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |

Intersection: 5: Creek Ln N \& Triangle Ln N

| Movement | EB | EB | WB | WB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | T | R | L | T |
| Maximum Queue (ft) | 31 | 55 | 39 | 30 |
| Average Queue (ft) | 5 | 33 | 8 | 4 |
| 95th Queue (ft) | 24 | 50 | 31 | 21 |
| Link Distance (ft) | 807 |  | 147 | 147 |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  | 150 |  |  |
| Storage Blk Time (\%) |  |  |  |  |

## Intersection: 8: CR 9 \& CR 57/Valley View Drive

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | T | R | L | T | R | L | T | R | L | T | T |
| Maximum Queue (tt) | 122 | 50 | 146 | 177 | 63 | 57 | 207 | 282 | 94 | 63 | 134 | 126 |
| Average Queue (tt) | 58 | 19 | 63 | 86 | 18 | 15 | 76 | 129 | 33 | 22 | 75 | 59 |
| 95th Queue (tt) | 104 | 45 | 114 | 151 | 46 | 40 | 147 | 245 | 68 | 51 | 124 | 110 |
| Link Distance (tt) |  | 783 |  |  | 905 |  |  | 1153 | 1153 |  | 1263 | 1263 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  | 275 |  |  |
| Storage Bay Dist (ft) | 250 |  | 250 | 200 |  | 200 | 300 |  |  | 25 |  |  |
| Storage Blk Time (\%) |  |  |  | 0 |  |  |  | 0 |  |  |  |  |
| Queuing Penalty (veh) |  |  |  | 0 |  |  |  | 0 |  |  |  |  |

Intersection: 8: CR 9 \& CR 57/Valley View Drive

| Movement | SB |
| :--- | ---: |
| Directions Served | R |
| Maximum Queue (ft) | 43 |
| Average Queue (ft) | 13 |
| 95th Queue (ft) | 32 |
| Link Distance (ft) |  |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) | 275 |
| Storage Blk Time (\%) |  |
| Queuing Penalty (veh) |  |

## Intersection: 9: TH 282 \& Triangle Ln N

| Movement | EB | WB | WB | WB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | T | R | R |
| Maximum Queue (ft) | 10 | 202 | 199 | 50 | 143 |
| Average Queue (ft) | 0 | 56 | 29 | 4 | 66 |
| 95th Queue (ft) | 7 | 160 | 121 | 38 | 120 |
| Link Distance (ft) | 186 | 251 | 251 |  | 807 |
| Upstream Blk Time (\%) |  | 0 | 0 |  |  |
| Queuing Penalty (veh) |  | 1 | 0 |  |  |
| Storage Bay Dist (ft) |  |  |  | 100 |  |
| Storage Blk Time (\%) |  |  | 1 | 0 |  |
| Queuing Penalty (veh) |  |  | 1 | 0 |  |

Intersection: 29: TH 282/CR 9 \& TH 169 EB Off Ramp/TH 169 EB On Ramp

| Movement | EB | EB | NB | NB | NB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LT | R | T | T | R | L | T | T |
| Maximum Queue (ft) | 382 | 244 | 220 | 230 | 186 | 215 | 276 | 265 |
| Average Queue (ft) | 185 | 101 | 166 | 138 | 71 | 110 | 94 | 108 |
| 95th Queue (ft) | 313 | 195 | 258 | 251 | 177 | 186 | 209 | 222 |
| Link Distance (ft) | 840 | 840 | 186 | 186 |  |  | 304 | 304 |
| Upstream Blk Time (\%) |  |  | 13 | 5 | 0 |  | 0 | 0 |
| Queuing Penalty (veh) |  |  | 71 | 26 | 0 |  | 0 | 0 |
| Storage Bay Dist (ft) |  |  |  |  | 150 | 180 |  |  |
| Storage Blk Time (\%) |  |  |  | 7 | 0 | 1 | 1 |  |
| Queuing Penalty (veh) |  |  |  | 15 | 1 | 5 | 3 |  |

## Zone Summary

```
Zone wide Queuing Penalty: 124
```


## 1: Site Access \& TH 282 Performance by movement

| Movement | EBT | EBR | WBL | WBT | NBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.3 | 0.1 | 0.2 | 0.1 |
| Total Del/Veh (s) | 1.2 | 0.9 | 22.4 | 3.4 | 18.6 | 3.4 |

5: Creek Ln N \& Triangle Ln N Performance by movement

| Movement | EBT | EBR | WBL | WBT | NBL | NBT | NBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.1 | 0.1 | 0.0 | 0.0 | 0.0 |  |
| Total Del/Veh (s) | 0.7 | 3.4 | 3.9 | 5.1 | 4.8 | 2.5 | 3.6 |  |

8: CR 9 \& CR 57/Valley View Drive Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBR |  |  |  |  |  |  |  |  |  |  |  |
| Denied Del/Veh (s) | 3.5 | 0.9 | 3.6 | 3.8 | 0.5 | 3.8 | 0.0 | 0.0 | 0.0 | 2.4 | 0.4 |
| Total Del/Veh (s) | 42.7 | 43.0 | 17.6 | 36.5 | 39.5 | 6.7 | 25.5 | 8.5 | 3.0 | 14.0 | 21.0 |

## 8: CR 9 \& CR 57/Valley View Drive Performance by movement

| Movement | All |
| :--- | ---: |
| Denied Del/Veh (s) | 1.1 |
| Total Del/Veh (s) | 19.5 |

9: TH 282 \& Triangle Ln N Performance by movement

| Movement | EBT | WBT | WBR | SBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 1.1 | 3.4 | 2.3 | 25.7 | 3.2 |

29: TH 282/CR 9 \& TH 169 EB Off Ramp/TH 169 EB On Ramp Performance by movement

| Movement | EBL | EBR | NBT | NBR | SBL | SBT | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.2 | 0.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Del/Veh (s) | 50.4 | 25.9 | 10.6 | 2.7 | 25.6 | 6.9 | 12.3 |

Total Zone Performance

|  |  |
| :--- | ---: |
| Denied Del/Veh (s) | 1.2 |
| Total Del/Veh (s) | 27.8 |

Intersection: 1: Site Access \& TH 282

| Movement | EB | EB | EB | WB | WB | WB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | R | L | T | T | R |
| Maximum Queue (ft) | 67 | 80 | 32 | 136 | 34 | 117 | 146 |
| Average Queue (ft) | 6 | 8 | 3 | 45 | 1 | 6 | 62 |
| 95th Queue (ft) | 44 | 53 | 18 | 92 | 25 | 51 | 123 |
| Link Distance (ft) | 251 | 251 |  |  | 452 | 452 | 195 |
| Upstream Blk Time (\%) |  |  |  |  |  |  | 0 |
| Queuing Penalty (veh) |  |  |  |  |  |  | 0 |
| Storage Bay Dist (ft) |  |  | 135 | 200 |  |  |  |
| Storage Blk Time (\%) |  | 0 |  |  |  |  |  |

Intersection: 5: Creek Ln N \& Triangle Ln N

| Movement | EB | EB | WB | WB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | R | L | T | L | R |
| Maximum Queue (ft) | 31 | 67 | 30 | 30 | 70 | 21 |
| Average Queue (ft) | 4 | 36 | 9 | 5 | 34 | 3 |
| 95th Queue ( ft ) | 20 | 55 | 31 | 23 | 60 | 15 |
| Link Distance (ft) | 807 |  | 147 | 147 | 413 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  | 150 |
| Storage Bay Dist ( ft$)$ |  |  |  |  |  |  |

## Intersection: 8: CR 9 \& CR 57/Valley View Drive

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | R | L | T | R | L | T | R | L | T | T |
| Maximum Queue (ft) | 170 | 91 | 218 | 160 | 89 | 50 | 264 | 216 | 74 | 66 | 300 | 333 |
| Average Queue (ft) | 63 | 28 | 96 | 72 | 31 | 18 | 118 | 91 | 23 | 24 | 177 | 184 |
| 95th Queue (ft) | 129 | 70 | 177 | 131 | 70 | 40 | 205 | 187 | 57 | 55 | 274 | 286 |
| Link Distance (ft) |  | 783 |  |  | 902 |  |  | 1152 | 1152 |  | 1263 | 1263 |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (ft) | 250 |  | 250 | 300 |  | 300 | 300 |  |  | 275 |  |  |
| Storage Blk Time (\%) | 0 |  | 0 |  |  |  | 0 |  |  |  | 1 | 1 |
| Queuing Penalty (veh) | 0 |  | 0 |  |  |  | 0 |  |  |  | 0 | 1 |

Intersection: 8: CR 9 \& CR 57/Valley View Drive

| Movement | SB |
| :--- | ---: |
| Directions Served | R |
| Maximum Queue (ft) | 153 |
| Average Queue (ft) | 27 |
| 95th Queue (ft) | 98 |
| Link Distance (ft) |  |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) | 275 |
| Storage Blk Time (\%) | 0 |
| Queuing Penalty (veh) | 0 |

Intersection: 9: TH 282 \& Triangle Ln N

| Movement | WB | WB | WB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | T | T | R | R |
| Maximum Queue (ft) | 192 | 259 | 124 | 170 |
| Average Queue (ft) | 23 | 48 | 11 | 69 |
| 95th Queue (ft) | 117 | 173 | 68 | 135 |
| Link Distance (ft) | 251 | 251 |  | 807 |
| Upstream Blk Time (\%) | 0 | 1 |  |  |
| Queuing Penalty (veh) | 0 | 3 |  |  |
| Storage Bay Dist (ft) |  |  | 100 |  |
| Storage Blk Time (\%) |  | 3 | 0 |  |
| Queuing Penalty (veh) |  | 5 | 0 |  |

Intersection: 29: TH 282/CR 9 \& TH 169 EB Off Ramp/TH 169 EB On Ramp

| Movement | EB | EB | NB | NB | NB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LT | R | T | T | R | L | T | T |
| Maximum Queue (ft) | 126 | 264 | 210 | 227 | 186 | 229 | 309 | 313 |
| Average Queue (ft) | 54 | 133 | 101 | 141 | 33 | 99 | 94 | 105 |
| 95th Queue (ft) | 107 | 227 | 216 | 249 | 118 | 198 | 255 | 276 |
| Link Distance (ft) | 840 | 840 | 186 | 186 |  |  | 304 | 304 |
| Upstream Blk Time (\%) |  |  | 4 | 7 | 0 |  | 0 | 1 |
| Queuing Penalty (veh) |  |  | 21 | 36 | 0 |  | 3 | 4 |
| Storage Bay Dist (ft) |  |  |  |  | 150 | 180 |  |  |
| Storage Blk Time (\%) |  |  |  | 10 |  | 2 | 3 |  |
| Queuing Penalty (veh) |  |  |  | 11 |  | 10 | 5 |  |

## Zone Summary

```
Zone wide Queuing Penalty: }10
```


## Kimley»Horn

8. DESIGN YEAR (2040) CONCEPT 3 RODEL REPORTS

## Scheme Summary

## Control Data

Control Data and Model Parameters

| TH 169 \& 2nd St Interchange | 2040 PHF Flow Profile (veh) |
| :--- | :--- |
| 2nd St/Creek Ln 2040 AM peak hour | 7.5 min Time Slice |
| Rodel-Win1 | Queuing Delays (sec) |
| Right Hand Drive | Daylight conditions |
| AM Peak Hour | Peak 60/15 min Results |
| Full Geometry | Output flows: Vehicles |
| English Units (ft) | $50 \%$ Confidence Level |

## Available Data

| Entry Capacity Calibrated | No |
| :--- | :---: |
| Entry Capacity Modified | No |
| Crosswalks | No |
| Flows Factored | No |
| Approach/Exit Road Capacity Calibrated | No |
| Accidents | No |
| Accident Costs | No |
| Bypass Model | Yes |
| Bypass Calibration | No |
| Global Results | Yes |

2040 AM Peak
50\% Confidence Level
Daylight conditions

Project: TH 169 \& 2nd St Interchange Scheme: 2nd St/Creek Ln 2040 AM peak hour Rodel-Win1 - Full Geometry

## Operational Data

## Main Geometry (ft)

Approach and Entry Geometry

| Leg | Leg Names | Approach <br> Bearing <br> (deg) | Grade <br> Separation <br> $\mathbf{G}$ | Half Width <br> $\mathbf{V}$ | Approach <br> Lanes <br> $\mathbf{n}$ | Entry <br> Width <br> $\mathbf{E}$ | Entry <br> Lanes <br> $\mathbf{n}$ | Flare <br> Length <br> $\mathbf{L}^{\prime}$ | Entry <br> Radius <br> $\mathbf{R}$ | Entry <br> Angle <br> $\boldsymbol{?}$ |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 0 | 0 | 24.00 | 2 | 28.00 | 2 | 164.00 | 66.00 | 30.00 |
| 2 | Creek Ln EB | 90 | 0 | 12.00 | 1 | 14.00 | 1 | 164.00 | 66.00 | 30.00 |
| 3 | 2nd St NB | 180 | 0 | 24.00 | 2 | 28.00 | 2 | 164.00 | 66.00 | 30.00 |
| 4 | Creek Ln WB | 270 | 0 | 12.00 | 1 | 14.00 | 1 | 164.00 | 66.00 | 30.00 |

Circulating and Exit Geometry

| Leg | Leg Names | Inscribed <br> Diameter <br> D | Circulating <br> Width <br> C | Circulating <br> Lanes <br> nc | Exit <br> Width <br> Ex | Exit <br> Lanes <br> nex | Exit <br> Half Width <br> Vx | Exit Half <br> Width Lanes <br> nvx |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 164.00 | 15.00 | 1 | 28.00 | 2 | 24.00 | 2 |
| 2 | Creek Ln EB | 164.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |
| 3 | 2nd St NB | 164.00 | 15.00 | 1 | 14.00 | 1 | 12.00 | 1 |
| 4 | Creek Ln WB | 164.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |

Capacity Modifiers and Capacity Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity |  | Entry Calibration |  | Approach Road |  |  | Exit Road |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Capacity + or - | XWalk <br> Factor | Intercept + or - | Slope Factor | V <br> (ft) | Default Capacity | Calib Capacity | $\begin{gathered} \text { V } \\ (\mathrm{ft}) \end{gathered}$ | Default Capacity | Calib Capacity |
|  | 2nd St SB | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 24.00 | 3584 | 0 |
| 2 | Creek Ln EB | 0 | 1.000 | 0 | 1.000 | 20.00 | 1792 | 0 | 12.00 | 1792 | 0 |
| 3 | 2nd St NB | 0 | 1.000 | 0 | 1.000 | 20.00 | 3584 | 0 | 12.00 | 1792 | 0 |
| 4 | Creek Ln WB | 0 | 1.000 | 0 | 1.000 | 20.00 | 1792 | 0 | 12.00 | 1792 | 0 |

## Bypass Geometry

Bypass Approach Geometry (ft)

| Leg | Leg Names | Bypass <br> Type | Bypass <br> Flows | V | nv | Vb | nvb | Vt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | Yield | 240 | 24 | 2 | 12 | 1 | 24 |

Bypass Entry and Exit Geometry (ft)

| Leg | Leg Names | Eb | neb | Lb | Lt | Rb | Phib | Leg | Leg Names |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2nd St SB | 12 | 1 | 0 | 130 | 66.00005 <br> 914 | 30 | 2 | Creek Ln EB |
| nex | 1 | Nmx |  |  |  |  |  |  |  |

Bypass Entry Capacity Modifiers and Calibration (veh/hr)

| Leg | Leg Names | Capacity <br> + or - | Eross Walk <br> Factor | Intercept <br> + or - | Calibration <br> Slope |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2nd St SB | 0 | 1.000 | 0 | 1.000 |

## Traffic Flow Data (veh/hr)

## 2040 AM Peak Peak Hour Flows

| Leg | Leg Names | Turning Flows |  |  |  |  | Flow Modifiers |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks \% | Flow Factor | Peak Hour Factor |
| 1 | 2nd St SB | 45 | 50 | 765 | 0 | 240 | 5.0 | 1.00 | 0.9 |
| 2 | Creek Ln EB | 0 | 230 | 40 | 60 | 0 | 5.0 | 1.00 | 0.9 |
| 3 | 2nd St NB | 0 | 120 | 780 | 30 | 0 | 5.0 | 1.00 | 0.9 |
| 4 | Creek Ln WB | 0 | 75 | 15 | 25 | 0 | 5.0 | 1.00 | 0.9 |

## Operational Results

## 2040 AM Peak - 60 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit <br> Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | 2nd St SB | Yield | 860 | 240 | 210 | 210 | 1080 | 1985 | 952 | 0.4385 | 0.2561 |
| 2 | Creek Ln EB | None | 330 |  | 935 |  | 375 | 766 |  | 0.4417 |  |
| 3 | 2nd St NB | None | 930 |  | 365 |  | 900 | 1833 |  | 0.5150 |  |
| 4 | Creek Ln WB | None | 115 |  | 1175 |  | 120 | 681 |  | 0.1730 |  |

Delays, Queues and Level of Service

| Leg | Leg Names |  | Bypass | Average Delay (sec) |  | $95 \%$ Queue (veh) |  | Level of Service <br> Type |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |  |
| 1 | 2nd St SB | Yield | 3.27 | 5.00 | 3.65 | 2.48 | 1.03 | A | A |
| 2 | Creek Ln EB | None | 7.53 |  | 7.53 | 2.32 |  | A |  |
| 3 | 2nd St NB | None | 4.13 |  | 4.13 | 3.50 |  | A | A |
| 4 | Creek Ln WB | None | 5.94 |  | 5.94 | 0.62 | A | A |  |

## 2040 AM Peak - 15 minutes

Flows and Capacity

| Leg | Leg Names | Bypass <br> Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit <br> Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | 2nd St SB | Yield | 956 | 267 | 233 | 233 | 1199 | 1963 | 941 | 0.4903 | 0.2865 |
| 2 | Creek Ln EB | None | 367 |  | 1038 |  | 416 | 729 |  | 0.5111 |  |
| 3 | 2nd St NB | None | 1033 |  | 405 |  | 999 | 1794 |  | 0.5813 |  |
| 4 | Creek Ln WB | None | 128 |  | 1304 |  | 133 | 635 |  | 0.2038 |  |

Delays, Queues and Level of Service

| Leg | Leg Names |  | Bypass | Average Delay (sec) |  | $95 \%$ Queue (veh) |  | Level of Service <br> Type |  | Entry |
| :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |  |  |
| 1 | 2nd St SB | Yield | 3.40 | 5.03 | 3.76 | 2.48 | 1.03 | A | A | A |
| 2 | Creek Ln EB | None | 8.12 |  | 8.12 | 2.32 |  | A | A |  |
| 3 | 2nd St NB | None | 4.43 |  | 4.43 | 3.50 |  | A | A |  |
| 4 | Creek Ln WB | None | 6.19 |  | 6.19 | 0.62 | A | A |  |  |

2040 AM Peak 50\% Confidence Level Daylight conditions

Project: TH 169 \& 2nd St Interchange Scheme: 2nd St/Creek Ln 2040 AM peak hour Rodel-Win1 - Full Geometry

## Approach Flow Profile

2040 AM Peak - Approach Flows (Veh / Hour)

| Time Slice | 2nd St SB | Creek Ln EB | 2nd St NB | Creek Ln WB |
| :--- | :---: | :---: | :---: | :---: |
| $0.0-7.5$ | 132.41 | 39.72 | 111.94 | 13.84 |
| $7.5-15.0$ | 132.41 | 39.72 | 111.94 | 13.84 |
| $15.0-22.5$ | 132.41 | 39.72 | 111.94 | 13.84 |
| $22.5-30.0$ | 152.78 | 45.83 | 129.17 | 15.97 |
| $30.0-37.5$ | 152.78 | 45.83 | 129.17 | 15.97 |
| $37.5-45.0$ | 132.41 | 39.72 | 111.94 | 13.84 |
| $45.0-52.5$ | 132.41 | 39.72 | 111.94 | 13.84 |
| $52.5-60.0$ | 132.41 | 39.72 | 129.17 | 13.84 |
| Peak 15 min | 152.78 | 45.83 | 116.25 | 15.97 |
| Peak 60 min | 137.50 | 41.25 |  | 14.38 |

## Exit Flow Profile

2040 AM Peak - Exit Flows (Veh / Hour)

| Time Slice | 2nd St SB | Creek Ln EB | 2nd St NB | Creek Ln WB |
| :--- | :---: | :---: | :---: | :---: |
| $0.0-7.5$ | 129.84 | 45.07 | 108.24 | 14.43 |
| $7.5-15.0$ | 129.99 | 45.14 | 108.33 | 14.44 |
| $15.0-22.5$ | 130.00 | 45.14 | 108.33 | 14.44 |
| $22.5-30.0$ | 149.74 | 51.98 | 124.86 | 16.64 |
| $30.0-37.5$ | 149.99 | 52.08 | 124.99 | 16.67 |
| $37.5-45.0$ | 130.26 | 45.24 | 108.47 | 14.47 |
| $45.0-52.5$ | 130.01 | 45.14 | 108.34 | 14.45 |
| $52.5-60.0$ | 130.00 | 45.14 | 108.33 | 14.44 |
| $0-60$ | 1080 | 375 | 900 | 120 |
| $\%$ Trucks | 5.00 | 5.00 | 5.00 | 5.00 |

2040 AM Peak
50\% Confidence Level
Daylight conditions

Project: TH 169 \& 2nd St Interchange Scheme: 2nd St/Creek Ln 2040 AM peak hour

Rodel-Win1 - Full Geometry

## Economics

## Economic Input Data

## 2040 - Vehicle Delay Parameters

| Peaks | Peak / Day | Days / Year | Delay Cost <br> (\$ / hour) |
| :---: | :---: | :---: | :---: |
| AM Peak | 1 | 325 | 15.00 |
| OFF Peak | 14 | 325 | 15.00 |
| PM Peak | 1 | 325 | 15.00 |

2040 - Accident Severity Proportions and Costs

| Accident Type | Proportion (\%) | Cost (\$) |
| :--- | :---: | :---: |
| Fatal Vehicle Accident | 0.3 | 0 |
| Incapacitating Vehicle Accident | 17.7 | 0 |
| Non-incapacitating Vehicle Accident | 82 | 0 |
| Damage Only Vehicle Accident | 100 | 0 |
| Pedestrian Injury Accident | 100 | 0 |

## Economics - Results Data

2040 Delay and Accident Costs

|  | Delay Costs <br> Delays <br> Veh.hrs | Costs <br> (\$) | Accident <br> Types | Accident Costs <br> Annual <br> Accidents | Accident <br> Costs | Total Costs <br> Cost <br> Type | Costs <br> (\$/year) |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM | 994.94 | 14924 | Vehicles Injury | 0.00 | 0 | Vehicle Delay Cost | 14924 |
| OFF | 0.00 | 0 | Vehicles DO | 0.00 | 0 | Vehicle Injury Acc Cost | 0 |
| PM | 0.00 | 0 | Pedestrians | 0.00 | 0 | Vehicle DO Acc Cost | 0 |
|  |  |  |  |  |  | Pedestrian Accident Cost | 0 |
|  |  |  |  |  |  | Total Accident Cost | 0 |
| Total | 994.94 | 14924 | Totals | 0.00 | 0 | TOTAL COST | 14924 |

## Global Results

## Performance and Accidents

2040 AM Peak Global Performance

| Parameter | Units | Entries | Bypasses | Total |
| :--- | :---: | :---: | :---: | :---: |
| Arrive Flows | $\mathrm{veh} / \mathrm{hr}$ | 2235 | 240 | 2475 |
| Capacity | $\mathrm{veh} / \mathrm{hr}$ | 5265 | 952 | 6217 |
| Average Delay | $\mathrm{sec} / \mathrm{veh}$ | 4.39 | 5.00 | 4.45 |
| L.O.S. (Signal) | $\mathrm{A}-\mathrm{F}$ | A | A | A |
| L.O.S. (Unsig) | $\mathrm{A}-\mathrm{F}$ | A | A | A |
| Total Delay | veh.hrs | 2.73 | 0.33 | 3.06 |

## Scheme Summary

## Control Data

Control Data and Model Parameters

| TH 169 \& 2nd St Interchange | 2040 PHF Flow Profile (veh) |
| :--- | :--- |
| 2nd St/Creek Ln 2040 PM peak hour | 7.5 min Time Slice |
| Rodel-Win1 | Queuing Delays (sec) |
| Right Hand Drive | Daylight conditions |
| PM Peak Hour | Peak 60/15 min Results |
| Full Geometry | Output flows: Vehicles |
| English Units (ft) | $50 \%$ Confidence Level |

## Available Data

| Entry Capacity Calibrated | No |
| :--- | :---: |
| Entry Capacity Modified | No |
| Crosswalks | No |
| Flows Factored | No |
| Approach/Exit Road Capacity Calibrated | No |
| Accidents | No |
| Accident Costs | No |
| Bypass Model | Yes |
| Bypass Calibration | No |
| Global Results | Yes |

## Operational Data

## Main Geometry (ft)

Approach and Entry Geometry

| Leg | Leg Names | Approach <br> Bearing <br> (deg) | Grade <br> Separation <br> $\mathbf{G}$ | Half Width <br> $\mathbf{V}$ | Approach <br> Lanes <br> $\mathbf{n}$ | Entry <br> Width <br> $\mathbf{E}$ | Entry <br> Lanes <br> $\mathbf{n}$ | Flare <br> Length <br> $\mathbf{L}^{\prime}$ | Entry <br> Radius <br> $\mathbf{R}$ | Entry <br> Angle <br> $\boldsymbol{?}$ |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 0 | 0 | 24.00 | 2 | 28.00 | 2 | 164.00 | 66.00 | 30.00 |
| 2 | Creek Ln EB | 90 | 0 | 12.00 | 1 | 14.00 | 1 | 164.00 | 66.00 | 30.00 |
| 3 | 2nd St NB | 180 | 0 | 24.00 | 2 | 28.00 | 2 | 164.00 | 66.00 | 30.00 |
| 4 | Creek Ln WB | 270 | 0 | 12.00 | 1 | 14.00 | 1 | 164.00 | 66.00 | 30.00 |

Circulating and Exit Geometry

| Leg | Leg Names | Inscribed <br> Diameter <br> D | Circulating <br> Width <br> C | Circulating <br> Lanes <br> nc | Exit <br> Width <br> Ex | Exit <br> Lanes <br> nex | Exit <br> Half Width <br> Vx | Exit Half <br> Width Lanes <br> nvx |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 164.00 | 15.00 | 1 | 28.00 | 2 | 24.00 | 2 |
| 2 | Creek Ln EB | 164.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |
| 3 | 2nd St NB | 164.00 | 15.00 | 1 | 14.00 | 1 | 12.00 | 1 |
| 4 | Creek Ln WB | 164.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |

Capacity Modifiers and Capacity Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity |  | Entry Calibration |  | Approach Road |  |  | Exit Road |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Capacity + or - | XWalk <br> Factor | Intercept + or - | Slope <br> Factor | $\begin{gathered} \mathrm{V} \\ (\mathrm{ft}) \end{gathered}$ | Default Capacity | Calib Capacity | $\begin{gathered} \mathrm{V} \\ (\mathrm{ft}) \end{gathered}$ | Default Capacity | Calib Capacity |
| 1 | 2nd St SB | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 24.00 | 3584 | 0 |
| 2 | Creek Ln EB | 0 | 1.000 | 0 | 1.000 | 20.00 | 1792 | 0 | 12.00 | 1792 | 0 |
| 3 | 2nd St NB | 0 | 1.000 | 0 | 1.000 | 20.00 | 3584 | 0 | 12.00 | 1792 | 0 |
| 4 | Creek Ln WB | 0 | 1.000 | 0 | 1.000 | 20.00 | 1792 | 0 | 12.00 | 1792 | 0 |

## Bypass Geometry

Bypass Approach Geometry (ft)

| Leg | Leg Names | Bypass <br> Type | Bypass <br> Flows | V | nv | Vb | nvb | Vt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | Yield | 410 | 24 | 2 | 12 | 1 | 24 |

Bypass Entry and Exit Geometry (ft)

| Leg | Leg Names | Eb | neb | Lb | Lt | Rb | Phib | Leg | Leg Names | Exit Lanes <br> nex |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2nd St SB | 12 | 1 | 0 | 130 | 66.00005 <br> 491 | 30 | 2 | Creek Ln EB | 1 |

Bypass Entry Capacity Modifiers and Calibration (veh/hr)

| Leg | Leg Names | Capacity <br> + or - | Eross Walk <br> Factor | Intercept <br> + or - | Calibration <br> Slope |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2nd St SB | 0 | 1.000 | 0 | 1.000 |

## Traffic Flow Data (veh/hr)

## 2040 PM Peak Peak Hour Flows

| Leg | Leg Names | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks <br> $\%$ | Flow Modifiers <br> Flow <br> Factor | Peak Hour <br> Factor |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 85 | 85 | 1030 | 0 | 410 | 5.0 | 1.00 | 0.9 |
| 2 | Creek Ln EB | 0 | 155 | 30 | 90 | 0 | 5.0 | 1.00 | 0.9 |
| 3 | 2nd St NB | 0 | 100 | 905 | 25 | 0 | 5.0 | 1.00 | 0.9 |
| 4 | Creek Ln WB | 0 | 75 | 15 | 35 | 0 | 5.0 | 1.00 | 0.9 |

## Operational Results

## 2040 PM Peak - 60 minutes

Flows and Capacity

| Leg | Leg Names | Bypass | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) <br> Type |  | Arrival Flow |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Entry | Opposing Flow | Expass | Entry | Bypass | Flow | Capacity | Average VCR <br> Entry |  |
| Bypass | Entry | Bypass |  |  |  |  |  |  |  |  |
| 1 | 2nd St SB | Yield | 1200 | 410 | 190 | 190 | 1180 | 2005 | 962 | 0.6075 |
| 2 | Creek Ln EB | None | 275 |  | 1275 |  | 525 | 645 | 0.4343 |  |
| 3 | 2nd St NB | None | 1030 |  | 355 | 1195 | 1843 | 0.4398 |  |  |
| 4 | Creek Ln WB | None | 125 |  | 1245 | 140 | 656 | 0.5676 |  |  |

Delays, Queues and Level of Service

| Leg | Leg Names |  | Bypass | Average Delay (sec) |  | $95 \%$ Queue (veh) |  | Level of Service <br> Type |  | Entry |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |  |  |
| 1 | 2nd St SB | Yield | 4.61 | 6.44 | 5.07 | 5.08 | 2.33 | A | A | A |
| 2 | Creek Ln EB | None | 8.91 |  | 8.91 | 2.40 |  | A | A |  |
| 3 | 2nd St NB | None | 4.38 |  | 4.38 | 4.19 |  | A | A |  |
| 4 | Creek Ln WB | None | 6.33 |  | 6.33 | 0.72 | A | A |  |  |

## 2040 PM Peak - 15 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit <br> Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | 2nd St SB | Yield | 1333 | 456 | 211 | 211 | 1310 | 1984 | 952 | 0.6788 | 0.4853 |
| 2 | Creek Ln EB | None | 306 |  | 1415 |  | 582 | 596 |  | 0.5233 |  |
| 3 | 2nd St NB | None | 1144 |  | 394 |  | 1326 | 1805 |  | 0.6403 |  |
| 4 | Creek Ln WB | None | 139 |  | 1382 |  | 155 | 607 |  | 0.2318 |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass Type | Average Delay (sec) |  |  | 95\% Queue (veh) |  | Level of Service |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | 2nd St SB | Yield | 5.03 | 6.69 | 5.45 | 5.08 | 2.33 | A | A | A |
| 2 | Creek Ln EB | None | 9.93 |  | 9.93 | 2.40 |  | A |  | A |
| 3 | 2nd St NB | None | 4.79 |  | 4.79 | 4.19 |  | A |  | A |
| 4 | Creek Ln WB | None | 6.65 |  | 6.65 | 0.72 |  | A |  | A |

2040 PM Peak
Project: TH 169 \& 2nd St Interchange
50\% Confidence Level
Daylight conditions

Scheme: 2nd St/Creek Ln 2040 PM peak hour
Rodel-Win1 - Full Geometry

## Approach Flow Profile

2040 PM Peak - Approach Flows (Veh / Hour)

| Time Slice | 2nd St SB | Creek Ln EB | 2nd St NB | Creek Ln WB |
| :--- | :---: | :---: | :---: | :---: |
| $0.0-7.5$ | 193.80 | 33.10 | 123.98 | 15.05 |
| $7.5-15.0$ | 193.80 | 33.10 | 123.98 | 15.05 |
| $15.0-22.5$ | 193.80 | 33.10 | 123.98 | 15.05 |
| $22.5-30.0$ | 223.61 | 38.19 | 143.06 | 17.36 |
| $30.0-37.5$ | 223.61 | 38.19 | 143.06 | 17.36 |
| $37.5-45.0$ | 193.80 | 33.10 | 123.98 | 15.05 |
| $45.0-52.5$ | 193.80 | 33.10 | 123.98 | 15.05 |
| $52.5-60.0$ | 193.80 | 33.10 | 143.06 | 15.05 |
| Peak 15 min | 223.61 | 34.19 | 128.75 | 17.36 |
| Peak 60 min | 201.25 |  |  | 15.62 |

## Exit Flow Profile

## 2040 PM Peak - Exit Flows (Veh / Hour)

| Time Slice | 2nd St SB | Creek Ln EB | 2nd St NB | Creek Ln WB |
| :--- | :---: | :---: | :---: | :---: |
| $0.0-7.5$ | 141.84 | 63.03 | 143.65 | 16.83 |
| $7.5-15.0$ | 142.03 | 63.19 | 143.83 | 16.85 |
| $15.0-22.5$ | 142.04 | 63.19 | 143.84 | 16.85 |
| $22.5-30.0$ | 163.55 | 72.68 | 165.64 | 19.40 |
| $30.0-37.5$ | 163.87 | 72.90 | 165.95 | 19.44 |
| $37.5-45.0$ | 142.37 | 63.42 | 144.17 | 16.90 |
| $45.0-52.5$ | 142.05 | 63.20 | 143.85 | 16.85 |
| $52.5-60.0$ | 142.04 | 63.20 | 143.84 | 16.85 |
| $0-60$ | 1180 | 525 | 5.00 | 140 |
| $\%$ Trucks | 5.00 | 5.00 |  | 5.00 |

2040 PM Peak
50\% Confidence Level
Daylight conditions

Project: TH 169 \& 2nd St Interchange
Scheme: 2nd St/Creek Ln 2040 PM peak hour
Rodel-Win1 - Full Geometry

## Economics

## Economic Input Data

## 2040 - Vehicle Delay Parameters

| Peaks | Peak / Day | Days / Year | Delay Cost <br> (\$ / hour) |
| :---: | :---: | :---: | :---: |
| AM Peak | 1 | 325 | 15.00 |
| OFF Peak | 14 | 325 | 15.00 |
| PM Peak | 1 | 325 | 15.00 |

## 2040 - Accident Severity Proportions and Costs

| Accident Type | Proportion (\%) | Cost (\$) |
| :--- | :---: | :---: |
| Fatal Vehicle Accident | 0.3 | 0 |
| Incapacitating Vehicle Accident | 17.7 | 0 |
| Non-incapacitating Vehicle Accident | 82 | 0 |
| Damage Only Vehicle Accident | 100 | 0 |
| Pedestrian Injury Accident | 100 | 0 |

## Economics - Results Data

2040 Delay and Accident Costs

|  | Delay Costs <br> Delays <br> Veh.hrs | Costs <br> (\$) | Accident <br> Types | Accident Costs <br> Annual <br> Accidents | Accident <br> Costs | Total Costs <br> Cost <br> Type | Costs <br> (\$/year) |
| :--- | :---: | :--- | :--- | :---: | :---: | :---: | :---: |
| AM | 0.00 | 0 | Vehicles Injury | 0.00 | 0 | Vehicle Delay Cost | 21569 |
| OFF | 0.00 | 0 | Vehicles DO | 0.00 | 0 | Vehicle Injury Acc Cost | 0 |
| PM | 1437.96 | 21569 | Pedestrians | 0.00 | 0 | Vehicle DO Acc Cost | 0 |
|  |  |  |  |  |  | Pedestrian Accident Cost | 0 |
|  |  |  |  |  |  | Total Accident Cost | 0 |
| Total | 1437.96 | 21569 | Totals | 0.00 | 0 | TOTAL COST | 21569 |

## Global Results

## Performance and Accidents

2040 PM Peak Global Performance

| Parameter | Units | Entries | Bypasses | Total |
| :--- | :---: | :---: | :---: | :---: |
| Arrive Flows | $\mathrm{veh} / \mathrm{hr}$ | 2630 | 410 | 3040 |
| Capacity | $\mathrm{veh} / \mathrm{hr}$ | 5149 | 962 | 6111 |
| Average Delay | $\mathrm{sec} / \mathrm{veh}$ | 5.05 | 6.44 | 5.24 |
| L.O.S. (Signal) | $\mathrm{A}-\mathrm{F}$ | A | A | A |
| L.O.S. (Unsig) | $\mathrm{A}-\mathrm{F}$ | A | A | A |
| Total Delay | veh.hrs | 3.69 | 0.73 | 4.42 |

## Scheme Summary

## Control Data

## Control Data and Model Parameters

| TH 169 \& 2nd St Interchange | 2040 PHF Flow Profile (veh) |
| :--- | :--- |
| WB ramps/2nd St/Frontage Rd 2040 AM Peak | 7.5 min Time Slice |
| Rodel-Win1 | Queuing Delays (sec) |
| Right Hand Drive | Daylight conditions |
| AM Peak Hour | Peak 60/15 min Results |
| Full Geometry | Output flows: Vehicles |
| English Units (ft) | $50 \%$ Confidence Level |

## Available Data

| Entry Capacity Calibrated | No |
| :--- | :---: |
| Entry Capacity Modified | No |
| Crosswalks | No |
| Flows Factored | No |
| Approach/Exit Road Capacity Calibrated | No |
| Accidents | No |
| Accident Costs | No |
| Bypass Model | No |
| Bypass Calibration | No |
| Global Results | Yes |

## Operational Data

## Main Geometry (ft)

## Approach and Entry Geometry

| Leg | Leg Names | Approach <br> Bearing <br> (deg) | Grade <br> Separation <br> $\mathbf{G}$ | Half Width <br> $\mathbf{V}$ | Approach <br> Lanes <br> $\mathbf{n}$ | Entry <br> Width <br> $\mathbf{E}$ | Entry <br> Lanes <br> $\mathbf{n}$ | Flare <br> Length <br> $\mathbf{L}^{\prime}$ | Entry <br> Radius <br> $\mathbf{R}$ | Entry <br> Angle <br> $?$ |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 0 | 0 | 24.00 | 2 | 28.00 | 2 | 131.00 | 66.00 | 30.00 |
| 2 | WB on ramp | 90 | 0 | 12.00 | 1 | 14.00 | 1 | 131.00 | 66.00 | 30.00 |
| 3 | 2nd St NB | 180 | 0 | 24.00 | 2 | 28.00 | 2 | 131.00 | 66.00 | 30.00 |
| 4 | WB off ramp | 270 | 0 | 24.00 | 2 | 28.00 | 2 | 131.00 | 66.00 | 30.00 |
| 5 | Frontage SWB | 315 | 0 | 12.00 | 1 | 14.00 | 1 | 131.00 | 66.00 | 30.00 |

## Circulating and Exit Geometry

| Leg | Leg Names | Inscribed <br> Diameter <br> D | Circulating <br> Width <br> C | Circulating <br> Lanes <br> nc | Exit <br> Width <br> Ex | Exit <br> Lanes <br> nex | Exit <br> Half Width <br> Vx | Exit Half <br> Width Lanes <br> nvx |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 230.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |
| 2 | WB on ramp | 230.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |
| 3 | 2nd St NB | 230.00 | 15.00 | 1 | 28.00 | 2 | 24.00 | 2 |
| 4 | WB off ramp | 230.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |
| 5 | Frontage SWB | 230.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |

Capacity Modifiers and Capacity Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity |  | Entry Calibration |  | Approach Road |  |  | Exit Road |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Capacity + or - | XWalk <br> Factor | Intercept + or - | Slope Factor | V <br> (ft) | Default Capacity | Calib Capacity | V (ft) | Default Capacity | Calib Capacity |
| 1 | 2nd St SB | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 12.00 | 1792 | 0 |
| 2 | WB on ramp | 0 | 1.000 | 0 | 1.000 | 24.00 | 1792 | 0 | 12.00 | 1792 | 0 |
| 3 | 2nd St NB | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 24.00 | 3584 | 0 |
| 4 | WB off ramp | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 12.00 | 1792 | 0 |
| 5 | Frontage SWB | 0 | 1.000 | 0 | 1.000 | 24.00 | 1792 | 0 | 12.00 | 1792 | 0 |

## Traffic Flow Data (veh/hr)

2040 AM Peak Peak Hour Flows

| Leg | Leg Names | U-Turn | Exit-4 | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks <br> $\%$ | Flow Modifiers <br> Flow <br> Factor | Peak Hour <br> Factor |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 0 | 30 | 0 | 700 | 150 | 0 | 5.0 | 1.00 | 0.9 |
| 2 | WB on ramp | 0 | 0 | 0 | 0 | 1 | 0 | 5.0 | 1.00 | 0.9 |
| 3 | 2nd St NB | 0 | 280 | 770 | 110 | 0 | 0 | 5.0 | 1.00 | 0.9 |
| 4 | WB off ramp | 0 | 110 | 0 | 170 | 5 | 0 | 5.0 | 1.00 | 0.9 |
| 5 | Frontage SWB | 0 | 0 | 130 | 25 | 10 | 0 | 5.0 | 1.00 | 0.9 |

## Operational Results

## 2040 AM Peak - 60 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | 2nd St SB | None | 880 |  | 545 |  | 950 | 1869 |  | 0.4776 |  |
| 2 | WB on ramp | None | 1 |  | 970 |  | 455 | 812 |  | 0.0013 |  |
| 3 | 2nd St NB | None | 1160 |  | 30 |  | 941 | 2165 |  | 0.5430 |  |
| 4 | WB off ramp | None | 285 |  | 1190 |  | 0 | 1490 |  | 0.1950 |  |
| 5 | Frontage SWB | None | 165 |  | 1330 |  | 145 | 759 |  | 0.2222 |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass Type | Average Delay (sec) |  |  | 95\% Queue (veh) |  | Level of Service |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | 2nd St SB | None | 3.98 |  | 3.98 | 3.14 |  | A |  | A |
| 2 | WB on ramp | None | 0.00 |  | 0.00 | 0.00 |  | A |  | A |
| 3 | 2nd St NB | None | 4.22 |  | 4.22 | 4.30 |  | A |  | A |
| 4 | WB off ramp | None | 4.55 |  | 4.55 | 1.15 |  | A |  | A |
| 5 | Frontage SWB | None | 5.64 |  | 5.64 | 0.84 |  | A |  | A |

## 2040 AM Peak - 15 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | 2nd St SB | None | 978 |  | 605 |  | 1055 | 1834 |  | 0.5378 |  |
| 2 | WB on ramp | None | 1 |  | 1077 |  | 505 | 780 |  | 0.0014 |  |
| 3 | 2nd St NB | None | 1289 |  | 33 |  | 1045 | 2162 |  | 0.6015 |  |
| 4 | WB off ramp | None | 317 |  | 1321 |  | 0 | 1413 |  | 0.2264 |  |
| 5 | Frontage SWB | None | 183 |  | 1477 |  | 161 | 715 |  | 0.2597 |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass Type | Average Delay (sec) |  |  | 95\% Queue (veh) |  | Level of Service |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | 2nd St SB | None | 4.21 |  | 4.21 | 3.14 |  | A |  | A |
| 2 | WB on ramp | None | 0.00 |  | 0.00 | 0.00 |  | A |  | A |
| 3 | 2nd St NB | None | 4.44 |  | 4.44 | 4.30 |  | A |  | A |
| 4 | WB off ramp | None | 4.70 |  | 4.70 | 1.15 |  | A |  | A |
| 5 | Frontage SWB | None | 5.88 |  | 5.88 | 0.84 |  | A |  | A |

## Approach Flow Profile

2040 AM Peak - Approach Flows (Veh / Hour)

| Time Slice | 2nd St SB | WB on ramp | 2nd St NB | WB off ramp | Frontage SWB |
| :--- | :---: | :---: | :---: | :---: | :---: |
| $0.0-7.5$ | 105.93 | 0.12 | 139.63 | 34.31 | 19.86 |
| $7.5-15.0$ | 105.93 | 0.12 | 139.63 | 34.31 | 19.86 |
| $15.0-22.5$ | 105.93 | 0.12 | 139.63 | 34.31 | 19.86 |
| $22.5-30.0$ | 122.22 | 0.14 | 161.11 | 39.58 | 22.92 |
| $30.0-37.5$ | 122.22 | 0.14 | 161.11 | 39.58 | 22.92 |
| $37.5-45.0$ | 105.93 | 0.12 | 139.63 | 34.31 | 19.86 |
| $45.0-52.5$ | 105.93 | 0.12 | 139.63 | 34.31 | 19.86 |
| $52.5-60.0$ | 105.93 | 0.12 | 139.63 | 34.31 | 19.86 |
| Peak 15 min | 122.22 | 0.14 | 161.11 | 39.58 | 22.92 |
| Peak 60 min | 110.00 | 0.12 | 145.00 | 35.63 | 20.63 |

## Exit Flow Profile

2040 AM Peak - Exit Flows (Veh / Hour)

| Time Slice | 2nd St SB | WB on ramp | 2nd St NB | WB off ramp | Frontage SWB |
| :--- | :---: | :---: | :---: | :---: | :---: |
| $0.0-7.5$ | 114.24 | 54.71 | 113.15 | 0.00 | 17.44 |
| $7.5-15.0$ | 114.35 | 54.77 | 113.26 | 0.00 | 17.45 |
| $15.0-22.5$ | 114.35 | 113.27 | 0.00 | 17.45 |  |
| $22.5-30.0$ | 131.77 | 63.11 | 130.52 | 0.00 | 20.11 |
| $30.0-37.5$ | 131.94 | 63.19 | 130.69 | 0.00 | 20.14 |
| $37.5-45.0$ | 114.52 | 54.85 | 113.44 | 0.00 | 17.48 |
| $45.0-52.5$ | 114.36 | 54.77 | 113.27 | 0.00 | 17.45 |
| $52.5-60.0$ | 114.35 | 455 | 941 | 0.00 | 17.45 |
| $0-60$ | 950 | 5.00 | 5.00 | 0.00 | 145 |
| $\%$ Trucks |  |  |  | 5.00 |  |

## Economics

## Economic Input Data

2040 - Vehicle Delay Parameters

| Peaks | Peak / Day | Days / Year | Delay Cost <br> $(\$ /$ hour $)$ |
| :---: | :---: | :---: | :---: |
| AM Peak | 1 | 325 | 15.00 |
| OFF Peak | 14 | 325 | 15.00 |
| PM Peak | 1 | 325 | 15.00 |

2040 - Accident Severity Proportions and Costs

| Accident Type | Proportion (\%) | Cost (\$) |
| :--- | :---: | :---: |
| Fatal Vehicle Accident | 0.3 | 0 |
| Incapacitating Vehicle Accident | 17.7 | 0 |
| Non-incapacitating Vehicle Accident | 82 | 0 |
| Damage Only Vehicle Accident | 100 | 0 |
| Pedestrian Injury Accident | 100 | 0 |

## Economics - Results Data

## 2040 Delay and Accident Costs

| Peak | Delay Costs <br> Delays <br> Veh.hrs | Costs <br> (\$) | Accident <br> Types | Accident Costs <br> Annual <br> Accidents | Accident <br> Costs | Total Costs <br> Cost <br> Type | Costs <br> (\$/year) |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM | 958.87 | 14383 | Vehicles Injury | 0.00 | 0 | Vehicle Delay Cost | 14383 |
| OFF | 0.00 | 0 | Vehicles DO | 0.00 | 0 | Vehicle Injury Acc Cost | 0 |
| PM | 0.00 | 0 | Pedestrians | 0.00 | 0 | Vehicle DO Acc Cost | 0 |
|  |  |  |  |  | Pedestrian Accident Cost | 0 |  |
|  |  |  |  |  | Total Accident Cost | 0 |  |
| Total | 958.87 | 14383 | Totals | 0.00 | 0 | TOTAL COST | 14383 |

## Global Results

## Performance and Accidents

2040 AM Peak Global Performance

| Parameter | Units | Entries | Bypasses |
| :--- | :---: | :---: | :---: |
| Arrive Flows | $\mathrm{veh} / \mathrm{hr}$ | 2491 |  |
| Capacity | $\mathrm{veh} / \mathrm{hr}$ | 7095 | 2491 |
| Average Delay | $\mathrm{sec} / \mathrm{veh}$ | 4.26 | 7095 |
| L.O.S. (Signal) | $\mathrm{A}-\mathrm{F}$ | A | 4.26 |
| L.O.S. (Unsig) | $\mathrm{A}-\mathrm{F}$ | A | A |
| Total Delay | veh.hrs | 2.95 | A |

## Scheme Summary

## Control Data

## Control Data and Model Parameters

| TH 169 \& 2nd St Interchange | 2040 PHF Flow Profile (veh) |
| :--- | :--- |
| WB ramps/2nd St/Frontage Rd 2040 PM Peak | 7.5 min Time Slice |
| Rodel-Win1 | Queuing Delays (sec) |
| Right Hand Drive | Daylight conditions |
| PM Peak Hour | Peak 60/15 min Results |
| Full Geometry | Output flows: Vehicles |
| English Units (ft) | $50 \%$ Confidence Level |

## Available Data

| Entry Capacity Calibrated | No |
| :--- | :---: |
| Entry Capacity Modified | No |
| Crosswalks | No |
| Flows Factored | No |
| Approach/Exit Road Capacity Calibrated | No |
| Accidents | No |
| Accident Costs | No |
| Bypass Model | No |
| Bypass Calibration | No |
| Global Results | Yes |

## Operational Data

## Main Geometry (ft)

## Approach and Entry Geometry

| Leg | Leg Names | Approach <br> Bearing <br> (deg) | Grade <br> Separation <br> $\mathbf{G}$ | Half Width <br> $\mathbf{V}$ | Approach <br> Lanes <br> $\mathbf{n}$ | Entry <br> Width <br> $\mathbf{E}$ | Entry <br> Lanes <br> $\mathbf{n}$ | Flare <br> Length <br> $\mathbf{L}^{\prime}$ | Entry <br> Radius <br> $\mathbf{R}$ | Entry <br> Angle <br> $?$ |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 0 | 0 | 24.00 | 2 | 28.00 | 2 | 131.00 | 66.00 | 30.00 |
| 2 | WB on ramp | 90 | 0 | 12.00 | 1 | 14.00 | 1 | 131.00 | 66.00 | 30.00 |
| 3 | 2nd St NB | 180 | 0 | 24.00 | 2 | 28.00 | 2 | 131.00 | 66.00 | 30.00 |
| 4 | WB off ramp | 270 | 0 | 24.00 | 2 | 28.00 | 2 | 131.00 | 66.00 | 30.00 |
| 5 | Frontage SWB | 315 | 0 | 12.00 | 1 | 14.00 | 1 | 131.00 | 66.00 | 30.00 |

## Circulating and Exit Geometry

| Leg | Leg Names | Inscribed <br> Diameter <br> D | Circulating <br> Width <br> C | Circulating <br> Lanes <br> nc | Exit <br> Width <br> Ex | Exit <br> Lanes <br> nex | Exit <br> Half Width <br> Vx | Exit Half <br> Width Lanes <br> nvx |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 230.00 | 30.00 | 2 | 28.00 | 2 | 24.00 | 2 |
| 2 | WB on ramp | 230.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |
| 3 | 2nd St NB | 230.00 | 15.00 | 1 | 28.00 | 2 | 24.00 | 2 |
| 4 | WB off ramp | 230.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |
| 5 | Frontage SWB | 230.00 | 30.00 | 2 | 14.00 | 1 | 12.00 | 1 |

Capacity Modifiers and Capacity Calibration (veh/hr)

| Leg | Leg Names |  | Entry Capacity <br> Capacity <br> + or - |  | XWalk <br> Factor | Entry Calibration <br> Intercept <br> + or - |  | Slope <br> Factor | Approach Road <br> (ft)   Default <br> Capacity Calib <br> Capacity V <br> (ft) Exit Road <br> Default <br> Capacity Calib <br> Capacity <br> 1        2nd St SB | 0 | 1.000 |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 1.000 | 24.00 | 3584 | 0 | 24.00 | 3584 | 0 |  |  |  |  |
| 2 | WB on ramp | 0 | 1.000 | 0 | 1.000 | 24.00 | 1792 | 0 | 12.00 | 1792 | 0 |
| 3 | 2nd St NB | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 24.00 | 3584 | 0 |
| 4 | WB off ramp | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 12.00 | 1792 | 0 |
| 5 | Frontage SWB | 0 | 1.000 | 0 | 1.000 | 24.00 | 1792 | 0 | 12.00 | 1792 | 0 |

## Traffic Flow Data (veh/hr)

2040 PM Peak Peak Hour Flows

| Leg | Leg Names | U-Turn | Exit-4 | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks <br> $\%$ | Flow Modifiers <br> Flow <br> Factor | Peak Hour <br> Factor |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2nd St SB | 0 | 30 | 0 | 1075 | 350 | 0 | 5.0 | 1.00 | 0.9 |
| 2 | WB on ramp | 0 | 0 | 0 | 0 | 1 | 0 | 5.0 | 1.00 | 0.9 |
| 3 | 2nd St NB | 0 | 370 | 555 | 110 | 0 | 0 | 5.0 | 1.00 | 0.9 |
| 4 | WB off ramp | 0 | 220 | 0 | 160 | 5 | 0 | 5.0 | 1.00 | 0.9 |
| 5 | Frontage SWB | 0 | 0 | 130 | 40 | 20 | 0 | 5.0 | 1.00 | 0.9 |

## Operational Results

## 2040 PM Peak - 60 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | 2nd St SB | None | 1455 |  | 760 |  | 735 | 1743 |  | 0.8649 |  |
| 2 | WB on ramp | None | 1 |  | 1454 |  | 760 | 669 |  | 0.0015 |  |
| 3 | 2nd St NB | None | 1035 |  | 30 |  | 1426 | 2165 |  | 0.4847 |  |
| 4 | WB off ramp | None | 385 |  | 1065 |  | 0 | 1563 |  | 0.2510 |  |
| 5 | Frontage SWB | None | 190 |  | 1305 |  | 145 | 767 |  | 0.2533 |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass Type | Average Delay (sec) |  |  | 95\% Queue (veh) |  | Level of Service |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | 2nd St SB | None | 13.37 |  | 13.37 | 22.16 |  | B |  | B |
| 2 | WB on ramp | None | 0.00 |  | 0.00 | 0.00 |  | A |  | A |
| 3 | 2nd St NB | None | 4.48 |  | 4.48 | 3.99 |  | A |  | A |
| 4 | WB off ramp | None | 4.95 |  | 4.95 | 1.68 |  | A |  | A |
| 5 | Frontage SWB | None | 5.79 |  | 5.79 | 1.00 |  | A |  | A |

## 2040 PM Peak - 15 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | 2nd St SB | None | 1617 |  | 843 |  | 816 | 1694 |  | 0.9852 |  |
| 2 | WB on ramp | None | 1 |  | 1599 |  | 838 | 626 |  | 0.0018 |  |
| 3 | 2nd St NB | None | 1150 |  | 33 |  | 1567 | 2163 |  | 0.5368 |  |
| 4 | WB off ramp | None | 428 |  | 1181 |  | 0 | 1495 |  | 0.2892 |  |
| 5 | Frontage SWB | None | 211 |  | 1448 |  | 160 | 723 |  | 0.2955 |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass Type | Average Delay (sec) |  |  | 95\% Queue (veh) |  | Level of Service |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | 2nd St SB | None | 18.01 |  | 18.01 | 22.16 |  | C |  | C |
| 2 | WB on ramp | None | 0.00 |  | 0.00 | 0.00 |  | A |  | A |
| 3 | 2nd St NB | None | 4.63 |  | 4.63 | 3.99 |  | A |  | A |
| 4 | WB off ramp | None | 5.12 |  | 5.12 | 1.68 |  | A |  | A |
| 5 | Frontage SWB | None | 6.06 |  | 6.06 | 1.00 |  | A |  | A |

## Approach Flow Profile

2040 PM Peak - Approach Flows (Veh / Hour)

| Time Slice | 2nd St SB | WB on ramp | 2nd St NB | WB off ramp | Frontage SWB |
| :--- | :---: | :---: | :---: | :---: | :---: |
| $0.0-7.5$ | 175.14 | 0.12 | 124.58 | 46.34 | 22.87 |
| $7.5-15.0$ | 175.14 | 0.12 | 124.58 | 46.34 | 22.87 |
| $15.0-22.5$ | 175.14 | 0.12 | 124.58 | 46.34 | 22.87 |
| $22.5-30.0$ | 202.08 | 0.14 | 143.75 | 53.47 | 26.39 |
| $30.0-37.5$ | 202.08 | 0.14 | 143.75 | 53.47 | 26.39 |
| $37.5-45.0$ | 175.14 | 0.12 | 124.58 | 46.34 | 22.87 |
| $45.0-52.5$ | 175.14 | 0.12 | 124.58 | 46.34 | 22.87 |
| $52.5-60.0$ | 175.14 | 0.12 | 124.58 | 46.34 | 22.87 |
| Peak 15 min | 202.08 | 0.14 | 143.75 | 53.47 | 26.39 |
| Peak 60 min | 181.88 | 0.12 | 129.38 | 48.13 | 23.75 |

## Exit Flow Profile

2040 PM Peak - Exit Flows (Veh / Hour)

| Time Slice | 2nd St SB | WB on ramp | 2nd St NB | WB off ramp | Frontage SWB |
| :--- | :---: | :---: | :---: | :---: | :---: |
| $0.0-7.5$ | 88.38 | 91.24 | 171.02 | 0.00 | 17.42 |
| $7.5-15.0$ | 88.47 | 91.46 | 171.59 | 0.00 | 17.45 |
| $15.0-22.5$ | 88.47 | 91.47 | 171.63 | 0.00 | 17.45 |
| $22.5-30.0$ | 101.82 | 104.21 | 194.21 | 0.00 | 20.00 |
| $30.0-37.5$ | 102.08 | 105.39 | 197.55 | 0.00 | 20.12 |
| $37.5-45.0$ | 88.73 | 93.03 | 176.10 | 0.00 | 17.61 |
| $45.0-52.5$ | 88.48 | 91.51 | 171.72 | 0.00 | 17.46 |
| $52.5-60.0$ | 88.47 | 760 | 171.67 | 0.00 | 17.45 |
| $0-60$ | 735 | 5.00 | 5.00 | 0 | 145 |
| $\%$ Trucks | 5.00 |  | 0.00 | 5.00 |  |

## Economics

## Economic Input Data

2040 - Vehicle Delay Parameters

| Peaks | Peak / Day | Days / Year | Delay Cost <br> (\$ /hour) |
| :---: | :---: | :---: | :---: |
| AM Peak | 1 | 325 | 15.00 |
| OFF Peak | 14 | 325 | 15.00 |
| PM Peak | 1 | 325 | 15.00 |

2040 - Accident Severity Proportions and Costs

| Accident Type | Proportion (\%) | Cost (\$) |
| :--- | :---: | :---: |
| Fatal Vehicle Accident | 0.3 | 0 |
| Incapacitating Vehicle Accident | 17.7 | 0 |
| Non-incapacitating Vehicle Accident | 82 | 0 |
| Damage Only Vehicle Accident | 100 | 0 |
| Pedestrian Injury Accident | 100 | 0 |

## Economics - Results Data

## 2040 Delay and Accident Costs

| Peak | Delay Costs <br> Delays <br> Veh.hrs | Costs <br> (\$) | Accident <br> Types | Accident Costs <br> Annual <br> Accidents | Accident <br> Costs | Total Costs <br> Cost <br> Type | Costs <br> (\$/year) |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM | 0.00 | 0 | Vehicles Injury | 0.00 | 0 | Vehicle Delay Cost | 36683 |
| OFF | 0.00 | 0 | Vehicles DO | 0.00 | 0 | Vehicle Injury Acc Cost | 0 |
| PM | 2445.53 | 36683 | Pedestrians | 0.00 | 0 | Vehicle DO Acc Cost | 0 |
|  |  |  |  |  |  | Pedestrian Accident Cost | 0 |
|  |  |  |  |  |  | Total Accident Cost | 0 |
| Total | 2445.53 | 36683 | Totals | 0.00 | 0 | TOTAL COST | 36683 |

## Global Results

## Performance and Accidents

2040 PM Peak Global Performance

| Parameter | Units | Entries | Bypasses |
| :--- | :---: | :---: | :---: |
| Arrive Flows | $\mathrm{veh} / \mathrm{hr}$ | 3066 |  |
| Capacity | $\mathrm{veh} / \mathrm{hr}$ | 6908 | 3066 |
| Average Delay | $\mathrm{sec} / \mathrm{veh}$ | 8.84 | 6908 |
| L.O.S. (Signal) | $\mathrm{A}-\mathrm{F}$ | A | 8.84 |
| L.O.S. (Unsig) | $\mathrm{A}-\mathrm{F}$ | A | A |
| Total Delay | veh.hrs | 7.52 | A |

## APPENDIX F - PRELIMINARY COST ESTIMATES



PRELIMINARY COST ESTIMATE - OPTION 1A (OPTION 1 PLUS RR OVERPASS)


## NOTES:

1. NO WATERMAIN OR SANITARY SEWER IMPROVEMENTS INCLUDED.
2. INCLUDES NO SOIL CORRECTION COSTS. NO GEOTECHNICAL EXPLORATION WAS COMPLETED FOR THE CONCEPTUAL DESIGN.
3. WETLAND IMPACTS BASED ON NWI. WETLAND MITIGATION RATIO 2.5:1. ASSUMED PURCHASE OF BANK CREDITS REQUIRED AT $\$ 2.50 / \mathrm{SF}$. 4. PAVEMENT SECTION FOR TRIANGLE LANE INCLUDES 2" BITUMINOUS WEAR, 2" NON-WEAR, AND 12" CLASS 5 AGGREGATE BASE.
4. PAVEMENT SECTION FOR CREEK LANE INCLUDES 2" BIT. WEAR, 2.5" NON-WEAR, $10^{\prime \prime}$ CLASS 5, AND $12^{\prime \prime}$ SELECT GRANULAR.
5. TH 282, CR 9 \& RAMP PAVEMENT SECTION INCLUDES 4" BIT. WEAR, $3^{\prime \prime}$ NON-WEAR, 12 " CLASS 5, AND 24 " SELECT GRANULAR.
6. ASSUMES THAT FLOODPLAIN LOSS CAN BE MITIGATED ON-SITE.


PRELIMINARY COST ESTIMATE - OPTION 3 (ROUNDABOUT/SPLIT DIAMOND)



## APPENDIX G - IMPLEMENTATION PLAN CONCEPT



## DEPARTMENT OF TRANSPORTATION

Minnesota Department of Transportation-Metro District<br>1500 County Rd B-2<br>Roseville, MN 55113

November 14, 2018
Mr. Tom Nikunen
Jordan City Administrator
210 East First Street
Jordan, MN 55352

Dear Mr. Nikunen,
The Minnesota Department of Transportation (MnDOT) appreciates the opportunity to work with the City of Jordan and Scott County on a concept study to address the need for a future interchange at Hwy 169/282/CSAH 9 in Jordan. We support grade-separating this intersection by removing the existing signal and constructing an interchange that meets both transportation and community needs. We understand that this interchange will increase safety and mobility and help the City of Jordan sustain local businesses and plan for future development. After months of environmental screening, traffic study and stakeholder involvement, several concepts have been developed to carry forward into an environmental document. MnDOT is in support of many of these concepts, but we also have some concerns about others. This letter is to clarify MnDOT's interests so that these can be factored into decisions about next steps.

As you know, MnDOT has had several large Hwy 169 paving projects near this intersection in recent years. In 2015, we reconstructed the highway from just south of Hwy 282/CSAH 9 to about a half mile north of Hwy 21, including Hwy 169 bridge repairs. In 2018, we constructed a concrete overlay from just south of Hwy 282/CSAH 9 (where the 2015 project ended) all the way to the Metro District border at Hwy 19. These were major pavement investments and the expected service life is $25-30$ years. For this reason, MnDOT is not in support of concepts that realign or raise Hwy 169. It would not be responsible or prudent to consider concepts that would render the new pavement work in the intersection area as throw away. In addition, CSAH 9 is a roadway leading to an important Minnesota River crossing. Currently, there is an at-grade RR crossing on CSAH 9 just to the north of Hwy 169. The number of trains using that track currently is minimal. This could change in the future. MnDOT supports options that would leave us the opportunity to grade separate that RR crossing should the need arise. Constructing an interchange that brings Hwy 169 over Hwy 282/CSAH 9 precludes that from occurring. Only the options raising Hwy 282/CSAH 9 over Hwy 169 would make that feasible.

Now that the study is narrowing down the interchange concepts and looking for future regional funding, it's important to complete the Metropolitan Council's Appendix F Preliminary Interchange Approval Process. Its purpose is to demonstrate that the proposed project is consistent with the region's long-range plans and that its location is suitable for an interchange based on general transportation planning principles.

More information can be found at the following link: https://metrocouncil.org/Transportation/Planning-2/Key-Transportation-Planning-Documents/Transportation-Policy-Plan/tpp-update/2018-TPP-Update-
Appendices/Appendix-F-Preliminary-Interchange-Appropriation.aspx
MnDOT appreciates the transportation partnership that we've established with the City of Jordan and Scott County. The current Hwy 169/282/CSAH 9 interchange concept study is one more example of us collaborating effectively. We look forward to continuing our work together to get one step closer to making the future Hwy 169/282/CSAH 9 interchange a reality.

Please let me know if you have any questions or if you'd like to discuss this further.


Acting South Area Manager

CC: Lisa Freese, Scott County
Toni Winiecki, Scott County
Almin Ramic, MnDOT Traffic
Michael Corbett, MnDOT Planning

Equal Opportunity Employer

APPENDIX I - DECEMBER 18, 2018 SCOTT COUNTY LETTER

## SCOTT COUNTY BOARD OF COMMISSIONERS

200 FOURTH AVENUE WEST • SHAKOPEE, MN 55379-1220
(952)496-8100 - Fax (952)496-8180 *ww.scottcountymn.gov

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JON ULRICH, DISTRICT 5

December 18, 2018

Mayor Tanya Velishek
210 East First Street
Jordan, MN 55352

Dear Mayor Velishek:
The County would like to take this opportunity to thank the City leaders and staff for their efforts in coming to a general consensus with MnDOT on an interchange vision.

At a recent County Board workshop, the Board members reviewed with County staff the interchange options that were developed through the City's effort. The County supports the planning work done to remove the signal on TH 169. The Board did not make a recommendation on an option since it is too early in the process; however, they support an option that allows grade separation at the Union Pacific Railroad crossing on County Highway 9.

Having recently completed three interchanges, the Board is aware that additional design analysis and environmental work is needed to bring this project to approval. The Board directed an additional $\$ 850,000$ of sales tax funds be set aside in 2019 and 2020 to begin this preliminary design work. This will allow the City, County, and MnDOT to get to an approved layout. Since federal funding will likely be needed to accomplish this project, it is imperative to gain Federal Highway Administration support through detailed engineering and environmental analysis to flesh out all the issues not identified in the recently completed planning study.

The County had previously committed to fund an at-grade separation study at TH 169 and CH 59 with a study in 2019. We would like to discuss performing this work in conjunction with the preliminary design for TH $169 / 282 / \mathrm{CH} 9$, to ensure that the impacts and traffic analysis are looked at comprehensively. In doing so, it will help to coordinate the overall vision for the TH169 corridor and remain consistent with the regional interchange requirements in the Metropolitan Council's Transportation Policy Plan. Completing this work by mid-2020 may provide an opportunity to apply for Federal funds through the Met Council process.

Please continue to work with Lisa Freese, Transportation Services Director, and her staff on these next steps.

Respectfully,


Thomas J. Wolf
Chair and Commissioner, District 2


## Barb Weckman Brake

Vice-Chair and Commissioner, District 1
CC. Thomas Nikunen, City of Jordan, City Administrator Amber Blanchard, MnDOT Acting South Area Manager Lisa Freese, Transportation Services Director


[^0]:    Kimley")Horn $\boldsymbol{\Delta}$ Scout $\boldsymbol{m}$

